

HIERARCHICAL POROUS METAL-ORGANIC FRAMEWORKS (MOFS):  
DESIGN, SYNTHESIS, AND THEIR APPLICATION AS GAS ADSORPTION  
MATERIALS

by  
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## ABSTRACT

### HIERARCHICAL POROUS MOFS: DESIGN, SYNTHESIS, AND THEIR APPLICATIONS AS GAS ADSORPTION MATERIALS

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Climate change is a global concern and interacts with economics, energy, and environment. Alternative energy resources are necessary to act towards global climate change and to produce energy in a sustainable way. In this Ph.D. thesis, hierarchical porous MOFs were designed to enhance the CO<sub>2</sub> and H<sub>2</sub> adsorption capacities of traditional MOFs.

Hierarchical porous MOFs were synthesized via a perturbation assisted nanofusion synthesis strategy at which the sizes of textural pores were controlled by metal to linker ratio and synthesis temperature. Formation of hierarchical pores enhanced the BET surface areas and total pore volumes and the highest of all the reported BET surface areas and the pore volumes for MIL-88B and Fe-BTC are achieved. Introducing hierarchical porosity to the

pore structure enhanced the measured CO<sub>2</sub> and H<sub>2</sub> adsorption capacities at 298 K. The achieved CO<sub>2</sub> and H<sub>2</sub> adsorption capacities (298 K and 1 bar) are higher than those of previously reported ones for MIL-88Bs and Fe-BTCs. The enhanced gas adsorption capacities are attributed to the ultramicropores present in the pore structure which have higher binding energies than the wider pores. This Ph.D. study experimentally proves the necessity of ultramicropores in the gas adsorption studies (at 298 K), reports an effortless, and feasible synthesis strategy that can form hierarchical pores and enhance the textural properties and gas adsorption capacities measured at 298 K. This study paves the way for the design of hierarchical porous MOFs and leads the way for the use of hierarchical porous MOFs in gas adsorption studies.

## ÖZET

### HİYERARŞİK GÖZENEKLİ METAL KAFESLİ YAPILARIN TASARIMI, ÜRETİMİ VE GAZ ADSORPSİYON ÇALIŞMALARINDA ADSORBAN MALZEMELER OLARAK KULLANIMI

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Anahtar Kelimeler: Metal-kafesli yapılar, hiyerarşik gözenekli MOFlar, hiyerarşik gözenekler, karbon dioksit adsorpsiyonu, hidrojen adsorpsiyonu

İklim değişikliği, ekonomi, enerji ve çevre ile etkileşime giren küresel bir sorundur. Alternatif enerji kaynakları, küresel iklim değişikliğine karşı harekete geçmek ve sürdürülebilir enerji üretimi için gereklidir. Bu doktora tezinde, hiyerarşik gözenekli metal-kafesli yapılar (MOFlar) gaz adsorpsiyon çalışmalarında kullanılmak üzere ve oda sıcaklığında ölçülen CO<sub>2</sub> ve H<sub>2</sub> adsorpsiyon kapasitelerini arttırmak için tasarlanmıştır. Hiyerarşik gözenekli bir yapı oluşturmak için şablonsuz, kolay uygulanabilir bir sentez stratejisi kullanılmıştır. Hiyerarşik gözenekli MOFlar dokusal gözenek boyutlarının metal

bağlayıcı oranı ile ve sentez sıcaklığı ile kontrol edilebildiği pertürbasyon destekli nanofüzyon sentez stratejisi ile sentezlenmiştir. Bu çalışmada sentezlenen hiyerarşik gözenekli MOFların BET yüzey alanları ve toplam gözenek hacimleri önemli miktarda artmış ve literatürde bugüne kadar MIL-88B ve Fe-BTC için rapor edilen en yüksek BET yüzey alanına ve toplam gözenek hacmine ulaşılmıştır.

Hiyerarşik gözenekler sentezlemek, 298 K'de ölçülen CO<sub>2</sub> ve H<sub>2</sub> adsorpsiyon kapasitelerini arttırmıştır. Ulaşılan CO<sub>2</sub> ve H<sub>2</sub> adsorpsiyon kapasiteleri (298 K ve 1 bar) MIL-88B ve Fe-BTC için daha önce bildirilen adsorpsiyon kapasitelerinden daha yüksektir. Artan gaz adsorpsiyon kapasiteleri, daha yüksek bağlanma enerjisine sahip ultramikro gözenek yapıları ile ilişkilendirilmiştir. Bu doktora tez çalışması ile gaz adsorpsiyon çalışmalarında ultramikro gözenek yapılarının gerekliliği deneysel olarak kanıtlanmış, hiyerarşik gözenek oluşturan ve 298 K'de ölçülen gaz adsorpsiyon kapasitelerini arttıran bir sentez yöntemi ve hiyerarşik gözeneklerin boyutlarının sentez parametreleri ile değiştirilme mekanizması rapor edilmiştir. Bu çalışma, hiyerarşik gözenekli MOFların tasarımına zemin hazırlamakta ve hiyerarşik gözenekli MOFların gaz adsorpsiyon çalışmalarında kullanılması için öncü olmaktadır.

*This thesis has been dedicated to my beloved parents, Figen and Mustafa Yurduşen, who  
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## LIST OF SYMBOLS AND ABBREVIATIONS

ACs: Activated carbons  
ACS: American Chemical Society  
BTC: Benzene-1,3,5-tricarboxylic acid  
CNTs: Carbon nanotubes  
APTS: 3-aminopropyl-triethoxysilane  
BET: Brunauer Emmett Teller  
CCS: Carbon capture and storage  
CO<sub>2</sub>: Carbon dioxide  
DMF: N, N-Dimethylformamide  
DOE: U.S. Department of Energy  
DMAB: (dimethylamino)-2-butanol  
FeCl<sub>3</sub>·6H<sub>2</sub>O: Iron(III) chloride hexahydrate  
FTIR: Fourier Transformed Infrared Spectroscopy  
HEEBAB: 4-((2-hydroxyethyl)(ethyl)amino)-2-butanol  
HEMAB: 4-((2 hydroxyethyl)(methyl)amino)-2-butanol  
HPLC: High performance liquid chromatography  
IEA: International Energy Agency  
IGA: Intelligent Gravimetric Analyzer  
ILs: Ionic liquids  
IUPAC: International Union of Pure and Applied Chemistry  
IPCC: Intergovernmental Panel on Climate Change  
MEA: Monoethanolamine  
MeOH: Methanol  
MOFs: Metal-organic frameworks  
NH<sub>3</sub>: Ammonia  
NLDFT: Non-Local Density Functional Theory  
PDMS: Polydimethylsiloxane  
PE: Polyethylene  
PP: Polypropylene  
PTFE: Polytetrafluoroethylene

PVDF: Polyvinylidene fluoride  
PXRD: Powder x-ray diffraction  
rGO: Reduced graphene oxide  
SBUs: Secondary building units  
SEM: Scanning Electron Microscopy  
STP: Standard temperature and pressure  
TEA: Triethanolamine  
TGA: Thermal Gravimetric Analyzer  
TPA: Benzene-1,4-dicarboxylic acid  
XRD: X-ray Diffraction  
 $C_e$ : Adsorbate concentration in equilibrium (mg/L)  
 $K_a$ : Langmuir adsorption constant (L/mg)  
 $K_F$ : Freundlich constant (mg/g)  
 $1/n$ : Measure of intensity (Freundlich isotherm)  
 $Q_e$ : Solute amount adsorbed per unit weight of adsorbent (mg/g)  
 $Q_m$ : Capacity at monolayer coverage (mg/g)  
 $Q_o$ : Maximum monolayer coverage capacity(mg/g)  
 $R^2$ : Coefficient of determination value  
 $\Delta G$ : Free energy change  
 $\Delta H$ : Ethalphy change (kJ/ mol)  
 $\Delta S$ : Entropy change (kJ/mol)

## Chapter I

### Introduction

*“I’d put my money on the sun and solar energy, what a source of power. I hope we don’t have to wait until oil and coal run out, before we tackle that”.*

*Thomas Edison, 1931*

#### **1.1. Motivation**

We, humanity, are the richest of all times, have prolonged life times, we have developed technology, we have machines that can solve even the most difficult problems that we cannot solve. However, we still cannot figure out a solution for climate change which poses a direct threat on our rights to access clean, safe, and cheap water, clean air, food, energy, our health, and our communities’ development.

Climate change is a global concern, at which a vision has to be shared globally, and a world-wide cooperation has to be established. Climate change interacts with economics, energy and environment. While trying to find out a solution, we should always keep in mind that economics, energy and environment cannot be separated from each other. Energy is necessary for the development of the society but also it is the major contributor to the anthropogenic greenhouse gas emissions. We do need alternative energy resources to act towards global climate change and resupply the depleted hydrocarbon reserves. Moreover, the development of alternative energy sources has to be fast enough to keep the depletion pace of hydrocarbon sources while switching our conventional energy sources into alternative energy sources.



## 1.2. Challenges and research needs

10% of the CO<sub>2</sub> produced today remains in the atmosphere for ten thousand years, which makes CO<sub>2</sub> come to the front. To reduce the risks and the magnitude of the impacts of climate change, a target has been set by Intergovernmental Panel on Climate Change (IPCC) which limits the global temperature rise to 1.5 °C. However, none of the mitigation measures are able to decrease the CO<sub>2</sub> emissions to zero, unless all of them, together applied.

Carbon capture and storage (CCS) is one of the measures that can decrease the CO<sub>2</sub> emissions by 80 to 90% in power plants. Absorption process which is the mostly used CO<sub>2</sub> capture technology is limited by its high energy demand, energy intensive regeneration processes, by-product formation (ammonia and salts), and decreased absorption capacities due to absorption of end-products. In the meanwhile, the use of membrane contactors is limited by membrane degradation, membrane fouling, and membrane wetting. For the commercial use of membrane contactors, these limitations should be overcome and chemically and thermally stable membranes should be developed at industrial scale.

Adsorption comes to front with its low-cost, less energy intensive regeneration processes, feasibility, and easy applicability. However, for the commercial use of adsorbents, there is still room for improvement. For instance, carbon-based materials show low CO<sub>2</sub> adsorption performances, and low selectivity; zeolites show low CO<sub>2</sub> adsorption performances. CO<sub>2</sub> adsorption capacities of silica-based materials decrease at high temperatures. Polymer-based materials show promising CO<sub>2</sub> adsorption capacities. However, after several adsorption and desorption cycles, CO<sub>2</sub> adsorption capacities of polymer-based materials decrease, drastically. Alkali-metal carbonate-based materials are also investigated for their use in CO<sub>2</sub> adsorption studies. However, the low durability, and slow carbonation reaction rates limits the use of these materials in practical applications. The CO<sub>2</sub> adsorption capacities of MgO and CaO based materials are also investigated. However, the use of MgO based sorbents are limited with the long regeneration processes while the use of CaO based sorbents are limited with the low durability, and short-life cycle of these materials.

MOFs get ahead of the above-mentioned adsorbents owing to their tunable topology, high BET surface area, and high porosity. However, due to weak van der Waals interactions between CO<sub>2</sub> molecules and MOFs, adsorption capacity of MOFs decreases drastically at

ambient temperature. Despite all the strategies developed and the progresses made, it is still a challenge to achieve an optimum CO<sub>2</sub> adsorption capacity at 298 K. There remains a big room to develop MOFs with larger isosteric heat of adsorption values.

Transport sector contribute to the overall greenhouse gas emissions by 14%. Hydrogen is a promising alternative to fossil fuels since it is abundant, and no by-product is formed. However, storing hydrogen in a safe, light and economic way still remains as a challenge which is necessary for the practical use of on-board hydrogen storage systems. Among the hydrogen storage methods investigated to date, physisorption comes to front owing to its low cost and feasibility. However, physisorption is limited by the weak van der Waals forces and despite the high H<sub>2</sub> adsorption capacities measured at 77 K, the measured H<sub>2</sub> adsorption capacities decrease dramatically at room temperature and atmospheric pressure.

Carbon-based materials were considered as promising H<sub>2</sub> storage materials owing to their availability, low-cost, high BET surface areas, and high porosities. However, when the H<sub>2</sub> adsorption studies are conducted at 298 K, the measured H<sub>2</sub> adsorption capacities decrease drastically. Despite the developed strategies and enhancements achieved, the measured H<sub>2</sub> adsorption capacities are far from meeting the U.S. DOE target of on-board hydrogen storage.

Zeolites are another family of materials that were considered as promising candidates as on-board hydrogen storage materials. Despite all the strategies developed, H<sub>2</sub> adsorption capacities of zeolite-based materials are also far from achieving the U.S. DOE target of on-board hydrogen storage.

MOFs are considered as promising candidates for hydrogen storage studies and get ahead of other materials owing to their high porosity, tunability and promising results obtained from H<sub>2</sub> adsorption measurements at 77 K. Despite the very high H<sub>2</sub> adsorption capacities measured at 77 K and high pressures, H<sub>2</sub> adsorption capacities of MOFs decrease drastically at 298 K and atmospheric pressure. It is still a challenge to design a MOF with a high H<sub>2</sub> adsorption capacity that meets the U.S. DOE target of on-board hydrogen storage.

The low H<sub>2</sub> adsorption capacities of MOFs at 298 K are attributed to the very weak van der Waals interactions between MOFs and H<sub>2</sub> molecules. The very weak van der Waals interactions result isosteric heat of adsorption values of MOFs to vary in between 4 to 7 kJ/mol while to adsorb considerable amount of H<sub>2</sub> at ambient temperature 15 kJ/mol of

energy is needed. In order to develop MOFs that function optimally at 298 K, binding energies between the H<sub>2</sub> molecules and MOFs should be enhanced and a MOF that possesses an adsorption enthalpy of 15 kJ/mol should be developed.

### **1.3. Objective of thesis**

The overall objective of this Ph.D. study is to develop hierarchical porous MOFs, enhance their gas adsorption capacities measured at 298 K, and show the influence of pore size and pore size distribution on the gas adsorption capacities measured at 298 K.

The scope is to synthesize hierarchical porous MOFs with different pore size and pore size distributions, and characterize these materials, analyze their pore size and pore size distribution extensively, and measure and evaluate the CO<sub>2</sub> and H<sub>2</sub> adsorption capacities. The CO<sub>2</sub> and H<sub>2</sub> adsorption behaviors of these materials are further studied by analyzing their pore size distributions, in detail. The findings are used to develop adsorbents with enhanced gas adsorption capacities. The objectives of this study are listed as follows:

- (1) To synthesize hierarchically porous MOFs with different pore size distributions,
- (2) To optimize synthesis parameters to form textural pores with different pore diameters,
- (3) To investigate CO<sub>2</sub> and H<sub>2</sub> adsorption capacities of hierarchical porous MOFs,
- (4) To evaluate the CO<sub>2</sub> and H<sub>2</sub> adsorption behaviors of the hierarchical porous MOFs with pore size distribution analysis,
- (5) To develop a hierarchical porous MOF with enhanced CO<sub>2</sub> and H<sub>2</sub> adsorption capacity.

### **1.4. Thesis outline**

This thesis is divided into eight chapters. You can find the content of the chapters as listed below:

- Chapter I presents the motivation, challenges and research needs, objectives, and outline of thesis,

- Chapter II provides a brief literature survey of climate change, mitigation measures, gas adsorption theory, materials used for CO<sub>2</sub> adsorption studies, metal-organic frameworks (MOFs), and hierarchical porous MOFs,
- Chapter III describes the synthesis method and the characterization analyses of hierarchical porous MIL-88Bs, and discusses the effect of iron to benzene-1,4-dicarboxylic acid ratio and synthesis temperature on the textural properties of hierarchical porous MIL-88Bs,
- Chapter IV investigates the CO<sub>2</sub> adsorption capacity of hierarchically porous MIL-88Bs and discusses the crucial role of narrow micropores on the CO<sub>2</sub> adsorption capacity of hierarchically porous MIL-88Bs,
- Chapter V examines the H<sub>2</sub> adsorption capacity of hierarchically porous MIL-88Bs and discusses the role of ultramicropores on the H<sub>2</sub> adsorption capacity of hierarchically porous MIL-88Bs,
- Chapter VI describes the synthesis and the characterization analyses of hierarchical porous Fe-BTCs, and investigates the CO<sub>2</sub> adsorption capacity of Basolite F300 like hierarchical porous Fe-BTCs,
- Chapter VII presents the results of H<sub>2</sub> adsorption studies conducted with hierarchically porous Fe-BTCs and discusses the influence of pore size distribution on the H<sub>2</sub> adsorption capacity,
- Chapter VIII summarizes the conclusions of the study and discusses the possible further work.

## Chapter II

### Literature Survey

#### 2.1. Introduction

The impact of carbon dioxide (CO<sub>2</sub>) on the Earth's surface temperature was firstly mentioned by Arrhenius (Svante, 1896). From the pre-industrial period (1850 to 1900) till today, the global surface temperature has increased by 1 °C (IPCC, 2018). Moreover, the five warmest years were recorded since 2010 (NASA, 2019) and the year 2016 has been reported as the warmest year since 1880 (NASA/GISS, 2019). The following graph (Figure 1) shows the temperature anomaly with respect to years.

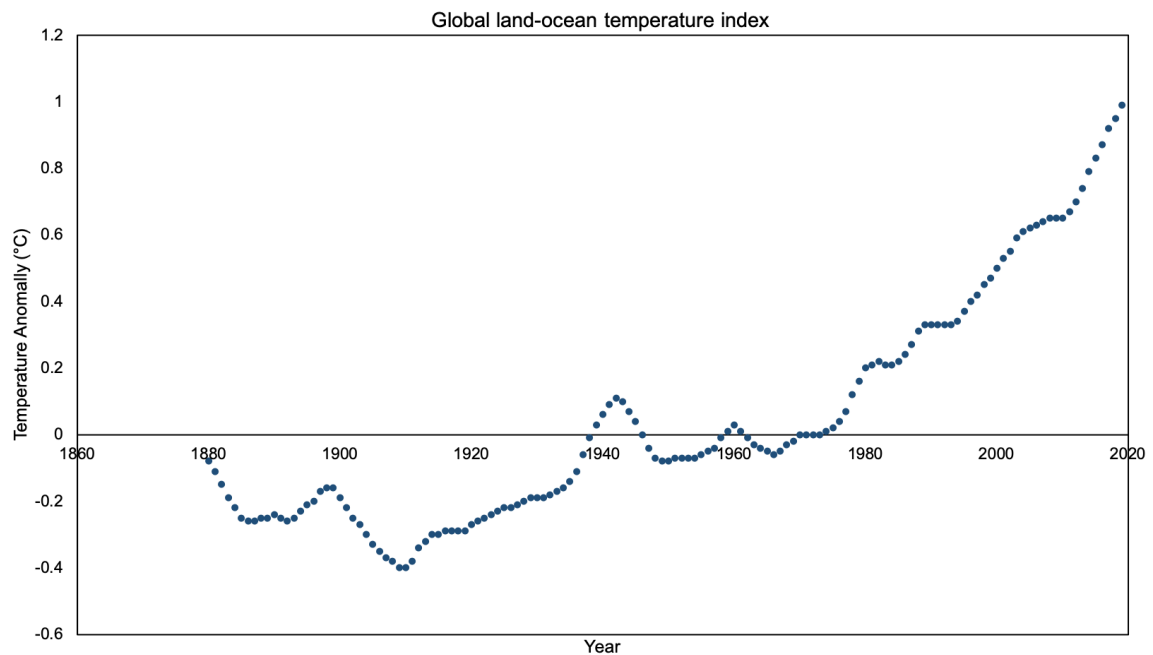


Figure 1. Temperature anomaly with respect to years (“Global Temperature | Vital Signs – Climate Change: Vital Signs of the Planet,” n.d.)

Since the mid 20<sup>th</sup> century, a significant rise is observed in the annual mean temperatures. This significant rise is attributed to the anthropogenic greenhouse gas emissions. Recently conducted investigations pointed out the substantial increase in CO<sub>2</sub>

levels. From preindustrial period till today CO<sub>2</sub> concentrations increased from 280 to 413 ppm and the measured CO<sub>2</sub> concentration of today is the highest of all the measured CO<sub>2</sub> concentrations for 650 thousand years (NASA, 2020). Scientists associated the increase in the surface temperatures of the late 21<sup>st</sup> century to the increase in the cumulative CO<sub>2</sub> emissions.

Among the greenhouse gases, CO<sub>2</sub> plays a key role (Ciais et al., 2013). Particularly, water vapor, methane, and nitrous oxides leave the atmosphere in 10 days, 10 years, and 100 years, respectively while 10% of the CO<sub>2</sub> emitted today, remains in the atmosphere for ten thousand years, past our lifetimes (Ciais et al., 2013). Within the last forty years, the cumulative CO<sub>2</sub> concentrations have reached 50% of the measured CO<sub>2</sub> concentrations and the greenhouse gas emissions have increased from 27 to 49 gigatons of CO<sub>2</sub> equivalent (Adger & Coauthors including Fischlin, 2007; Intergovernmental Panel on Climate Change, 2014). Fossil fuel combustion and the industrial processes contribute to the total greenhouse gas emissions by 78% (Adger & Coauthors including Fischlin, 2007; Intergovernmental Panel on Climate Change & Intergovernmental Panel on Climate Change, 2015). Our activities caused surface temperatures to increase by 1 °C from pre-industrial period till today. However, if no precautions are taken and the warming continues to rise at the same rate global warming would reach 1.5 °C in between 2030 and 2052 (Masson-Delmotte et al., 2018).

The Intergovernmental Panel on Climate Change (IPCC) points out that further increase in surface temperatures will increase the irreversible effects of climate change. As climate system changes, the magnitude of the risks rises. These risks include extinction of some species, food insecurity, difficulty in finding accessible surface and groundwaters in dry regions, increases in illnesses, and extreme weather events. However, it is foreseen that even if the greenhouse gas emissions are totally cut now, the impacts of climate change will be issued for centuries and reducing the greenhouse gas emissions will only reduce the magnitude of the impacts of climate change (Stocker et al., 2013).

Within the framework of the Paris Agreement, a target has been set to decrease the greenhouse gas emissions, by this way risks and the magnitude of the impacts of climate change can be reduced. According to Paris Agreement, to decrease the risks and impacts of climate change, considerable efforts will be put to limit the global temperature rise to 1.5 °C above the pre-industrial levels (United Nations, 2015). Thereby, several strategies have been

suggested to decrease CO<sub>2</sub> emissions: (i) developing energy systems that decrease energy intensity; (ii) decreasing carbon intensity by using low carbon fuels; (iii) developing renewable energy sources; and last (iv) developing technologies for CO<sub>2</sub> capture. These strategies will all contribute to stabilize and decrease greenhouse gas emissions. However, none of them will decrease the greenhouse gas emissions to zero by itself, all the mitigation measures should be improved and applied together.

## **2.2. Carbon Dioxide Capture and Storage Technologies**

IPCC estimates that CO<sub>2</sub> emissions can only be decreased by 80 to 90% if power plants use carbon dioxide capture and storage (CCS) technologies (IPCC, 2005a). CCS involves the separation of CO<sub>2</sub> from its source, and transportation to a location where the separated CO<sub>2</sub> can be stored without being emitted to the atmosphere. CCS can be used in large point sources such as heat and energy production facilities and then the CO<sub>2</sub> captured can be transferred either to storage areas or to industries that can re-use the captured CO<sub>2</sub> (IPCC, 2005b). There are three main CO<sub>2</sub> capture methods: (i) post-combustion, (ii) oxy-fuel combustion, and (iii) pre-combustion. It has been 80 years that CO<sub>2</sub> is captured from industrial process streams. However, the captured CO<sub>2</sub> was charged directly to atmosphere (Metz, Davidson, de Coninck, Loos, & Meyer, 2005).

In the post-combustion capture systems, CO<sub>2</sub> formed during fossil fuel combustion is captured and separated from the flue gas. Separated CO<sub>2</sub> is transferred to a storage area and the flue gas is emitted to the atmosphere. Combustion processes contribute significantly to the anthropogenic CO<sub>2</sub> emissions. Combustion chambers have been used for centuries owing to their low-cost and high efficiency. Cement kilns, iron and steel production plants, and power plants are some of the examples of the processes or the industries that use combustion systems. To decrease the anthropogenic CO<sub>2</sub> emissions, post-combustion CO<sub>2</sub> capture systems should be used in industries that have combustion processes. Post-combustion process comes a head of the other CO<sub>2</sub> capture processes since the existing facilities can be easily converted into facilities that can imply post-combustion CO<sub>2</sub> capture process for very low cost (Rochelle, 2009; Singh, Croiset, Douglas, & Douglas, 2003). Post-combustion systems can be used for any type of flue gas. However, as the combustion

products become more complicated, the process becomes more energy intensive and expensive.

In the oxy-fuel combustion systems, combustion process is conducted under oxygen environment at which  $\text{CO}_2$  and  $\text{H}_2\text{O}$  are produced as final products.

In pre-combustion capture systems, fuel reacts either with oxygen or air which produces carbon monoxide and hydrogen as a final product. Produced carbon monoxide is reacted in a catalytic reactor with steam to produce  $\text{CO}_2$  and hydrogen. Then the produced  $\text{CO}_2$  is separated by an absorption process which forms a hydrogen-rich fuel.

To separate  $\text{CO}_2$  from the  $\text{CO}_2$  capture systems different separation techniques are used.  $\text{CO}_2$  can be separated with sorbents/solvents, with membranes and by distillation. When  $\text{CO}_2$  is separated with sorbents or solvents, a liquid or a solid sorbent is used to capture  $\text{CO}_2$  from the flue gas. The main limitation of sorbents is the energy requirement of regeneration process. Moreover, the sorbents should be cost-effective, should be used for several cycles, and the residues should be environmentally friendly. Another method to separate  $\text{CO}_2$  from the flue gas is membrane separation. By the selective permittivity of the membrane,  $\text{CO}_2$  can be separated from the flue gas. However, reliability and the cost of membrane systems still limit the commercial use of these membranes in large scale systems. The last method to separate  $\text{CO}_2$  from the flue gas is distillation. In distillation method, by compressing, cooling and expanding the gas a liquid is obtained and  $\text{CO}_2$  is separated from this gas in a distillation column. This method is used commercially.

### **2.2.1. Absorption**

Absorption is the mostly preferred  $\text{CO}_2$  capture technology (Riemer & Ormerod, 1995). It has several advantages such as high capture efficiency, selectivity, low energy requirement, and low cost. However, it also has limitations. These limitations are: (i) the high energy demand; (ii) by-product formation (ammonia, and salts), and (iii) absorption of gasses that are produced at the end of the combustion process which decreases the absorption capacity of the solvent.

Flue gas combustion processes are conducted at atmospheric pressure and therefore,  $\text{CO}_2$  present in the flue gas is diluted and possesses a very low pressure. Moreover, flue gas does not only contain  $\text{CO}_2$ , but it also contains other gasses which makes the separation more



difficult and the use of a highly selective absorbent necessary. For instance, in natural gas combustion processes  $\text{NO}_x$ , and in coal combustion processes  $\text{NO}_x$  and  $\text{SO}_x$  are produced besides  $\text{CO}_2$ . These by-products also interact with the alkaline solvent which form heat stable salts and decrease the absorption capacity of the solvent. As the absorption capacity of the solvent decreases, the regeneration cycle and the cost increases. Therefore, it is necessary to remove other gasses ( $\text{NO}_x$  and  $\text{SO}_x$ ) prior to  $\text{CO}_2$  capture process. Last but not least, the heat of desorption should be low to decrease the energy consumption during the absorption process.

Among the various absorbents (amines, ammonia, aqueous solvents, blends, and ionic liquids) used, the most effective ones are the aqueous amine solutions (Kohl & Nielsen, 1997). It has been more than 50 years that a primary amine, monoethanolamine (MEA) is used for post combustion  $\text{CO}_2$  capture systems (Jones, 2011; S. Zhang et al., 2018). This primary amine, MEA has many advantages over other amine solutions such that it is cost-effective, highly reactive with  $\text{CO}_2$ , and has an easy synthesis procedure. However, it also has its own drawbacks. Regeneration process demands for high energy, it is highly corrosive, and has poor thermal stability besides its low  $\text{CO}_2$  absorption capacity (Aroonwilas & Veawab, 2004; Davidson, 2007; Dawodu & Meisen, 1994; Lepaumier, Picq, & Carrette, 2009; Olajire, 2010; A. B. Rao & Rubin, 2002; Van Der Zwaan & Smekens, 2009). When compared with MEA, ammonia ( $\text{NH}_3$ ) possesses a greater absorption capacity, and  $\text{NH}_3$  can remove  $\text{NO}_x$  and  $\text{SO}_x$  from the flue gas. However, being highly volatile and having a slow absorption rate,  $\text{NH}_3$  is expensive to be used in  $\text{CO}_2$  absorption processes.

Recently, some amines come to front with their high absorption capacities and rates, low heats of absorption and fast regeneration rates. These amines are 4-(dimethylamino)-2-butanol (DMAB), 4-((2-hydroxyethyl)(ethyl)amino)-2-butanol (HEEBAB), and 4-((2-hydroxyethyl)(methyl)amino)-2-butanol (HEMAB) (Singto et al., 2016) which were investigated for their  $\text{CO}_2$  absorption performances. Despite their high absorption capacities, and selectivity, higher corrosion resistances and cost-effective regeneration processes, they have low absorption rates (Aboudheir, Tontiwachwuthikul, & Idem, 2006; Y. E. Kim et al., 2013; Mandal & Bandyopadhyay, 2005; Sartori & Savage, 1983; Sherman, Ciftja, & Rochelle, 2016). By blending tertiary amines with secondary-tertiary amines a new class of absorbents with improved features are introduced. Secondary-tertiary amines with high reaction rates are blended with tertiary amines that possess high equilibrium capacities (J. H.

Choi et al., 2016; Dash, Samanta, & Bandyopadhyay, 2014; D. Fu, Wang, Mi, & Zhang, 2016; K. Fu et al., 2012; J. Gao et al., 2016; Hairul, Shariff, & Bustam, 2017; W. Luo, Guo, Zheng, Gao, & Chen, 2016; Shuangchen Ma et al., 2016; Nwaoha et al., 2016; Ramazani, Samsami, Jahanmiri, Van der Bruggen, & Mazinani, 2016; Shamiri et al., 2016; Svendsen, Hessen, & Mejdell, 2011; Vaidya & Kenig, 2008; X. Zhang et al., 2014; Z. Zhang, 2016).

Aqueous ammonia ( $\text{NH}_3$ ) is another absorbent that has been used in post-combustion  $\text{CO}_2$  capture processes (Guo et al., 2011). It is easily available, cost-effective, has high  $\text{CO}_2$  absorption capacity and can remove  $\text{NO}_x$  and  $\text{SO}_x$  (W. J. Choi, Min, Seo, Park, & Oh, 2009; Gouedard, Picq, Launay, & Carrette, 2012; Olajire, 2010; Pellegrini, Strube, & Manfrida, 2010; Puxty, Rowland, & Attalla, 2010; Yeh & Bai, 1999; B. Zhao, Su, Tao, Li, & Peng, 2012). However, due to ammonia slip, the use of aqueous ammonia in  $\text{CO}_2$  capture processes becomes limited.

Ionic liquids (ILs) come to front with their low vapor pressure, high thermal stability, high selectivity, and easy regeneration processes (Dai & Deng, 2016). Imidazolium based ionic liquids are used in  $\text{CO}_2$  capture processes. Inflammability, high selectivity, high reaction rates, chemical and thermal durability, and low cost make imidazolium based ionic liquids promising candidates for  $\text{CO}_2$  capture processes (Rogers, 2007; Sreenivasulu, Gayatri, Sreedhar, & Raghavan, 2015; Wappel, Gronald, Kalb, & Draxler, 2010). To enhance the absorption capacity of ionic liquids, they were blended with amines. However, these blends were not applicable to be used commercially due to the fact that they were expensive, and they had high viscosities. To decrease the costs, and to lower the viscosity, solutions of non-ionic surfactants and ionic liquids were investigated. It was observed that viscosity decreased, the cost was reduced, and the absorbent can be used after regeneration (A. B. Rao & Rubin, 2002). Despite the many advantages of ILs, the contradictory effects of absorbent concentration and viscosity on the absorption performance (absorption capacity and rate) limits the use of ILs at commercial scale (Z. Feng, Jing-Wen, Zheng, You-Ting, & Zhi-Bing, 2012; D. Fu, Zhang, & Mi, 2016; Y. Gao et al., 2013; Xue, Zhang, Han, Chen, & Mu, 2011).

Some solvents have been used commercially in post-combustion  $\text{CO}_2$  capture processes (Sreedhar, Nahar, Venugopal, & Srinivas, 2017). However, several limitations exist. Using solvents in  $\text{CO}_2$  capture processes demands for high energy due to energy intensive regeneration process, and degradation of the solvents results in corrosion which is

not environmentally friendly. To be used commercially, novel solvents should be developed which possess high absorption capacities and absorption rates, low heats of absorption/desorption, and low viscosities while being non-toxic, and easily regenerable.

In conclusion, from the perspective of absorbents, solvents that have easy synthesis procedures and easy regeneration processes; solvents that possess low viscosity, and faster mass transport properties; solvents that are chemically and thermally stable, and non-toxic should be developed to be used commercially. Researchers should give considerable attention to regeneration process which should be environmentally friendly, and cost-effective.

### **2.2.2. Membrane Contactors**

Amine-based absorption is the mostly used CO<sub>2</sub> capture technology. However, it is energy intensive, and faces corrosion and degradation issues. Membrane contactor is one of the promising alternatives to CO<sub>2</sub> absorption which was firstly used in 1980s (Qi & Cussler, 1985a). In a membrane contactor, a porous membrane separates liquid and gas phases. Without the dispersion of phases, these two phases (liquid and gas) flow at different sides of the membrane which prevents flooding and foaming. Mass transfer occurs at three steps. Firstly, diffusion occurs from bulk gas to gas-membrane interface, and then diffuses through the membrane pores to liquid-membrane interface, and transfers to the bulk liquid and lastly, physical or chemical absorption occurs (S. Zhao et al., 2016).

In a membrane contactor, flue gas passes through a selective membrane at which CO<sub>2</sub> is separated. CO<sub>2</sub> flows through a nonselective porous membrane and then, absorbed by a liquid absorbent. To separate CO<sub>2</sub> from the flue gas, a high CO<sub>2</sub> permeance and a high CO<sub>2</sub> to N<sub>2</sub> selectivity is necessary. By this way, the advantages of absorption (high selectivity) and membrane separation (compact structure) can be combined.

Membrane contactors have some advantages over absorption systems (Cui & Demontigny, 2013; Gabelman & Hwang, 1999; J. L. Li & Chen, 2005; A. Mansourizadeh & Ismail, 2009). Membrane contactors are easy to operate; their surface area per contactor volume is high; the flow rates of liquid and gas phases can be controlled independently and thereby, foaming and flooding can be prevented; independent of the flow rates of each phase, the membrane surface area is available to both phases; membrane contactors are compact so

that much more gas-liquid interfaces can be achieved; they are less energy intensive; cost-effective; and efficient (Demontigny, Tontiwachwuthikul, & Chakma, 2005; Drioli, Stankiewicz, & Macedonio, 2011; Karoor & Sirkar, 1993; J. L. Li & Chen, 2005; Qi & Cussler, 1985b). However, membranes face several challenges. These are: (i) membrane degradation; (ii) membrane fouling; and (iii) membrane wetting (Lu, Wang, Sun, Li, & Liu, 2005; Mosadegh-Sedghi, Rodrigue, Brisson, & Iliuta, 2014; Rangwala, 1996; H.-Y. Zhang, Wang, Liang, & Tay, 2008). For long-term use, membrane systems should be chemically and thermally stable since they can be degraded by the absorbent or the solvents (Barbe, Hogan, & Johnson, 2000; R. Wang, Li, Zhou, Liu, & Liang, 2004).

Absorbents, especially the ones with higher CO<sub>2</sub> absorption capacities, are found to be even more corrosive which can cause changes in the chemical structure, morphology, and properties of the membranes (Barbe et al., 2000; Kladkaew, Idem, Tontiwachwuthikul, & Saiwan, 2011; Saiwan, Supap, Idem, & Tontiwachwuthikul, 2011). Not only the absorbents or the chemical solvents, but also the degradation products of solvents can cause damages. Moreover, fine particles lower the performance of membrane contactors. Depositing on the surface and the pores of the membrane, fine particles plug the pores. This deposition that occurs on the surface and the pores of the membrane is irreversible causing mass transfer resistance to increase and membrane performance to decrease (Xia Wang et al., 2014; L. Zhang, Qu, Sha, Wang, & Yang, 2015). To achieve better separation efficiencies, flue gas has to be treated prior to membrane separation. Membrane wetting results in significant increases in mass transfer resistance which causes CO<sub>2</sub> absorption capacity to decrease (Kreulen, Smolders, Versteeg, & van Swaaij, 1993; Lu et al., 2005; Mosadegh-Sedghi et al., 2014; Rangwala, 1996; H.-Y. Zhang et al., 2008).

Membrane resistance is found to be dependent on the textural properties of the membrane, membrane hydrophobicity, surface roughness, surface tension of the absorbent, and operation conditions (J. L. Li & Chen, 2005; A. Mansourizadeh & Ismail, 2009; R. Wang, Zhang, Feron, & Liang, 2005). There are three different modes that membranes are operated: (i) non-wetted; (ii) partially wetted; and (iii) fully wetted (A. Mansourizadeh & Ismail, 2009; Y. Zhang & Wang, 2013b). Non-wetting mode is the mostly used mode in membrane contactors since a minimum diffusion is achieved (Boributh, Rongwong, Assabumrungrat, Laosiripojana, & Jiraratananon, 2012; Dindore, Brilman, Geuzebroek, & Versteeg, 2004; J. L. Li & Chen, 2005; A. Mansourizadeh & Ismail, 2009; Mavroudi, Kaldis,

& Sakellaropoulos, 2006). However, achieving a complete non-wetted mode is practically not possible. Solutions of absorbents can fill the membrane pores causing partial wetting. Moreover, in the long-term uses, membrane pores get wetted which increases mass transfer resistance (Malek, Li, & Teo, 1997; A. Mansourizadeh & Ismail, 2009; Mavroudi, Kaldis, & Sakellaropoulos, 2003; R. Wang et al., 2005; H.-Y. Zhang et al., 2008). In order to minimize membrane wetting hydrophobic membranes or composite membranes should be preferred, high surface tension liquids and absorbents that are less corrosive should be used, and operating conditions should be optimized (J. L. Li & Chen, 2005; Mosadegh-Sedghi et al., 2014). In the long-term uses, absorbent (absorbent operating conditions (Boributh, Assabumrungrat, Laosiripojana, & Jiraratananon, 2011; Boributh et al., 2012; Dindore et al., 2004; J.-G. Lu, Zheng, & Cheng, 2008; A Mansourizadeh, Ismail, & Matsuura, 2010; Rongwong, Jiraratananon, & Atchariyawut, 2009; R. Wang, Li, Zhou, et al., 2004; H.-Y. Zhang et al., 2008; Q.-S. Zheng, Yu, & Zhao, 2005), absorbent type (Bougie & Iliuta, 2010b, 2010a, 2011; Bougie, Lauzon-Gauthier, & Iliuta, 2009; S.-C. Chen, Lin, Chien, Wang, & Hsiao, 2011; Dindore et al., 2004; García-Payo, Izquierdo-Gil, & Fernández-Pineda, 2000; S.-H. Lin, Hsieh, Li, & Tung, 2009; S.-H. Lin, Tung, Chen, & Chang, 2009; J.-G. Lu et al., 2008; Ma'mun, Svendsen, Hoff, & Juliussen, 2007; Mosadegh-Sedghi, Brisson, Rodrigue, & Iliuta, 2012; Portugal, Sousa, Magalhães, & Mendes, 2009; Rangwala, 1996; R. Wang, Li, & Liang, 2004; S. Yan et al., 2007; H.-Y. Zhang et al., 2008) and absorbent concentration (J.-G. Lu et al., 2008; Rongwong et al., 2009; Yeon, Lee, Sea, Park, & Lee, 2005)) influence membrane wetting, significantly. Membrane wetting is affected by absorbent flow rate, and pressure, significantly. Several researchers reported that pore wetting was enhanced, when liquid flow rates were increased (Boributh et al., 2012; Mavroudi et al., 2006; H.-Y. Zhang et al., 2008). The higher flow rates cause liquid boundary to decrease and thereby, the resistance inside the membrane pores increases which results mass transfer resistance to increase. Additionally, operating pressure was observed to effect pore wetting, considerably (Boributh et al., 2011; J.-G. Lu et al., 2008; R. Wang, Li, & Liang, 2004; Q.-S. Zheng et al., 2005). Several researchers reported that when high absorbent pressures are applied, membrane wetting increases (Boributh et al., 2011; J.-G. Lu et al., 2008; Rongwong et al., 2009; R. Wang, Li, & Liang, 2004). The increase in liquid pressure cause transmembrane pressure to increase which therefore increases the pore wetness (J.-G. Lu et al., 2008). Absorbent properties (surface tension and viscosity) have considerable effects on membrane

wetting. For instance, as the surface tension increases, the tendency to observe membrane wetting decreases (Dindore et al., 2004). For CO<sub>2</sub> capture processes, aqueous amines are the mostly used absorbents. However, the tendency of wetting increases when single and mixed alkanolamine solutions are used (Dindore et al., 2004; Rangwala, 1996; Rongwong et al., 2009; R. Wang, Li, & Liang, 2004; H.-Y. Zhang et al., 2008). It was concluded that when the surface tension of the solution is low, it has a low contact angle with the membrane surface which causes the tendency of wetting to increase (Dindore et al., 2004; J. L. Li & Chen, 2005; S.-H. Lin, Chiang, Hsieh, Li, & Tung, 2008). Viscosity is another parameter that effects membrane wetting. Absorbents that have lower viscosities can flow into pores more easily (S.-H. Lin et al., 2008). For instance, when pure water is used as an absorbent, CO<sub>2</sub> flux stays constant whereas when aqueous amines are used flux decreases. Surface tension and viscosity influences membrane wetting, simultaneously. In order to minimize or eliminate membrane wetting, absorbents that lowers the tendency of wetting should be developed. Researchers worked on amino acid salts (Kumar, Hogendoorn, Feron, & Versteeg, 2002; J.-G. Lu, Ji, Zhang, & Chen, 2010; J.-G. Lu et al., 2008; Ma'mun et al., 2007; Portugal et al., 2009), potassium glycinate (S. Yan et al., 2007), mixed piperazine/amine absorbents (Bougie & Iliuta, 2010a, 2010b; Bougie et al., 2009; S.-C. Chen et al., 2011; S.-H. Lin, Hsieh, et al., 2009; S.-H. Lin, Tung, et al., 2009; Mosadegh-Sedghi et al., 2012), and mixed aqueous absorbent of MEA and triethanolamine (TEA) and obtained promising results. It was observed that with the increasing concentrations of amino acid salts, surface tension increases and thereby, breakthrough pressure increases (Kumar et al., 2002). In the case of potassium glycinate, the surface tension increases with increasing potassium glycinate concentration which decreases the tendency of wetting (S. Yan et al., 2007). Increasing piperazine/amine concentrations in a mixed absorbent increases absorbent viscosity which decreases the tendency of wetting (S.-H. Lin, Tung, et al., 2009). Studies showed that to decrease wetting tendency, significant effort has to be put on the surface tension and the viscosity of the absorbent. Several researches showed that absorbent concentration is another parameter that influences wetting tendency, significantly (Boributh et al., 2012; Franken, Nolten, Mulder, Bargeman, & Smolders, 1987; S.-H. Lin et al., 2008). However, the effect of absorbent concentration on its surface tension depends on its type. For instance, for absorbents that are formed of organic compounds, surface tension decreases with increasing organic compound concentration which increases the tendency of wetting

and therefore, increases the mass transfer resistance (Franken et al., 1987; Rongwong et al., 2009). Membrane surface energy is related with the surface hydrophobicity and thus the contact angle between the liquid drop and the membrane surface. For contact angles greater than 90 °, tendency of wetting decreases. However, for contact angles lower than 90 °, tendency of wetting increases. Thus, a membrane with a lower surface energy would have a lower tendency of wetting while a membrane with a higher surface energy would have a higher tendency of wetting. Pore size has a key role in membrane wetting tendency. Several studies showed that as pore size increases, the critical entry pressure also increases which therefore enhances the tendency of wetting (Keshavarz, Fathikalajahi, & Ayatollahi, 2008; Malek et al., 1997; Amir Mansourizadeh, 2012; H.-Y. Zhang et al., 2008). Membrane wettability depends on both the absorbent and the membrane. Using absorbents that have high surface tensions, increases the contact angle between the liquid drop and the membrane or using a membrane with a low surface energy, and using a membrane with a small pore size minimize the tendency of wetting and therefore, the mass transfer resistance decreases.

In conclusion, membrane degradation, membrane fouling and membrane wetting are the main challenges issued in membrane contactors. To overcome these limitations the following has to be taken into account. In order to increase the contact angle greater than 90 °, either hydrophobic membranes have to be used or hydrophobic modifications have to be made. A composite membrane formed of dense layers should be used, liquid absorbents with high surface tension should be preferred, in order to avoid membrane degradation, significant effort has to be given to absorbent and membrane compatibility and operation conditions should be optimized.

Another important parameter that influences absorption capacity is membranes. Membranes behave as barriers which are not selective to CO<sub>2</sub>. Most of the membrane contactors use hollow fibers. The outside layer of these membranes is selective. To achieve high performances from membrane contactors, membranes with the following properties should be used: (i) thermally stable; (ii) chemically stable; (iii) highly hydrophobic; and (iv) highly porous. Using a thermally and chemically stable membrane would minimize the probability of membrane degradation, using a highly hydrophobic membrane would minimize the tendency of membrane wetting, and lastly, using a highly porous membrane would decrease the mass transfer resistance. Different polymers are used as membrane materials for hydrophobic membranes. For instance, polypropylene (PP) (deMontigny,

Tontiwachwuthikul, & Chakma, 2006; Khaisri, deMontigny, Tontiwachwuthikul, & Jiraratananon, 2009; S.-H. Lin, Hsieh, et al., 2009; S.-H. Lin, Tung, et al., 2009; Mavroudi et al., 2006; H.-Y. Zhang et al., 2008), polyvinylidene fluoride (PVDF) (Atchariyawut, Feng, Wang, Jiraratananon, & Liang, 2006; C. Feng, Wang, Zhang, & Shi, 2011; Khaisri et al., 2009; S.-H. Lin, Hsieh, et al., 2009; A Mansourizadeh & Ismail, 2010; A Mansourizadeh et al., 2010; Amir Mansourizadeh & Ismail, 2011; H. H. Park, Deshwal, Kim, & Lee, 2008; A. Xu, Yang, Young, deMontigny, & Tontiwachwuthikul, 2008; H.-Y. Zhang et al., 2008), polytetrafluoroethylene (PTFE) (Chabanon, Roizard, & Favre, 2011; S.-C. Chen, Lin, Chien, & Hsu, 2010; deMontigny et al., 2006; Falk-Pedersen, Grønvold, Nøkleby, Bjerre, & Svendsen, 2005; Hoff, Juliussen, Falk-Pedersen, & Svendsen, 2004; Khaisri et al., 2009), and polyethylene (PE) (Mosadegh-Sedghi et al., 2012; Sedghi, Brisson, Rodrigue, & Iliuta, 2011). Membranes constructed of different materials show different CO<sub>2</sub> absorption performances which is attributed to different wetting tendencies of the membranes (Khaisri et al., 2009). For instance, it is found that PTFE membranes have better absorption performances and lower wetting tendencies than PP membranes (Chabanon et al., 2011; deMontigny et al., 2006). Thermal stabilities of these polymers have critical role in the absorption studies since desorption studies are conducted in between 100 and 150 °C. PTFE and PEEK are found to be promising candidates to be used in membrane contactors due to their high dimensional stability. Moreover, several factors are found to affect membrane performance, considerably. For instance, additives can be used to decrease the pore size, and to enhance hydrophobicity; polymer concentrations can be increased to have smaller pore size; and coagulant concentrations can be set accordingly to construct membranes that do not have an inner skin to decrease the mass transfer resistance. Liquid absorbents cause wetting in the membranes. Therefore, dense skin layer composite membranes are used. By this way, wetting tendency decreases and the chemical resistance of the membrane increases (Kreulen et al., 1993). However, to minimize the mass transfer resistance the dense layer should be very thin; the dense layer should be chemically and thermally stable; and the dense layer has to possess a high CO<sub>2</sub> permeability. Non-porous membrane contactors are investigated for their CO<sub>2</sub> absorption performance (Al-saffar, Ozturk, & Hughes, 1997; Heile, Rosenberger, Parker, Jefferson, & McAdam, 2014; McLeod, Buzatu, Autin, Jefferson, & McAdam, 2015; Scholes, Qader, Stevens, & Kentish, 2014). These membranes either of silicone rubber or polydimethylsiloxane (PDMS) are found to be promising candidates that minimize



membrane wetting. However, their high mass transfer resistances cause significant decrease in their CO<sub>2</sub> absorption capacities (Scholes et al., 2014).

Several researchers worked on nanoparticle incorporation to decrease mass transfer resistance and enhance membrane hydrophobicity. By adding fluorinated SiO<sub>2</sub> nanoparticles and surface hydrophobization, hydrophobicity was enhanced and absorption flux was increased (Y. Zhang & Wang, 2013a, 2014). Moreover, another researcher added clay particles to PVDF which showed promising results. A mixed matrix membrane was obtained with lower wetting tendency and higher CO<sub>2</sub> absorption performance (Rezaei, Ismail, Bakeri, Hashemifard, & Matsuura, 2015; Rezaei, Ismail, Hashemifard, Bakeri, & Matsuura, 2014).

In conclusion, membrane contactors come to front in CO<sub>2</sub> capture studies by combining the advantages of absorption and membrane separation: Membrane contactors are highly selective and compact. However, researchers have to put significant effort to develop membrane contractors to be commercially used. Membrane wetting is one of the crucial challenges that has to be worked on since it affects CO<sub>2</sub> absorption capacity and performance, considerably. Moreover, some more effort has to be put on solvents, especially green solvents should be developed. Lastly, in order to use membrane contactors at industrial scale, robust, chemically and thermally stable membrane materials should be developed.

### **2.2.3. Adsorption**

Even though amine-based absorption is the most commonly used CO<sub>2</sub> capture technology, it has several drawbacks. Particularly, solvents are corrosive, and the regeneration processes are highly energy intensive (D'Alessandro, Smit, & Long, 2010; Haszeldine, 2009; Leci, 1996). Therefore, studies were conducted to find a cost-effective and less energy intensive alternative to amine-based CO<sub>2</sub> capture process.

In 1990s adsorption process come to front as a promising alternative to amine based solvents (Chue, Kim, Yoo, Cho, & Yang, 1995; Ishibashi et al., 1996; Kikkinides, Yang, & Cho, 1993). For instance, an adsorption process can be retrofitted to any facility easily; adsorbents can be designed to work at a variety of pressures and temperatures; adsorption process is so environmentally friendly that by-product formation is minimized while amine-based solvents form toxic by-products; adsorption process is cost-effective; and the

regeneration step of adsorption process is less energy intensive since the heat capacity of an adsorbent is lower than the heat capacity of an amine based solvent.

Adsorption is the adhesion of atoms, ions or molecules to a surface (Lowell, Shields, Thomas, & Thommes, 2004a). Adsorbent is the material that the molecules are attached on while adsorbate is the atoms, ions or molecules that attach to a surface. Absorption and adsorption differ from each other since only the surface of the adsorbent is involved. Chemical and physical adsorption differ from each other by the type of bonding involved during adsorption. For instance, if adsorption occurs physically, van der Waals forces are involved. However, if adsorption occurs chemically, covalent bonds are involved.

From 1990s till today, researchers worked on adsorbents to increase their adsorption capacity, and selectivity. Theoretical studies show that an adsorbent with a CO<sub>2</sub> adsorption capacity equal to and/or greater than 3 mmol/g would decrease the energy demand of post-combustion CO<sub>2</sub> capture systems by 30 to 50% (Gray, Champagne, Fauth, Baltrus, & Pennline, 2008). However, it is also crucial to take into account that the flue gas contains impurities that would decrease the CO<sub>2</sub> adsorption capacity of the adsorbent.

To achieve the targets set by US Department of Energy and European Union SET plan, researchers focused on alternative technologies that are cost-effective, and less energy intensive. The National Energy Laboratory in the U.S. set some targets for the adsorbent materials. The targets are as follows:

- i) The energy requirement of an adsorbent for post-combustion carbon capture process should be 30 to 50% lower than the energy requirement of an amine-based adsorbent,
- ii) Under flue gas conditions, the adsorbent should have a minimum CO<sub>2</sub> adsorption capacity of 3.0. mmol/g,
- iii) The temperature to adsorb and desorb should be within a narrow temperature range (40 to 110 °C) and the adsorbent should be able to adsorb and desorb at atmospheric pressure,
- iv) The adsorbent should work in the presence of water vapor,
- v) The adsorbent should be chemically and thermally stable,
- vi) The adsorbent should have a high adsorption capacity even after regeneration, and

- vii) The adsorbent should maintain its high adsorption capacity even after several adsorption and regeneration cycles.

CO<sub>2</sub> adsorption capacity, CO<sub>2</sub> selectivity, adsorption/desorption kinetics, chemical stability, mechanical strength, regeneration process and the cost of sorbent are crucial parameters for the commercial use of adsorbents. For instance, adsorption capacity defines the quantity of adsorbent that will be used and determines the volume of the adsorbent containers. An adsorbent with a high CO<sub>2</sub> adsorption capacity would require lower amounts of adsorbent and thus, the size of the container would be reduced which will decrease the capital cost of the overall process.

An adsorbent has to be highly selective towards CO<sub>2</sub>. The high or the low selectivity of an adsorbent influences the transportation and sequestration processes, thus effects the cost of the system.

The adsorption/desorption kinetics determines the cycle time of an adsorption process. An ideal adsorbent would have fast CO<sub>2</sub> adsorption/desorption kinetics which would decrease the amount of adsorbent necessary to capture CO<sub>2</sub> from a certain amount of flue gas.

An ideal adsorbent should be chemically stable towards flue gasses and flue gas contaminants. An ideal adsorbent should be stable microstructurally and morphologically. Even if, the adsorbent goes through several adsorption and regeneration cycles it should maintain its CO<sub>2</sub> adsorption capacity. Operating conditions (high flow rates) should not lower the CO<sub>2</sub> adsorption capacity of an ideal adsorbent.

An ideal adsorbent should possess a low heat of adsorption (the energy needed for regeneration) and should maintain its CO<sub>2</sub> adsorption capacity even after several absorption-regeneration cycles. By this way, regeneration costs can be reduced. Carbon based materials, zeolites, silica-based materials, polymer-based materials, clay-based materials, alkali metal carbonate-based materials, immobilized ionic liquid-based materials, MgO, CaO, and metal-organic frameworks (MOFs) are some of the materials used in CO<sub>2</sub> adsorption studies.

#### **2.2.3.1. Carbon-based materials**

Carbon based adsorbents come to front with their high BET surface area, high porosity, low cost, easiness to modify the pore structure and easy regeneration processes. However, they possess poor selectivity towards CO<sub>2</sub> and low CO<sub>2</sub> adsorption capacities at

temperatures above 273 K (Arenillas, Smith, Drage, & Snape, 2005). Researchers focused their studies on the influence of BET surface area on the CO<sub>2</sub> adsorption capacity of the adsorbents. However, they have changed their direction towards the effect of pore size and pore structure. Several researchers showed that pore size influences CO<sub>2</sub> adsorption capacity of carbon-based materials, considerably (Environ, Sevilla, & Fuertes, 2011; S.-Y. Lee & Park, 2013; Marco-Lozar, Kunowsky, Suárez-García, & Linares-Solano, 2014; Wickramaratne & Jaroniec, 2013). Researchers put significant effort to develop methods and/or synthesis strategies to increase the CO<sub>2</sub> adsorption capacities of carbon-based adsorbents.

One of these methods is to introduce nitrogen groups which can be done in several ways (Arenillas et al., 2005; Drage et al., 2007; Gray et al., 2004; H. Y. Huang, Yang, Chinn, & Munson, 2003; Maroto-Valer, Tang, & Zhang, 2005; Plaza, Pevida, Arenillas, Rubiera, & Pis, 2007; Przepiórski, Skrodzewicz, & Morawski, 2004). First one is the carbonization of nitrogen-rich precursors. Some of the investigated precursors are dicyandiamide (J. Wei et al., 2013), chitosan (Fan, Zhang, Zhang, Shu, & Shi, 2013), HNO<sub>3</sub> (Xiaoyu Ma, Cao, & Hu, 2013), porous polyimine (J. Wang et al., 2013), polypyrrole (Meng, Meng, Chen, & Jin, 2014; Sevilla, Valle-Vigón, & Fuertes, 2011; Juhyon Yu et al., 2014), and ionic liquids (Sethia & Sayari, 2014).

Another method to introduce amine groups to the surface of these materials is surface modification which can be done by: i) impregnation with amine based polymers (Franchi, Harlick, & Sayari, 2005; Xiaoliang Ma, Wang, & Song, 2009; Satyapal, Filburn, Trela, & Strange, 2001; Son, Choi, & Ahn, 2008; Xingrui Wang, Li, Liu, & Hou, 2011; M. B. Yue, Chun, Cao, Dong, & Zhu, 2006); and ii) grafting (Harlick & Sayari, 2007; Hiyoshi, Yogo, & Yashima, 2005; Knowles, Delaney, & Chaffee, 2006; Serna-Guerrero, Belmabkhout, & Sayari, 2010a). All these methods involve the dispersion of amine-functionalities in the pores of a mesoporous carbon-based material which increases the amount of CO<sub>2</sub> captured by these mesoporous carbon-based materials. Among the above-mentioned surface modifications, grafting provides the highest stability to carbon-based materials even after the regeneration process.

Fluorination (B.-C. Bai, Kim, Im, Jung, & Lee, 2011), oxidation (Plaza et al., 2013), metal doping and metal loading are alternative methods that can be used to modify the surface of carbon-based materials. Fluorination method is reported to be a cost-effective,

easy, and efficient method that increases the CO<sub>2</sub> adsorption capacity. The increase in the CO<sub>2</sub> adsorption capacity is attributed to the interaction of the CO<sub>2</sub> molecules with oxygen functional groups (B.-C. Bai et al., 2011).

Some of the studies conducted in literature shows that increasing the oxygen content increases the CO<sub>2</sub> adsorption capacity of these carbon-based materials (Plaza et al., 2013).

Moreover, several studies investigated the effect of metal doping and metal loading on carbon-based materials. CuO (B.-J. Kim, Cho, & Park, 2010), and NiO (Jang & Park, 2012) are several examples of the metals doped/loaded.

Lastly, synthesis of hybrid composites can be an alternative way to enhance the CO<sub>2</sub> adsorption capacity and the performance of the carbon-based materials. The reported hybrid materials are: i) carbon/carbon; ii) carbon/carbon nitride (Y. Kong, Jin, & Qiu, 2013); and iii) carbon/MOF (Anbia & Hoseini, 2012).

#### **2.2.3.2. Graphite/graphene-based materials**

Graphite/graphene-based materials are low-cost materials which possess high specific surface areas. The low-cost and the high BET surface areas of these materials draw the attention of researchers and several researchers investigated the CO<sub>2</sub> adsorption capacity and CO<sub>2</sub> adsorption performance of these materials.

Prior to CO<sub>2</sub> adsorption studies, researchers exfoliated, functionalized, and synthesized the hybrids of graphite/graphene-based materials and then tested their respective CO<sub>2</sub> adsorption performances.

Graphene nanoplates prepared by exfoliation method achieve a high CO<sub>2</sub> adsorption capacity at 25 °C and 30 bar. This high CO<sub>2</sub> adsorption capacity is attributed to the enlarged inter-layer spacing and increased void volume (Meng & Park, 2012).

Despite its low cost, the low BET surface area and the low CO<sub>2</sub> adsorption capacity limit the use of graphite in CO<sub>2</sub> adsorption studies. In order to increase the CO<sub>2</sub> adsorption capacity of graphite, its surface was modified with 3-aminopropyl-triethoxysilane (APTS). The CO<sub>2</sub> adsorption capacity of graphite was still low (0.074 mmol/g) while the CO<sub>2</sub> adsorption capacity of graphene oxide increased, significantly (S.-M. Hong, Kim, & Lee, 2013).

Synthesizing graphene-inorganic hybrid materials is a promising alternative to enhance the CO<sub>2</sub> adsorption capacity (Yanwu Zhu et al., 2010). Several studies showed that

incorporation of nanoparticles in between graphene sheets enhanced the CO<sub>2</sub> adsorption capacity of graphene (Alhwaige, Agag, Ishida, & Qutubuddin, 2013; Mishra & Ramaprabhu, 2012; S. Yang et al., 2013). The enhanced CO<sub>2</sub> adsorption capacity is attributed to the nanoparticle incorporation which avoided graphene sheets to aggregate (Yanwu Zhu et al., 2010).

### **2.2.3.3. Zeolites**

Zeolites adsorb CO<sub>2</sub> molecules either by ion-dipole interaction or bi-coordination of carbonate species (Qiang Wang, Luo, Zhong, & Borgna, 2011). Even though zeolites possess high BET surface areas, and pore volumes, they show low CO<sub>2</sub> adsorption capacities at high temperatures (200 °C). There have been several zeolites investigated for their CO<sub>2</sub> adsorption performances (Araki, Kiyohara, Tanaka, & Miyake, 2012; Bezerra, Oliveira, Vieira, Cavalcante, & Azevedo, 2011; Bonelli, Onida, Fubini, Areán, & Garrone, 2000; Díaz, Muñoz, Vega, & Ordóñez, 2008; Hernández-Huesca, Díaz, & Aguilar-Armenta, 1999; P. Li & Handan Tezel, 2007; Z. Liang, Marshall, & Chaffee, 2009; Merel, Clausse, & Meunier, 2008; Pires, de Carvalho, Ribeiro, & Derouane, 1993; Su & Lu, 2012; Wirawan & Creaser, 2006; Xiao et al., 2008; J. Zhang, Singh, & Webley, 2008; Zukal et al., 2010). Several researchers showed that by applying cation exchange, CO<sub>2</sub> adsorption capacity was increased, significantly (Arévalo-Hidalgo, Almodóvar-Arbelo, & Hernández-Maldonado, 2011; T.-H. Bae et al., 2013; S.-H. Hong, Jang, Cho, & Ahn, 2014; K.-M. Lee, Lim, Park, & Jo, 2012; Lozinska et al., 2012; Ridha, Yang, & Webley, 2009; Walton, Abney, & Douglas LeVan, 2006).

Researchers figured out that modifying the surfaces of zeolites with amine groups enhanced the CO<sub>2</sub> adsorption capacity of these materials. It was observed that modifying the surfaces of zeolites by impregnation method increased the CO<sub>2</sub> adsorption capacity of several zeolites (Jadhav et al., 2007; Jing, Wei, Wang, & Yu, 2014; L.-Y. Lin, Kuo, & Bai, 2011; Su, Lu, Kuo, & Zeng, 2010). This enhancement in the adsorption capacities is attributed to the higher amount of nitrogen atoms present in the alkyl chains. As the temperature rises above 100 °C, the CO<sub>2</sub> adsorption capacities of zeolites decrease, significantly. To overcome this limitation, zeolites were grafted with aminosilanes (K. K. Han et al., 2012; Sanz, Calleja, Arencibia, & Sanz-Pérez, 2012; Serna-Guerrero et al., 2010a; Serna-Guerrero, Belmabkhout, & Sayari, 2010b). It was concluded that the distribution of amines through the pore channels

has a key role in enhancing the CO<sub>2</sub> adsorption capacity (Sanz et al., 2012). Moreover, moisture is found to be a factor that lower the CO<sub>2</sub> adsorption capacity of zeolites. Several researchers reported that water competes with CO<sub>2</sub> for the adsorption sites which results in a decreased CO<sub>2</sub> adsorption capacity (Brandani & Ruthven, 2004; Gallei & Stumpf, 1976; Jänchen, Möhlmann, & Stach, 2007; K.-M. Lee, Lim, & Jo, 2012; Rege & Yang, 2001).

#### **2.2.3.4.Silica-based materials**

Silica based materials possess high BET surface areas and pore volumes, and high chemical stability which make these materials promising support materials in CO<sub>2</sub> capture studies (S. Bai, Liu, Gao, Yang, & Li, 2012; Y. Du et al., 2013; Fauth et al., 2012; Goeppert et al., 2014; Ko, Lee, Oh, & Choi, 2013; Leal, Bolívar, Ovalles, García, & Espidel, 1995; J.-L. Liu & Lin, 2013; D. Wang, Sentorun-Shalaby, Ma, & Song, 2011; K. Wang et al., 2012; Jianguo Yu, Le, & Cheng, 2012; H. Zhang, Goeppert, Czaun, Prakash, & Olah, 2014). To enhance the CO<sub>2</sub> adsorption capacity, surface of the silica-based materials is functionalized with amines. Studies showed that functionalizing the surface of silica-based materials with amine or loading them with amine enhanced their CO<sub>2</sub> adsorption capacity (S. Bai et al., 2012; Y. Du et al., 2013; Goeppert et al., 2014; Ko et al., 2013; J.-L. Liu & Lin, 2013; Jianguo Yu et al., 2012).

Thermal stability is a material property that limits the commercial use of any material. In the case of CO<sub>2</sub> adsorption studies, a material that is thermally stable at temperatures above 100 °C is necessary. Several amine functionalized silica-based materials were investigated for their CO<sub>2</sub> adsorption performances above 100 °C and researchers developed strategies to improve their thermal stability (Jiao, Cao, Xia, & Zhao, 2016). Impregnation with amines enhanced the thermal stability of silicas and even after several adsorption-regeneration cycles, amine functionalized silicas were found to be chemically and thermally stable (W. Zhao, Zhang, Li, & Cai, 2013). Grafting is used as an alternative method to impregnation method for enhancing thermal stability. However, not all the grafted silicas show high CO<sub>2</sub> adsorption capacities (Leal et al., 1995).

### 2.2.3.5. Polymer-based materials

Porous polymers can be easily modified, they are light in weight, and they are chemically and thermally stable and cost-effective. Moreover, porous polymers show high CO<sub>2</sub> adsorption performances and selectivity. These properties make porous polymers come to front in adsorption studies (D'Alessandro et al., 2010; Dawson, Stöckel, Holst, Adams, & Cooper, 2011; Liebl & Senker, 2013).

Several polymers have been investigated for their CO<sub>2</sub> adsorption performances (Ben et al., 2012, 2011; X. Chen, Qiao, Du, Zhou, & Yang, 2013; Dawson, Adams, & Cooper, 2011; N. Du et al., 2011; H. J. Jeon et al., 2012; Kaliva, Armatas, & Vamvakaki, 2012; H. Lim, Cha, & Chang, 2012; W. Lu, Sculley, Yuan, Krishna, & Zhou, 2013; Y. Luo, Li, Liang, & Tan, 2011; Y. Luo, Li, Wang, Wu, & Tan, 2012; Martín et al., 2011; Rabbani & El-Kaderi, 2011; K. V. Rao, Mohapatra, Kulkarni, Maji, & George, 2011; Ritter, Senkovska, Kaskel, & Weber, 2011; Wilke & Weber, 2011; Xie & Suh, 2013; Yi Zhao, Shen, Bai, Hao, & Dong, 2012; X. Zhu et al., 2014). For instance, melamine-formaldehyde. It was observed that presence of porosity was necessary for this polymer to efficiently capture CO<sub>2</sub> (Wilke & Weber, 2011).

Hyper-crosslinked polymers were also investigated for their CO<sub>2</sub> adsorption performances. Their high surface areas, chemical stabilities, large-scale and low-cost productions, and high CO<sub>2</sub> adsorption capacities at 1 atm make these materials promising candidates for CO<sub>2</sub> adsorption studies (J.-H. Ahn et al., 2006; Germain, Svec, & Fréchet, 2008; Y. Luo et al., 2012; Martín et al., 2011).

Conjugated microporous polymers show promising CO<sub>2</sub> adsorption capacities which may be attributed to their high flexibility in structural modifications, tunable and high porosities, microporous pore structures, and high isosteric heats of adsorption (X. Chen et al., 2013; Dawson, Adams, et al., 2011; Xie & Suh, 2013).

Polymers with porous aromatic frameworks come to front with their very high surface areas, high stabilities in the presence of water, high isosteric heats of adsorption, high thermal stabilities, and high CO<sub>2</sub> selectivity towards CO<sub>2</sub>/N<sub>2</sub> and CO<sub>2</sub>/CH<sub>4</sub>. In addition to all these promising features, these porous aromatic frameworks show high CO<sub>2</sub> uptake capacities at room temperatures (Ben et al., 2012, 2011; Wenliang Li, Shi, & Zhang, 2014).

In conclusion, polymer-based materials show promising results in CO<sub>2</sub> adsorption studies owing to their high flexibility in structural modifications and high porosity. However,



further research has to be conducted to improve the stability of these materials after several cycles of adsorption and desorption.

#### **2.2.3.6. Clay-based materials**

Clay-based materials are low-cost, chemically and thermally stable and abundant materials (Swartzen-Allen & Matijevic, 1974). Two types of clays, montmorillonite and bentonite, take particular attention of researchers in CO<sub>2</sub> adsorption studies (Azzouz et al., 2013; C. Chen, Park, & Ahn, 2013; Gil, Vicente, & Korili, 2005; Leliveld, Ros, van Dillen, Geus, & Koningsberger, 1999; Roth, Agarwal, & Gupta, 2013; Stevens et al., 2013; Weilong Wang et al., 2013).

In order to be used in CO<sub>2</sub> adsorption studies, researchers modified bentonites and montmorillonites with amines since the non-modified ones show low CO<sub>2</sub> adsorption capacities. However, when modified, these materials show high chemical and thermal stabilities with enhanced CO<sub>2</sub> adsorption capacities.

#### **2.2.3.7. Alkali metal carbonate-based materials**

Alkali metal carbonate based materials (K<sub>2</sub>CO<sub>3</sub> and Na<sub>2</sub>CO<sub>3</sub>) have been used in CO<sub>2</sub> adsorption studies which possess high CO<sub>2</sub> uptake capacities (S. C. Lee et al., 2006; Y. Liang, Harrison, Gupta, Green, & McMichael, 2004; Y. Seo, Jo, Ryu, & Yi, 2007; C. Zhao, Chen, & Zhao, 2010a). However, these materials possess low durability, and slow reaction rates. Moreover, the adsorption and the regeneration processes can be conducted within a very limited temperature range (J. B. Lee et al., 2008; Y. Liang et al., 2004; C.-K. Yi et al., 2006; C. Zhao, Chen, & Zhao, 2010b).

To fasten the carbonation reaction rate, these alkali metal carbonate-based materials are loaded on a support material (Derevshikov, Veselovskaya, Kardash, Trubitsyn, & Okunev, 2014; W. Dong, Chen, & Wu, 2014; Harrison, 2005; S. C. Lee et al., 2009; Y. Liang et al., 2004; Sharonov, Okunev, & Aristov, 2004; Ye Wu et al., 2013; C.-K. Yi, Jo, Seo, Lee, & Ryu, 2007). Studies show that loading alkali metal carbonate-based materials on support materials improve their CO<sub>2</sub> adsorption capacities. However, loading these materials on support materials increases the regeneration temperatures which later on causes a significant decrease in the CO<sub>2</sub> adsorption capacities.

In conclusion, the commercial use of alkali metal carbonate-based materials is limited with the low durability, slow carbonation reaction rates and limited reaction temperatures of alkali metal carbonate-based materials.

#### **2.2.3.8. Immobilized ionic liquid-based materials**

Easy tunability, high CO<sub>2</sub> solubility, low volatility and high thermal stability of immobilized ionic liquid based materials (IL based materials) attract the attention of various researchers (Bara et al., 2009; Blanchard, Hancu, Beckman, & Brennecke, 1999; Hasib-ur-Rahman, Siaj, & Larachi, 2010; Jie Ren, Wu, & Li, 2012; Wappel et al., 2010). However, the hyper viscosity of IL based materials causes these materials to possess low sorption capacities.

Even if less viscous IL based materials are used, the increase in sorption capacities is not sufficient enough to be used in commercial applications (Blanchard et al., 1999; Blasig et al., 2007; Goodrich et al., 2011; Gutowski & Maginn, 2008; Tang, Sun, Tang, Radosz, & Shen, 2005; H. Yu, Wu, Jiang, Zhou, & Zhang, 2009; Qichao Zhao, Wajert, & Anderson, 2010). In order to overcome the above mentioned limitations and enhance the CO<sub>2</sub> adsorption capacities, IL based materials were: i) loaded on a support material (metal-organic frameworks, nanoporous polymers); ii) functionalized with pyridine containing-anion; and iii) synthesized as polymers (Bara et al., 2008; Y. Chen, Hu, Gupta, & Jiang, 2011; Eddaoudi et al., 2002; K. M. Gupta, Chen, Hu, & Jiang, 2012; Hasib-ur-Rahman et al., 2010; Kato, Tsujita, Yoshimizu, Kinoshita, & Higgins, 1997; X. Luo et al., 2014; Mogri & Paul, 2001; Privalova et al., 2013; Supasitmongkol & Styring, 2010; Tang, Sun, et al., 2005; Tang, Tang, Sun, Radosz, & Shen, 2005; Xianfeng Wang, Akhmedov, Duan, Luebke, & Li, 2013).

#### **2.2.3.9. MgO based materials**

Metal oxides have abundant basic sites at their surface which make them promising candidates in CO<sub>2</sub> adsorption studies. When MgO and CaO based sorbents are compared, it is found that MgO based sorbents can be regenerated at lower temperatures, and thus their energy needs for the regeneration process is lower than CaO based sorbents (S. Choi, Drese, & Jones, 2009b; B. Feng, An, & Tan, 2007; Philipp & Fujimoto, 1992). However, the very long regeneration processes or the necessity to conduct the regeneration processes at high

temperatures limit the use of MgO based sorbents, commercially (Bhagiyalakshmi, Lee, & Jang, 2010). In addition to the energy intensive regeneration processes, MgO based sorbents possess relatively low CO<sub>2</sub> adsorption capacities (Bhagiyalakshmi et al., 2010). To enhance the CO<sub>2</sub> sorption capacities, particle size was reduced, porous MgO based materials were synthesized, and MgO was dispersed on a porous material (Bhagiyalakshmi, Hemalatha, Ganesh, Mei, & Jang, 2011; Bian, Baltrusaitis, Galhotra, & Grassian, 2010; K. K. Han, Zhou, Lin, & Zhu, 2013; H. Jeon et al., 2012; T. K. Kim, Lee, Yuh, Kwak, & Moon, 2014; Lei Li et al., 2010; Y. Y. Li et al., 2013; W.-J. Liu, Jiang, Tian, Ding, & Yu, 2013; Ruminski, Jeon, & Urban, 2011; She et al., 2011).

#### **2.2.3.10. CaO based materials**

CaO based materials are cost-effective materials. The high theoretical CO<sub>2</sub> sorption capacities of CaO based materials make them promising candidates in CO<sub>2</sub> sorption studies (H. Gupta & Fan, 2002; Salvador, Lu, Anthony, & Abanades, 2003). However, durability of these sorbents suffer due to the sintering process at which the carbonation process is highly exothermic and the volume of CaO decreases while the volume of CaCO<sub>3</sub> increases (J Carlos Abanades & Alvarez, 2003; J Carlos Abanades, Anthony, Lu, Salvador, & Alvarez, 2004; Juan Carlos Abanades, 2002; Barker, 1973; Salvador et al., 2003; P Sun, Grace, Lim, & Anthony, 2007; Ping Sun, Grace, Lim, & Anthony, 2007). Therefore, to improve the durability of CaO based sorbents, researchers changed the morphology and the microstructure, modified the surface, synthesized mixed oxides, and investigated the effect of SO<sub>2</sub>. A study shows that synthesizing a CaO based sorbent as CaO/Ca<sub>12</sub>Al<sub>14</sub>O<sub>33</sub> hollow nanospheres with relatively high surface area, narrow pore size distribution, and with inert Ca<sub>12</sub>Al<sub>14</sub>O<sub>33</sub> binders enhances the CO<sub>2</sub> adsorption capacity and the life cycle performance of the sorbent (F.-Q. Liu, Li, Liu, & Li, 2013).

Introducing inert materials into CaO particles is found to be the most effective and the feasible way to improve the life cycle performance of CaO based sorbents (B. Feng, Liu, Li, & An, 2006; Gruene, Belova, Yegulalp, Farrauto, & Castaldi, 2011; C.-H. Huang, Chang, Yu, Chiang, & Wang, 2010; Kierzkowska, Poulikakos, Broda, & Müller, 2013; Liyu Li, King, Nie, & Howard, 2009; Yingjie Li, Zhao, Chen, Duan, & Chen, 2010; Z. Li, Cai, Huang, & Han, 2005; W. Liu, Low, Feng, Wang, & Diniz da Costa, 2010; C. Luo et al., 2010; Manovic & Anthony, 2010; Martavaltzi & Lemonidou, 2008; S. F. Wu & Zhu, 2010; K. B.

Yi, Ko, Park, & Kim, 2009; C.-T. Yu & Chen, 2014; M. Zhao et al., 2014; Z. Zhou, Qi, Xie, Cheng, & Yuan, 2012). The inert materials act as supports and thereby, the sorbent possesses improved resistance properties and thereby, life cycle performance of the sorbent increases. Reactivation of the degraded CaO based sorbents is crucial for the commercial use of these sorbents (Barker, 1973; Iyer, Gupta, Sakadjian, & Fan, 2004; Phalak, Deshpande, & Fan, 2012; P Sun et al., 2007; Valverde, Sanchez-Jimenez, & Perez-Maqueda, 2014). It was reported by several researchers that by steam hydration, degraded CaO based sorbents can be reactivated (Coppola, Salatino, Montagnaro, & Scala, 2014; Kuramoto et al., 2003; Y Wu, Blamey, Anthony, & Fennell, 2010; Yin et al., 2012; F.-C. Yu, Phalak, Sun, & Fan, 2012).

In conclusion, for the commercial use of CaO based sorbents the life-cycle performance and the degradation problem of the CaO based sorbents should be solved. Increasing the surface area of the sorbent, having high and accessible porosity would enhance the CO<sub>2</sub> adsorption performance of the sorbents while introducing inert particles into CaO based particles would improve the life cycle performance of the sorbent, considerably.

#### **2.2.3.11. Metal-Organic Frameworks (MOFs)**

MOFs are highly porous crystalline materials that are formed of an organic and an inorganic part. MOFs come to front in gas storage and separation studies with their high BET surface areas, and high and tunable porosities (Furukawa et al., 2010; Mueller et al., 2006). Their high porosities and high surface areas provide these materials to achieve very high CO<sub>2</sub> adsorption capacities at 77 K and high pressures. For instance, at 50 bar and 30 °C CO<sub>2</sub> adsorption capacities of MOF-177 and MIL-101 were found to be 33.5 mmol/g, and 40 mmol/g, respectively (Llewellyn et al., 2008; Millward & Yaghi, 2005c). However, at low pressures the CO<sub>2</sub> adsorption capacity of MOFs decreases, drastically (Demessence, D'Alessandro, Foo, & Long, 2009). Therefore, to enhance the CO<sub>2</sub> adsorption capacity of MOFs at low pressures, researchers focused on several approaches.

One of these strategies is to remove solvent molecules that are bound to terminals and thereby, open metal sites would be created (Britt, Furukawa, Wang, Glover, & Yaghi, 2009; B. Chen et al., 2000; Dietzel, Besikiotis, & Blom, 2009; Dietzel et al., 2008; Millward & Yaghi, 2005c). By this way, coordinatively unsaturated metal would act as adsorption sites for CO<sub>2</sub> molecule (Caskey, Wong-Foy, & Matzger, 2008; Mu, Li, Huang, & Walton, 2012; Sanz, Martínez, Orcajo, Wojtas, & Briones, 2013; Wade & Dincă, 2012; H. Wu, Simmons,

Srinivas, Zhou, & Yildirim, 2010). Several other researchers enhanced the achieved CO<sub>2</sub> uptake capacities by changing the organic linker which increases both the surface area and the CO<sub>2</sub> uptake capacity (H.-S. Choi & Suh, 2009; Farha et al., 2010, 2012; Henke, Schneemann, Wütscher, & Fischer, 2012; Masoomi, Stylianou, Morsali, Retailleau, & Maspoch, 2014; B. Zheng, Yun, et al., 2013). Moreover, some other researchers synthesized MOFs with different morphologies to increase the CO<sub>2</sub> adsorption performances (Bataille et al., 2012; T. Li, Sullivan, & Rosi, 2013; Sarawade, Tan, & Polshettiwar, 2013; Q. Yan et al., 2013). Another strategy to enhance the CO<sub>2</sub> uptake capacities of MOFs at low pressures is to functionalize MOFs with amines. However, amine functionalized MOFs did not show promising results in CO<sub>2</sub> capture studies (Duan et al., 2012; Montoro et al., 2012; Qingfei Wang et al., 2013; B. Zheng, Liu, et al., 2013). Several researchers investigated the effect of PEI, alkylamine and carboxyl group incorporation to the MOF structure which showed enhanced CO<sub>2</sub> adsorption capacity and performance (Yingli Hu, Verdegaal, Yu, & Jiang, 2014; Y. Lin, Yan, Kong, & Chen, 2013; Si et al., 2012; Xiang, Leng, & Cao, 2012).

Despite all the enhancements achieved, it is still a challenge to have optimum CO<sub>2</sub> adsorption capacity at 1 bar and 298 K. Researchers should focus on alternative methods that would develop low-cost, environmentally friendly, regenerable, chemically and thermally stable MOFs with high CO<sub>2</sub> adsorption capacities measured at 298 K and 1 bar.

### **2.3. Gas Adsorption**

In adsorption processes, the solid that is used to adsorb the gas is called the adsorbent while the gas that is being adsorbed is called the adsorptive and the vapor that is in the adsorbed state is the adsorbate (Lowell, Shields, Thomas, & Thommes, 2004b). The amount of gas adsorbed on the adsorbent depends on temperature, pressure, and the interaction potential between the adsorbate and the adsorbent. There are two types of adsorption processes: Physisorption and chemisorption. Interaction strength between the adsorbate and the adsorbent defines whether physisorption or chemisorption occur.

In chemisorption the adsorbate is strongly and chemically bonded to the surface and the adsorbate can be chemically adsorbed on a specific site which is due to the chemical bonds form between the site and the adsorbate. The very characteristic feature of

chemisorption is the large interaction potentials which results in high heats of adsorption (Lowell et al., 2004b).

Physisorption is a completely reversible process. Unlike chemisorption, it is very typical of physisorption to possess low heats of adsorption. Moreover, during the adsorption process no changes occur in the surface of the adsorbent and unlike in chemisorption, adsorbate covers the whole surface rather than being adsorbed on specific sites. In physisorption, surface of the adsorbent can be covered with more than a single layer of adsorbate. Despite the small pores, no activation energy is necessary for the adsorption equilibrium to be achieved (Lowell et al., 2004b).

### **2.3.1. Thermodynamics of Adsorption**

During the adsorption process, entropy of the adsorbate decreases since the degree of multiplicity of the adsorbate is lower than the degree of multiplicity of the adsorptive. It is assumed for physisorption that the entropy of the adsorbent does not change during adsorption. However, there may be cases where the entropy of the adsorbent increases. Even if it increases, this increase will be lower than the decrease in the adsorbate's entropy which makes the entropy change of the whole system lower than zero.

The spontaneity of the system depends on the change in Gibbs free energy. For a system to be spontaneous, the change in the Gibbs free energy ( $\Delta G$ ) should be negative. Physisorption processes are spontaneous processes. Gibbs free energy is defined by the following formula at constant temperatures where  $\Delta G$  is the change in the Gibbs free energy,  $\Delta H$  is the change in enthalpy, and  $\Delta S$  is the change in entropy:

$$\Delta G = \Delta H - T\Delta S$$

For the negative value of  $\Delta G$  and the negative value of  $\Delta S$ ,  $\Delta H$  becomes a negative value which means that physisorption processes are always exothermic (Lowell et al., 2004b).

### **2.3.2. Adsorption Potential**

International Union of Pure and Applied Chemistry (IUPAC) defined pore width as the pore diameter of the cylindrical pores or the distance between the pore walls of slit pores

(Lowell et al., 2004b). In accordance with the size of the pore widths, pores are divided into three categories: Micropores, mesopores, and macropores. The pore widths of micropores are smaller than 2 nm, the pore widths of mesopores range in between 2 to 50 nm and lastly, the pore width of macropores are greater than 50 nm (Lowell et al., 2004b). The following figure (Figure 2) illustrates the adsorption potential graphs of macro-, meso- and microporous adsorbents.

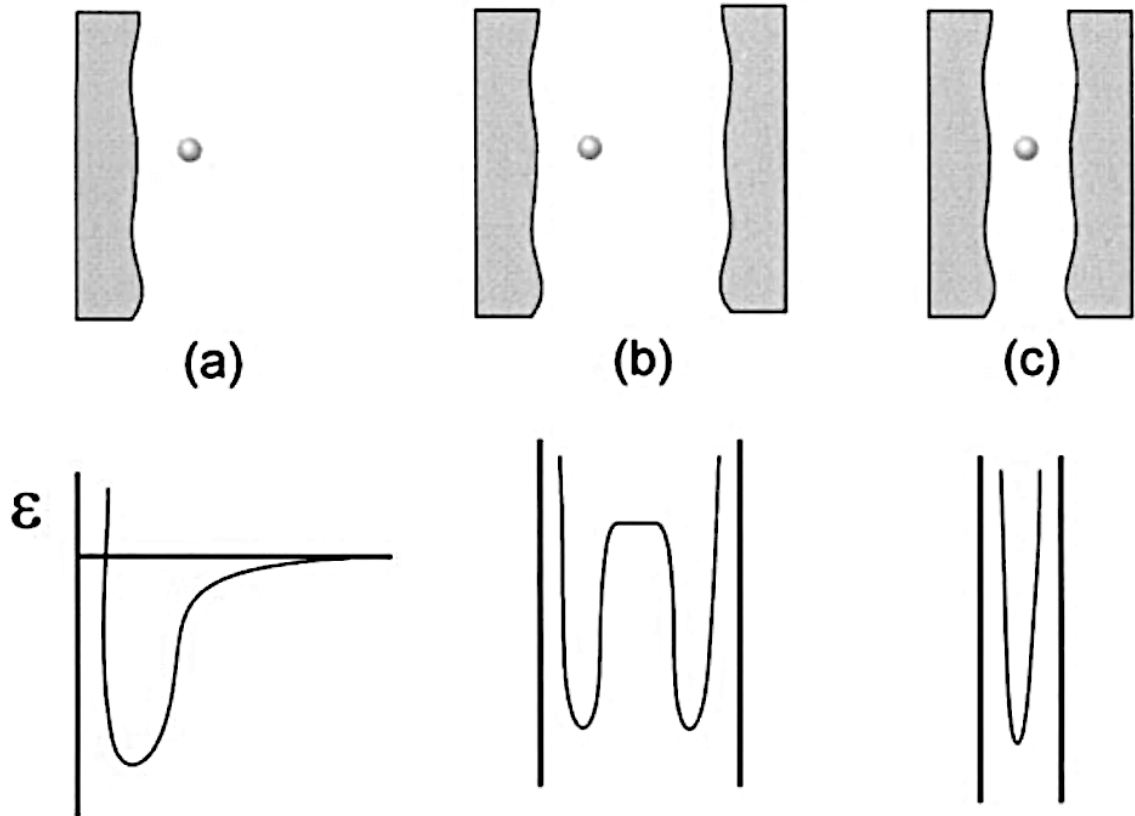


Figure 2. Illustration of the adsorption potential graph of (a) macroporous, (b) mesoporous, and (c) microporous adsorbents (Lowell et al., 2004b).

Figure 2 (a) illustrates the adsorption potential graph of a macropore. The pore width of a macropore is greater than 50 nm. The pore width is too large that a macropore is considered as a flat surface. Figure 2 (b) shows that in the middle of a mesopore, the adsorption potential is negligible. Therefore, the adsorption behavior of mesopores depends on both the attractive interactions between fluid molecules and the interactions between the wall and the fluid. Figure 2 (c) illustrates the adsorption potential of micropores. In the case of micropores, the adsorption behavior is mostly depended on the interactions between the pore walls and the fluid molecules.

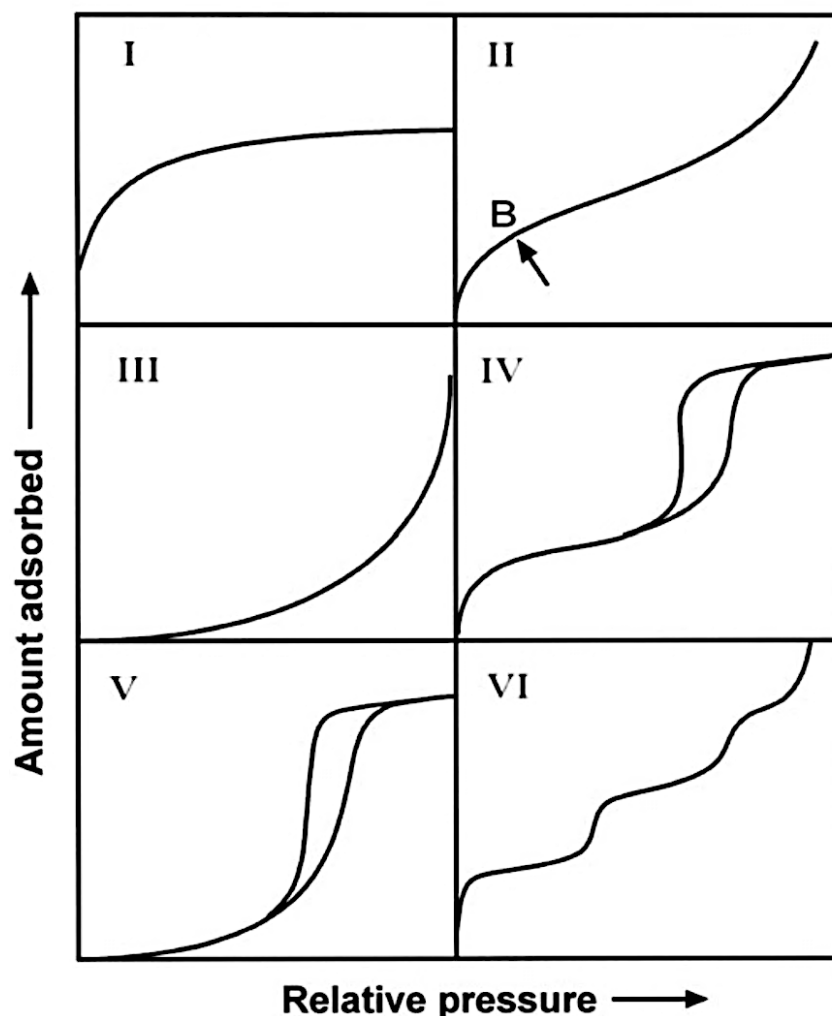


Figure 3. Adsorption isotherms (Lowell et al., 2004b)

Figure 3 shows the adsorption isotherms classified by IUPAC. In 1985, IUPAC classified the adsorption isotherms in six groups (Union, Pure, & Chemistry, 1985). Figure 3 I illustrates Type I isotherms at which micropores dominate the pore structure. High  $N_2$  uptakes obtained at low pressures ( $P/P_0 < 0.2$ ) illustrate the presence of micropores. Figure 3 II represents Type II isotherms which are the characteristic isotherms of macro- and/or nonporous materials. Point B shown on the graph (Figure 3 II) is the point where monolayer coverage is completed and multilayer adsorption starts. Figure 3 III illustrates Type III isotherms. These types of isotherms are rarely observed at which adsorbate-adsorbate interactions dominate. Type IV isotherms (Figure 3 IV) are the characteristic isotherms of mesoporous materials with hysteresis loop present. At the first part of the isotherm a monolayer-multilayer adsorption occurs and then a plateau is achieved which is associated



with limited N<sub>2</sub> uptake and thus, pore filling. Similar to Type IV isotherms, Type V isotherms (Figure 3 V) possess a hysteresis loop. However, the initial part of Type V isotherms is different from Type IV isotherms. The initial part of the Type V isotherms illustrates the presence of weak adsorbate-adsorbent interactions. Type VI isotherms (Figure 3 VI) shows the typical features of a non-porous adsorbent. The several steps of multilayer adsorption can be observed in the isotherm (Hill, 1955).

## **2.4. Hydrogen Storage**

Energy has a crucial role on society's economic development. Rising energy demand results in excessive fossil fuel consumption, and more importantly, adversely influences the ecosystem and human health (Fakioğlu, Yürüm, & Veziroğlu, 2004). A fuel that can meet the necessary energy demand should be developed before fossil fuel reserves are depleted (Andreas Züttel, Remhof, Borgschulte, & Friedrichs, 2010a).

Hydrogen is an abundant element that is a clean alternative to fossil fuels (Khan, Kang, Seok, & Jhung, 2011; L. Schlapbach & Züttel, 2001). Hydrogen has the following advantages over fossil fuels: i) CO<sub>2</sub> does not form during its combustion; and ii) hydrogen possesses a high energy density (energy per kilogram) which is three times greater than the energy density of the hydrocarbon based fuels (Mazloomi & Gomes, 2012; L. Schlapbach & Züttel, 2001).

Hydrogen fuel-based technologies are promising alternatives to fossil fuel-based technologies in the transportation sector since combustion of fossil fuels contribute by 24% to the overall CO<sub>2</sub> emissions ("Aviation – Tracking Transport 2019 – Analysis - IEA," n.d.). However, storing hydrogen in a safe, light and economic way still remains as a challenge which is necessary for the practical use of on-board hydrogen storage systems (Mazloomi & Gomes, 2012; Andreas Züttel, 2004).

Hydrogen is stored as: i) compressed gas in high pressure gas cylinders; ii) liquid hydrogen in cryogenic tanks; iii) absorbed hydrogen (metal hydrides); and iv) adsorbed hydrogen (Andreas Züttel, 2004). However, each method has its own drawbacks.

Being a widely used hydrogen storage technology, compressed hydrogen storage systems are used in various prototype fuel cell vehicles (J. Zheng et al., 2012). High pressures are necessary for the use of highly pressurized gas cylinders since compressed hydrogen gas

possesses a low volumetric density (Abe, Popoola, Ajenifuja, & Popoola, 2019; J. Yang, Sudik, Wolverton, & Siegel, 2010). However, having highly pressurized compressed gas cylinders in the vehicles is risky for safe transportation (Durbin & Malardier-Jugroot, 2013). Moreover, it is very expensive to store a highly pressurized hydrogen gas in a vessel that can safely store hydrogen under high pressure (O'Malley et al., 2015). Recently, DOE has made some suggestions: i) decreasing the cost of carbon fiber and carbon fiber composites; and ii) development of cost-effective alternative composites to carbon fiber. Lastly, in the case of large vehicles, the large volumes of the storage tanks may not have significant effect. However, the size of the storage tanks has particular importance in light-duty vehicles. Despite the progresses made, the use of compressed hydrogen gas at light-duty platforms remains as a challenge (Office-of-Energy-Efficiency-&-Renewable-Energy, 2015).

The energy content of liquid hydrogen storage systems is greater than the energy content of its compressed state. However, liquefaction temperature of hydrogen increases the power necessary for the liquifying process which makes hydrogen storage in cryogenic tanks even more expensive than its pressurized gas form (Carpetis, 1982; Sakintuna, Lamari-Darkrim, & Hirscher, 2007; Andreas Züttel et al., 2010a). Moreover, the cryogenic storage tanks should be thermally insulated to avoid boiling-off of the hydrogen. The energy necessary for the liquefaction process, and the thermal insulation necessary to avoid boil-off of hydrogen increase the cost of the process which limit the practical use of liquid hydrogen (Andreas Züttel, 2004).

At high temperatures transition metals and metal alloys react with hydrogen gas to form metal hydrides (Andreas Züttel, 2004). As hydrogen molecules come close to the metal surface these molecules experience an attractive force, van der Waals forces. In order to form a hydrogen metal bond, hydrogen molecules should overcome the necessary activation barrier. When hydrogen molecules overcome this activation barrier, they will be chemisorbed on the metal surface sharing their electrons with the metal atoms (Andreas Züttel, 2004). During the absorption process, phase transition occurs which offers metal hydrides to absorb large quantities of hydrogen at constant pressure. The chemical bonds formed between hydrogen and metal hydrides are stronger than the bonds formed in physisorption. Therefore, it requires higher amount of energy for hydrogen to be desorbed (Andersson & Grönkvist, 2019). Elemental metal hydrides, intermetallic hydrides, and complex metal hydrides are used in hydrogen storage studies. Most of the elemental metal

hydrides cannot be used practically in hydrogen storage applications owing to the thermodynamics of the process and/or the low hydrogen storage capacities (Sandrock, 1999). For instance, high temperatures are required for the hydrogenation and dehydrogenation process of magnesium hydrides, it is very difficult to regenerate aluminum unless the regeneration process is conducted at very high temperatures (Aguey-Zinsou & Ares-Fernández, 2010; de Rango, Marty, & Fruchart, 2016; Fabian San Francisco, CA (United States)], Petrie Menlo Park, CA (United States)], Crouch-Baker Menlo Park, CA (United States)], & Fong Menlo Park, CA (United States)], 2017; J Graetz et al., 2011; Jason Graetz & Hauback, 2013; Hua & Ahluwalia, 2011; Shao, He, Lin, & Li, 2018; Y. Sun et al., 2018; Yartys et al., 2019). In the case of intermetallic hydrides, they possess low gravimetric hydrogen storage capacities and the process is not cost-effective (Bellosta von Colbe et al., 2019; Harries, Paskevicius, Sheppard, Price, & Buckley, 2012; Sandrock, 1999; Wenger, Polifke, Schmidt-Ihn, Abdel-Baset, & Maus, 2009). However, intermetallic hydrides are used in several applications at which the weight of the storage system is not important such as mining vehicles and forklifts (Bevan, Züttel, Book, & Harris, 2011; Lototskyy et al., 2016; Sandrock & Bowman, 2003). The practical use of complex metal hydrides is limited with their high dehydrogenation temperatures (Felderhoff, Weidenthaler, von Helmolt, & Eberle, 2007; Møller et al., 2017; Puszkiel et al., 2017). Moreover, most of the complex metal hydrides cannot be reversibly dehydrogenated (Pommerin, Weidenthaler, Schüth, & Felderhoff, 2010; Puszkiel et al., 2017). The regeneration process is energy intensive and expensive (Ouyang, Zhong, Li, & Zhu, 2018). Metal hydrides can absorb large amounts of hydrogen (Andreas Züttel, 2004). However, the measured gravimetric hydrogen storage densities of reversible transition metals are lower than 3 wt.% (at room temperature and atmospheric pressure) (Mazloomi & Gomes, 2012; Andreas Züttel, 2004). There rises the necessity of the use of heavy tanks which fails the practical use of metal hydrides (Andreas Züttel, 2003a).

Lastly, hydrogen molecules can be adsorbed on the surface of porous sorbents reversibly by the weak van der Waals forces. Physisorption is the reversible hydrogen adsorption process at which van der Waals interactions dominate (Andreas Züttel, 2003a). Physisorption has the advantage over the other methods by its low cost and feasibility (Andreas Züttel, 2004). However, it is limited by the weak van der Waals forces. Despite the high H<sub>2</sub> adsorption capacities of adsorbents measured at 77 K, the measured H<sub>2</sub> adsorption

capacities decrease drastically at room temperature and atmospheric pressure (L. Schlapbach & Züttel, 2001; Andreas Züttel, 2004). Therefore, researchers have put extensive effort to develop porous sorbents that can store high amounts of hydrogen at ambient conditions (Attia, Menemparabath, Arepalli, & Geckeler, 2013; A. Gupta et al., 2019; Pareek, Rohan, Chen, Zhao, & Cheng, 2017; H. Zhou et al., 2015b). Porous materials with high BET surface areas have been investigated for their H<sub>2</sub> adsorption capacities (Dündar-Tekkaya & Yürüm, 2016; Durbin & Malardier-Jugroot, 2013; A. G. Klechikov et al., 2015a; A. Klechikov et al., 2015; Barbara Panella, Hirscher, & Roth, 2005a; L. Schlapbach & Züttel, 2001). Despite the achievements and enhancements obtained in H<sub>2</sub> adsorption studies, it is still a challenge to achieve the target set by DOE at ambient conditions (Broom et al., 2019; Moradi & Groth, 2019; Pyle, Gray, & Webb, 2016; Yürüm, Taralp, & Veziroglu, 2009a; Qiang Zhao, Yuan, Liang, & Li, 2013).

#### **2.4.1. Hydrogen Physisorption with Carbon-based Materials**

Carbon-based materials are considered as promising candidates in gas adsorption studies owing to their availability, low-cost, low densities, high BET surface areas and large pore volumes, high chemical stabilities and tunable structures (H.-M. Cheng, Yang, & Liu, 2001; Ritschel et al., 2002; Yürüm, Taralp, & Veziroglu, 2009b). Activated carbons (ACs), carbon nanotubes (CNTs), and graphene and graphene-based, graphene-like materials, are several carbon-based materials investigated for their H<sub>2</sub> adsorption capacities (C. C. Ahn et al., 1998; Baughman, Zakhidov, & de Heer, 2002; Bénard & Chahine, 2007; Chambers, Park, Baker, & Rodriguez, 1998; P. Chen, Wu, Lin, & Tan, 1999; H.-M. Cheng et al., 2001; Dillon et al., 1997; Gadiou et al., 2005; Gangu, Maddila, Mukkamala, & Jonnalagadda, 2019; Gohari-Bajestani, Akhlaghi, Yürüm, & Yürüm, 2017; Gohari Bajestani, Yürüm, & Yürüm, 2016; B. K. Gupta & Srivastava, 2000, 2001; M Hirscher et al., 2002; Kayiran, Lamari, & Levesque, 2004; C Liu et al., 1999; Lueking & Yang, 2003; Nijkamp, Raaymakers, van Dillen, & de Jong, 2001; Barbara Panella, Hirscher, & Roth, 2005b; Ritschel et al., 2002; Schimmel et al., 2004; Shiraz & Tavakoli, 2017; Takagi, Hatori, Soneda, Yoshizawa, & Yamada, 2004; Takagi, Hatori, Yamada, Matsuo, & Shiraishi, 2004; Texier-Mandoki et al., 2004; Thomas, 2007; Tozzini & Pellegrini, 2013; X. B. Wu, Chen, Lin, & Tan, 2000; Ye et

al., 1999; Yürüm et al., 2009b; X. B. Zhao, Xiao, Fletcher, & Thomas, 2005; Y. Zhou, Feng, Sun, & Zhou, 2003).

The fast adsorption desorption kinetics, high reversibility, high BET surface area, wide range of pore size make ACs promising candidates in gas adsorption studies (Y. Xia, Yang, & Zhu, 2013; Yürüm et al., 2009b). Studies show that the measured H<sub>2</sub> adsorption capacities (77 K) of ACs range in between 0.2 to 5.5 wt.% (Bénard & Chahine, 2007; Kayiran et al., 2004). However, when the H<sub>2</sub> adsorption studies are conducted at 298 K, the measured adsorption capacities decrease, drastically (Chahine & Bose, 1994; de la Casa-Lillo, Lamari-Darkrim, Cazorla-Amorós, & Linares-Solano, 2002; Thomas, 2007; L. Zhou, Zhou, & Sun, 2004). To enhance the measured H<sub>2</sub> adsorption capacities at 298 K, researchers prepared chemically activated carbons which showed an enhanced H<sub>2</sub> adsorption capacity of 3.2 wt.% at 298 K and 200 bar (Jordá-Beneyto, Suárez-García, Lozano-Castelló, Cazorla-Amorós, & Linares-Solano, 2007).

Studies show that CNTs possess H<sub>2</sub> adsorption capacities lower than 1 wt.% at 298 K and 1 bar (Ansón et al., 2004; M Hirscher et al., 2002; A Züttel et al., 2002). To enhance the measured H<sub>2</sub> adsorption capacities, researchers conducted acid treatment process which enhanced the measured H<sub>2</sub> adsorption capacities at 77 K to 1.7 wt.% (Takagi, Hatori, Soneda, et al., 2004). In the meanwhile, theoretical studies showed that neither the H<sub>2</sub> adsorption capacities at 77 K nor the H<sub>2</sub> adsorption capacities at 298 K are sufficient enough to meet the U.S. DOE target (Frankland & Brenner, 2001; Guay, Stansfield, & Rochefort, 2004).

H<sub>2</sub> storage capacities of graphene and graphene based materials are investigated by various researchers and research groups owing to their high BET surface areas, high pore volumes, light weight and high abundancies (Jin et al., 2011; Kaur & Pal, 2016; A. G. Klechikov et al., 2015b; Kostoglou et al., 2016; Qin et al., 2015; C. N. R. Rao, Sood, Subrahmanyam, & Govindaraj, 2009; Srinivas et al., 2010; Tozzini & Pellegrini, 2013; Vinayan, Nagar, & Ramaprabhu, 2013; L. Wang, Stuckert, & Yang, 2011; L. Wei & Mao, 2016; Q. Zhang et al., 2016; C. Zhou & Szpunar, 2016; C. Zhou, Szpunar, & Cui, 2016; H. Zhou et al., 2015a; Yu Zhu, James, & Tour, 2012). Researchers figured out that at 298 K and 120 bar the H<sub>2</sub> adsorption capacities of bulk graphene powders were at most 1 wt.% (A. G. Klechikov et al., 2015b). To enhance the measured H<sub>2</sub> adsorption capacities at 298 K, researchers used hydrogen spillover mechanism. For instance, researchers synthesized Ni/reduced graphene oxide (rGO), Ni/Pd/rGO, and Ni/Pd/Ag/rGO hybrid materials. The

measured H<sub>2</sub> adsorption capacities (293 K and 800 mm Hg) of Ni/rGO, Ni/Pd/rGO, and Ni/Pd/Ag/rGO hybrid materials were enhanced to 0.007 wt.%, 0.13 wt.% and 0.055 wt.%, respectively (L. Wei & Mao, 2016). Some other researchers developed hybrid rGO nanocomposites. The measured H<sub>2</sub> adsorption capacity (298 K and 10 bar) of Pd/Al<sub>2</sub>O<sub>3</sub>-rGO hybrid nanocomposite was enhanced to 0.31 wt.% (Gohari Bajestani et al., 2016). Another researcher synthesized Pt-doped HKUST-1/GO composite whose H<sub>2</sub> adsorption capacity was enhanced to 0.250 mmol/g at 298 K and 860 mm Hg (H. Zhou et al., 2015a). Researchers decorated graphene with Ni nanoparticles and formed a Ni-graphene composite. The measured H<sub>2</sub> adsorption capacities of Ni-graphene composite at 298 K are 0.14 wt.%, and 1.18 wt.% at 1 bar and 60 bar, respectively (C. Zhou et al., 2016). In conclusion, studies show that bulk graphene does not show an optimal H<sub>2</sub> adsorption capacity at 298 K that can meet the U.S. DOE target. Significant enhancements are achieved by spillover mechanism provided by metal catalysts and the hybrid nanocomposites. However, despite the all efforts spent, the measured optimal H<sub>2</sub> adsorption capacities at 298 K are far from meeting U.S. DOE target.

#### **2.4.2. Hydrogen Physisorption with Zeolites**

The high BET surface areas, high pore volumes, chemical and thermal stabilities of zeolites led researchers investigate the hydrogen storage performances of zeolites (Carraro et al., 2014; X. Du & Wu, 2006; Dündar-Tekkaya & Yürüm, 2015; J. Edler, A. Reynolds, J. Branton, R. Trouw, & W. White, 1997; H W Langmi et al., 2003; S.-J. Park & Lee, 2010; Ramachandran, Ha, & Kim, 2007; Sheppard, Maitland, & Buckley, 2005; Weitkamp, Fritz, & Ernst, 1995; C. Wu, Gao, Hu, Chen, & Shi, 2009; Andreas Züttel, 2003b). Theoretical studies show that the maximum H<sub>2</sub> adsorption capacity (77 K) of a zeolite can range in between 2.6 to 2.9 wt.% (Vitillo, Ricchiardi, Spoto, & Zecchina, 2005). In line with the theoretical studies, a maximum of 2.1 wt.% H<sub>2</sub> adsorption capacity was achieved at 77 K, experimentally (J. Dong, Wang, Xu, Zhao, & Li, 2007; H W Langmi et al., 2003; Sheppard & Buckley, 2008). In order to enhance the measured H<sub>2</sub> adsorption capacities, researchers incorporated transition metals into the frameworks of zeolites (Carraro et al., 2014; Dündar-Tekkaya & Yürüm, 2015; S.-J. Park & Lee, 2010; Prasanth, Raj, Bajaj, Kim, & Jasra, 2010; Ramachandran et al., 2007; Yamamoto et al., 2011). For instance, a Ni doped MCM-41

showed a H<sub>2</sub> adsorption capacity of 0.68 wt.% at 298 K and 65 bar. The enhancement in the H<sub>2</sub> adsorption capacity was attributed to the spillover effect owing to the presence of Ni particles (S.-J. Park & Lee, 2010). In order to enhance the H<sub>2</sub> adsorption capacity of MCM-41, researchers loaded it with Pd and Ni metal mixtures. Pd-Ni loaded MCM-41 showed a H<sub>2</sub> adsorption capacity of 0.98 wt.% at 298 K and 10 bar (Dündar-Tekkaya & Yürüm, 2015). Studies showed that doping zeolites with transition metals enhanced the H<sub>2</sub> adsorption capacities of zeolites measured at 298 K thanks to the spillover effect. However, the reported H<sub>2</sub> adsorption capacities cannot meet the DOE target (Carraro et al., 2014; Dündar-Tekkaya & Yürüm, 2015; S.-J. Park & Lee, 2010; Prasanth et al., 2010; Ramachandran et al., 2007; Yamamoto et al., 2011).

## **2.5. Metal-organic Frameworks (MOFs)**

MOFs, a new family of porous materials, were firstly introduced by Yaghi in 1995 (O M Yaghi, Li, & Li, 1995). These crystalline porous frameworks are constructed by linking metal ions or metal ion clusters (secondary building units) with organic ligands (“Emergence of Metal-Organic Frameworks,” 2019). Bridging ligands link neighboring secondary building units (SBUs) to each other.

Secondary building units (SBUs) define the final topology of the MOF framework. Moreover, the geometry of SBU depends on: i) the type of the ligand; ii) the type of the metal; and iii) metal to ligand ratio. Thus, depending on the choice of the starting materials, structural and textural properties of MOFs can be arranged which offers a wide variety of MOFs with different chemical and textural properties to be synthesized.

Most commonly, MOFs are synthesized via a solvothermal synthesis route. Metal salt, organic ligand and solvent are placed in a glass vial tube which is properly sealed, and the reaction takes place at elevated temperatures. Solvothermal synthesis follows the working principle of Lewis acid-base reactions at which the metal salt and the organic ligand are mixed in a solvent and heated in an oven at high temperatures. Metal ions act as Lewis acids while the deprotonated ligands act as Lewis bases. Considerable attention has to be given to the synthesis conditions which possess significant role on the produced MOF structures and determine whether a bulk precipitate or a single crystal will form (D. Zhao, Timmons, Yuan, & Zhou, 2011a).

Solvothermal synthesis produces high quality crystals while reaction duration lasts from hours to days. It is important to consider pH, temperature, concentrations of the metal salt, the ligand, and the solvent since all these parameters influence the final product, considerably.

Another method to synthesize MOFs is microwave-assisted method which accelerates the rates of the reactions (Biswas et al., 2009; Bux et al., 2009; Centrone, Harada, Speakman, & Hatton, 2010; Centrone, Yang, et al., 2010; Chalati, Horcajada, Gref, Couvreur, & Serre, 2011; J.-S. Choi, Son, Kim, & Ahn, 2008; Denysenko et al., 2011; Horcajada et al., 2010b; Jae et al., 2006; S. H. Jhung et al., 2007; Sung Hwa Jhung et al., 2006; Jung, Yang, Kim, Kim, & Ahn, 2010; Khan, Haque, & Jhung, 2010a; Khan et al., 2011; D. O. Kim et al., 2011; J. S. Lee et al., 2010; Wei Li, Jin, Huang, & Chen, 2010; B. Liu et al., 2008; H.-K. Liu, Tsao, Zhang, & Lin, 2009; C.-M. Lu, Liu, Xiao, & Harris, 2010; Ni & Masel, 2006; J. H. Park, Park, & Jhung, 2009; Sabouni, Kazemian, & Rohani, 2010; Schlesinger, Schulze, Hietschold, & Mehring, 2010; Y.-K. Seo et al., 2009; Silva, Valente, Rocha, & Almeida Paz, 2010; Taylor-Pashow, Della Rocca, Xie, Tran, & Lin, 2009; Tonigold et al., 2009; X.-F. Wang, Zhang, Huang, Zhang, & Chen, 2008; Xiang et al., 2010). In the microwave-assisted method, synthesis depends on the interaction of electric charges with electromagnetic waves at which the orientations of molecules change permanently. As molecules collide, kinetic energy of the system increases. Therefore, reaction durations are shortened.

In the electrochemical synthesis, an electrode that contains the metal ions and a solution that contains the linker are present (Ameloot et al., 2010, 2009; Hartmann et al., 2008; Mueller et al., 2006; Schlesinger et al., 2010). When voltage is applied, metal ions move through the reaction medium. Metal ions and linkers react and then form MOFs (Al-Kutubi, Gascon, Sudhölter, & Rassaei, 2015; Mueller et al., 2005).

Another synthesis method is mechanochemical synthesis at which a mechanical force induces chemical reactivity (Beldon et al., 2010; Beyer & Clausen-Schaumann, 2005; Frišćić, 2010; Frišćić & Fábián, 2009; Frišćić et al., 2010; Fujii et al., 2010; Garay, Pichon, & James, 2007; Klimakow, Klobes, Thünemann, Rademann, & Emmerling, 2010; Pichon & James, 2008; Schlesinger et al., 2010; Willans et al., 2011; Hongwei Yang, Orefuwa, & Goudy, 2011; W. Yuan, Frišćić, Apperley, & James, 2010; W. Yuan, Garay, et al., 2010).



Mechanochemical reactions benefit from the short reaction times, and solvent-free synthesis environments.

In sonochemical synthesis, reaction occurs as high-energy ultrasound is applied. Bubbles firstly form and then collapse which provide high local temperatures and pressures to be achieved. By this way, reactions occur faster. Sonochemical synthesis is used to scale-up MOF synthesis which decreases reaction durations while forming small MOF crystals (Chalati et al., 2011; Jung et al., 2010; Khan, Haque, & Jhung, 2010b; Khan & Jhung, 2009; J. Kim et al., 2011; Z.-Q. Li et al., 2009; Qiu, Li, et al., 2008; Sabouni et al., 2010; Schlesinger et al., 2010; Tranchemontagne, Hunt, & Yaghi, 2008).

MOFs significantly benefit from their highly porous and crystalline structure, high surface area, tunable pore structure, and their ability to be loaded with other elements and components without any changes in their topology (Rowsell & Yaghi, 2004b). These properties make MOFs promising candidates in many application areas such as adsorption and separation studies, catalysis, chemical separations, degradation of toxic substances, drug delivery, gas storage and release, light and water harvesting, and sensor studies (Adams, Carson, Ward, Tannenbaum, & Koros, 2010; T.-H. Bae et al., 2013; Y. S. Bae & Snurr, 2011; Corma, García, & Llabrés I Xamena, 2010; García-García, Moreno, Díaz, Bruix, & Corma, 2016; Hanikel et al., 2019; Hanikel, Prévot, & Yaghi, 2020; Horcajada et al., 2006; Katz et al., 2014, 2015; Jeongyong Lee et al., 2009; J. R. Li, Kuppler, & Zhou, 2009; J. R. Li et al., 2011; Jiewei Liu et al., 2014; López-Maya et al., 2015; Nguyen et al., 2020; Nunes, Gomes, Pillinger, Gonçalves, & Abrantes, 2015; Y. Peng et al., 2013; Rieth, Yang, Wang, & Dincă, 2017; J. S. Seo et al., 2000; So, Wiederrecht, Mondloch, Hupp, & Farha, 2015; Taylor-Pashow, Della Rocca, Huxford, & Lin, 2010; J.-L. Wang, Wang, & Lin, 2012).

Micropores make microporous materials promising candidates in gas storage and separation studies since the interactions between the pores and the pore walls are very strong. The high microporosity and large surface areas of MOFs make these materials promising in gas adsorption, storage and separation studies (Dincă & Long, 2008; Kitagawa, Kitaura, & Noro, 2004; JeongYong Lee et al., 2009; Mueller et al., 2006; Omar M Yaghi et al., 2003; X. Zhao et al., 2004). To enhance the adsorbed gas amount, the number of active adsorption sites within the porous framework should be increased which can be achieved by ligand expansion method. However, ligand expansion method was not as effective as it was thought: MOFs synthesized with expanded ligands were fragile, and had higher tendency to self-

interpenetrate (B. Chen, Eddaoudi, Hyde, O'Keeffe, & Yaghi, 2001; Furukawa et al., 2010; X. Lin, Jia, Hubberstey, Schröder, & Champness, 2007).

### **2.5.1. Hydrogen Storage in MOFs**

MOFs are highly crystalline and highly porous materials that possess high BET surface areas, tunable pore size and pore structure, and found to be promising candidates in various application areas including adsorption/desorption, gas storage and separation studies.

After the promising results obtained from the very first study conducted in 2003, many researchers and research groups spent particular attention on hydrogen storage performances of MOFs (Rosi et al., 2003). MOFs are promising candidates for hydrogen storage studies and get ahead of other materials since: i) pore sizes and structure of MOFs can be designed to enhance the H<sub>2</sub> adsorption performances, and ii) the specific hydrogen adsorption sites can be identified in a MOF. From 2003 till now, many studies have been conducted to enhance hydrogen storage performances of MOFs. MOFs possess very high H<sub>2</sub> adsorption capacities at 77 K and high pressures. However, when the studies are conducted at 298 K, H<sub>2</sub> adsorption capacities of MOFs decrease, dramatically. It is still a challenge to design a MOF with a H<sub>2</sub> adsorption capacity that meet the DOE target of hydrogen storage.

While conducting H<sub>2</sub> adsorption studies, one has to be careful about the excess and total H<sub>2</sub> adsorption capacities. At 1 bar the excess and total H<sub>2</sub> adsorption values are found to be the same while as the pressure increases to 100 bar, these two values differ from each other (Murray, Dincă, & Long, 2009). Excess adsorption is an approximation of the amount of H<sub>2</sub> that can be adsorbed on the surface of the material. In a microporous material, the excess adsorption would first reach its maximum, and then start to decrease with increasing pressure. Depending on the material, the maximum adsorption capacity would be achieved in between 20 to 40 bars. In the meanwhile, total uptake considers both the surface adsorbed H<sub>2</sub> and the compressed H<sub>2</sub> gas within the pores.

To understand the H<sub>2</sub> adsorption behavior in MOFs, several researchers worked on computational models. It was found that H<sub>2</sub> adsorption capacity measured at 77 K is correlated with surface area. Moreover, very low H<sub>2</sub> adsorption capacities can be achieved at 298 K. This correlation between H<sub>2</sub> adsorption capacity measured at 77 K and the surface

area and the low H<sub>2</sub> adsorption capacities achieved at 298 K are attributed to weak van der Waals interactions between MOFs and the H<sub>2</sub> molecules. The very weak van der Waals interactions result isosteric heats of adsorption values to vary in between 4 to 7 kJ/mol (Düren & Snurr, 2004; Frost, Düren, & Snurr, 2006b; Frost & Snurr, 2007; S. S. Han, Deng, & Goddard III, 2007; S. S. Han & Goddard, 2007; E Klontzas, Mavrandonakis, Froudakis, Carissan, & Kloppe, 2007; Emmanouel Klontzas, Mavrandonakis, Tylianakis, & Froudakis, 2008; Emmanouel Klontzas, Tylianakis, & Froudakis, 2008; Lochan & Head-Gordon, 2006; Mavrandonakis, Tylianakis, Stubos, & Froudakis, 2008).

In order to develop MOFs that function optimally at 298 K, the binding energies between the H<sub>2</sub> molecules and MOFs have to be increased and a MOF that possesses an adsorption enthalpy of 20 kJ/mol should be developed (Bhatia & Myers, 2006b; Garrone, Bonelli, & Otero Areán, 2008; Murray, Dincă, et al., 2009). Several studies showed that partial charges on the surface of MOFs strengthen the H<sub>2</sub> binding via dipole-induced dipole interactions (Lochan & Head-Gordon, 2006; Lochan, Khaliullin, & Head-Gordon, 2008).

H<sub>2</sub> adsorption studies conducted on microporous materials show that adsorption capacity depends on the pore size, considerably. For graphitic carbons, and carbon nanotubes calculations show that having pores with pore diameters of 7 Å would increase the H<sub>2</sub> adsorption capacity of the material to the maximum adsorption capacity at 298 K. Moreover, regardless of the pore shape, a pore size of 10 Å would provide the maximum H<sub>2</sub> adsorption capacity to be achieved at 100 bar (Rzepka, Lamp, & de la Casa-Lillo, 1998).

#### **2.5.1.1.Strategies to increase hydrogen adsorption enthalpy of MOFs**

Introducing open metal sites on the surface of MOFs is found to enhance the H<sub>2</sub> adsorption capacity of MOFs. However, strong metal-H<sub>2</sub> bonds should be avoided and charge-induced dipole interactions should be formed. However, it is challenging to form highly concentrated open metal sites (Dincă & Long, 2008). Strategies that are used to form open metal sites include thermally-assisted solvent molecule evacuation, photolysis, guest metal cation exchange, and use of reactive bridging ligands (Dincă et al., 2006; Dincă et al., 2007; Dincă & Long, 2007; Kaye, Dailly, Yaghi, & Long, 2007a; Kaye & Long, 2005, 2007; Mulfort & Hupp, 2007; Prestipino et al., 2006).

Catenation/interpenetration is a method to enhance H<sub>2</sub> adsorption capacity of MOFs. It is found that as the pore diameters increase, the attraction felt by H<sub>2</sub> molecules at the center

of the pore walls decreases which decreases the measured H<sub>2</sub> adsorption capacities. Therefore, microporous MOFs with smaller pore sizes would be more efficient in H<sub>2</sub> adsorption studies (Belof, Stern, Eddaoudi, & Space, 2007; Kabbour, Baumann, Satcher Joe H., Saulnier, & Ahn, 2006).

Framework interpenetration is a method to increase the amount of narrow pores present in the pore structure of the framework (Shengqian Ma et al., 2007; D. Sun, Ma, Ke, Collins, & Zhou, 2006). However, practically, it is not easy to control. Moreover, computational studies show that even though the heat of adsorption increases when framework interpenetration is issued, the decrease in the surface area, and the pore volume would decrease the total H<sub>2</sub> uptake (Frost & Snurr, 2007).

Hydrogen spillover is another method that can enhance the total H<sub>2</sub> uptake of the framework at which H<sub>2</sub> molecules dissociate into H<sup>\*</sup> on a metal surface while hydrogen atoms migrate towards the pores of the material (Christmann, Ertl, & Pignet, 1976; Gee, Hayden, Mormiche, & Nunney, 2000; Khoobiar, 1964; Pasteur, Dixon-Warren, Ge, & King, 1997; Somorjai, 1994). However, hydrogenation should be reversible and the packing density of H<sup>\*</sup> should be greater than the packing density of H<sub>2</sub> (H. Cheng, Chen, Cooper, Sha, & Pez, 2008; L. Wang & Yang, 2008). The effect of hydrogen spillover phenomenon was tested on several MOFs and encouraging results were obtained, the measured H<sub>2</sub> adsorption capacities of the frameworks increased (Yingwei Li, Yang, & Yang, 2007; Yingwei Li & Yang, 2006b, 2006a, 2007, 2008; Y.-Y. Liu, Zeng, Zhang, Xu, & Sun, 2007). However, there is still room for improvement. For instance, long-time recyclability and reproducibility of the materials should be investigated, and the H<sub>2</sub> adsorption performance of cheaper metals or metal clusters should be tested.

#### **2.5.1.2. Hydrogen adsorption capacities of several MOFs**

Zn<sub>4</sub>O(BDC)<sub>3</sub> is one of the MOFs whose H<sub>2</sub> adsorption capacity was reported for the first time in literature (Rosi et al., 2003). The H<sub>2</sub> adsorption capacity of Zn<sub>4</sub>O(BDC)<sub>3</sub> was measured at 77 K and found to be 1.3 wt. %, 5.1 wt.%, and 10.0 wt.% at 1 bar, 50 bar and 100 bar, respectively (Kaye, Dailly, Yaghi, & Long, 2007b; B Panella, Hirscher, Pütter, & Müller, 2006; Rowsell, Millward, Park, & Yaghi, 2004). However, it was observed that depending on the synthesis procedure reported, H<sub>2</sub> adsorption capacities of Zn<sub>4</sub>O(BDC)<sub>3</sub> vary (Dybtsev, Chun, & Kim, 2004; J. Y. Lee, Olson, Pan, Emge, & Li, 2007; Jinchen Liu

et al., 2008; Pan et al., 2004; B Panella & Hirscher, 2005; B Panella et al., 2006; Rosi et al., 2003; Rowsell et al., 2004; Sabo, Henschel, Fröde, Klemm, & Kaskel, 2007; Wong-Foy, Matzger, & Yaghi, 2006). Moreover,  $\text{Zn}_4\text{O}(\text{BDC})_3$  can be used for 24 cycles without the loss of its adsorption capacity (Kaye et al., 2007b). Researchers investigated the influence of Pd loading on the  $\text{H}_2$  adsorption performance of MOF-5 and found that  $\text{H}_2$  adsorption capacity (at 77 K and 1 bar) of Pd loaded MOF-5 increases from 1.15 to 1.86 wt.% (Sabo et al., 2007).

HKUST-1 is one of the first Cu based MOFs reported in literature (Chui, Lo, Charmant, Orpen, & Williams, 1999). HKUST-1 has a higher isosteric heat of adsorption at low coverage than MOF-5 which provides HKUST-1 to achieve a higher  $\text{H}_2$  adsorption capacity at 77 K and 1 bar (Batten & Robson, 1998; B Panella et al., 2006; Rowsell & Yaghi, 2006a). It was observed that removal of guest molecules and solvent molecules affect the measured  $\text{H}_2$  adsorption capacities, considerably; by a complete solvent removal process, the  $\text{H}_2$  adsorption capacity of HKUST-1 was enhanced to 4.1 wt.% (77 K and 26 bar) (Jinchen Liu et al., 2007).

A Mn based MOF possesses a BET surface area of  $2100 \text{ m}^2/\text{g}$ , an isosteric heat of adsorption of  $10.1 \text{ kJ/mol}$  and achieved a  $\text{H}_2$  adsorption capacity of 6.9 wt.% (77 K and 90 bar). This relatively high  $\text{H}_2$  adsorption capacity of Mn based MOF is attributed to its high isosteric heat of adsorption and the unsaturated  $\text{Mn}^{2+}$  sites present in its framework (Dincă et al., 2006).

MIL-53 that possesses 1D channels with large pore sizes and a BET surface area of  $1100 \text{ m}^2/\text{g}$  was investigated for its  $\text{H}_2$  adsorption capacity. The measured  $\text{H}_2$  adsorption capacities of MIL-53 formed of chromium and MIL-53 formed of aluminum are 3.1 wt.%, and 3.8 wt.% (77 K and 16 bar), respectively (Férey et al., 2003).

MIL-100 and MIL-101 were investigated for their  $\text{H}_2$  adsorption performances at 77 K. The measured maximum  $\text{H}_2$  adsorption capacity of MIL-100 is 3.28 wt.% at 77 K and 26.5 bar while MIL-101a achieved a maximum capacity of 4.5 wt.% (77 K and above 40 bar) and MIL-101b achieved a maximum capacity of 6.1 wt.% (77 K and 80 bar). The differences in the  $\text{H}_2$  adsorption capacities of MIL-100 and MIL-101 were attributed to their different isosteric heat of adsorption values. MIL-101b possesses an isosteric heat of adsorption value greater than MIL-100. Moreover, evacuating  $\text{BDCH}_2$  from the pores of MIL-101b provided MIL-101b to possess a higher  $\text{H}_2$  adsorption capacity than MIL-101a (Latroche, Surblé, Serre, Mellot-Draznieks, Llewellyn, Lee, Chang, Jung, et al., 2006).

MOFs possess very high H<sub>2</sub> adsorption capacities at 77 K. However, at 298 K their H<sub>2</sub> adsorption capacities decrease, drastically. Those lower H<sub>2</sub> adsorption capacities measured at 298 K are attributed to the weak van der Waals interactions between H<sub>2</sub> molecules and MOFs (Dincă et al., 2006; S. S. Han & Goddard, 2007; Kesanli et al., 2004; Latroche, Surblé, Serre, Mellot-Draznieks, Llewellyn, Lee, Chang, Jhung, et al., 2006; Yingwei Li & Yang, 2007; X. Lin et al., 2006; Y.-Y. Liu et al., 2007; Pan et al., 2004; Rosi et al., 2003). For instance, the H<sub>2</sub> adsorption capacities of HKUST-1 and MIL-101 were measured as 0.35 wt.%, and 0.51 wt.% (298 K 10 MPa), respectively (Yingwei Li & Yang, 2008). MIL-53(Al) attained its maximum H<sub>2</sub> adsorption capacity of 1.7 wt.% at 35 MPa (298 K) while MOF-177 which possesses a specific surface area of 4126 m<sup>2</sup>/g achieved its maximum H<sub>2</sub> adsorption capacity of 0.94 wt.% at 45 MPa (298 K) (Voskuilen, Pourpoint, & Dailly, 2012).

Researchers investigated the effect of interconnected channels on the H<sub>2</sub> adsorption capacity of MOFs measured at 298 K. [Co<sub>3</sub>(ndc)<sub>3</sub>(dabco)] achieves a higher H<sub>2</sub> adsorption capacity than [Co<sub>3</sub>(bdc)<sub>3</sub>(dabco)] which is attributed to the interconnected channels of [Co<sub>3</sub>(ndc)<sub>3</sub>(dabco)] and achieved a H<sub>2</sub> adsorption capacity of 0.89 wt.% at 298 K and 17.2 bar (Chun, Jung, Koo, Jeong, & Kim, 2008).

Researchers investigated the influence of spillover on the H<sub>2</sub> adsorption capacities of MOF-5, and IRMOF-8 at 298 K. It was observed that H<sub>2</sub> adsorption capacities of MOF-5 and IRMOF-8 were increased by a factor of 3.3 and 3.1, and a H<sub>2</sub> adsorption capacity of 1.32 wt.% and 1.8 wt.% were achieved, respectively (Yingwei Li & Yang, 2006b). Researchers investigated the effect of platinum doping on activated carbon/MOF-5 hybrid composites. By introducing hydrogen, favorable sites on the activated carbon/MOF-5 composite was created and the H<sub>2</sub> adsorption capacity was enhanced by a factor of 3 to 2.3 wt.% at 298 K and 100 bar (S.-Y. Lee & Park, 2011).

In order to obtain better performances from hydrogen spillover, researchers suggested to use a carbon precursor as a bridge that would enhance the contact between the spillover source and the MOF. Researchers used active carbon as the carbon precursor and enhanced the H<sub>2</sub> adsorption capacities of MOF-5 and IRMOF-8 by a factor of 2, and 8 to 3 wt.% and 4 wt.% at 298 K and 100 bar, respectively (Lachawiec, Qi, & Yang, 2005). Researchers tested the strategy of using a catalyst and a carbon bridge on MOF-177 and found that using a H<sub>2</sub> dissociation catalyst, Pt, and a carbon bridge enhanced the H<sub>2</sub> adsorption capacity of

MOF-177 by 2.5 to 1.5 wt.% at 298 K and 10 MPa. Researchers attributed the enhanced H<sub>2</sub> adsorption capacity to the contact between Pt and activated carbon which ensured a secondary spillover effect on the surface of AC/MOF-177 hybrid composite (Yingwei Li & Yang, 2007). However, some other researchers found contradictory results showing no enhancement in the H<sub>2</sub> adsorption capacities of the bridged composites (Campesi, Cuevas, Latroche, & Hirscher, 2010; Luzan & Talyzin, 2010). In the meanwhile, the bridged spillover strategy enhanced the H<sub>2</sub> adsorption capacities of HKUST-1 and MIL-101 by a factor of 3.2 and 2.8 to 1.12 wt.% and 1.4 wt.% (298 K and 10 MPa), respectively (Yingwei Li & Yang, 2008).

Researchers investigated the influence of doping metal supported carbon catalyst through a carbon bridge on the H<sub>2</sub> adsorption capacities of MIL-101, and MIL-53, and significant enhancements were achieved. H<sub>2</sub> adsorption capacities of MIL-101, and MIL-53 were measured as 1.14 wt.% and 0.63 wt.% at 293 K and 5 MPa, respectively (Y.-Y. Liu et al., 2007).

Researchers investigated the influence of Pt incorporation into MOF-177 framework. The H<sub>2</sub> adsorption capacity of Pt incorporated MOF-177 increased to 2.5 wt.% at 144 bar and 298 K. However, after several cycles of adsorption-desorption, its H<sub>2</sub> adsorption capacity decreased, drastically (Proch et al., 2008). Moreover, researchers tested the influence of Pt doping on the H<sub>2</sub> adsorption capacity of IRMOF-8. Pt-doped IRMOF-8 achieved a H<sub>2</sub> adsorption capacity of 0.85 wt.% at 10 MPa and 298 K while IRMOF-8 possessed a H<sub>2</sub> adsorption capacity of 0.44 wt.% at 298 K and 100 bar (Henrietta W Langmi, Ren, North, Mathe, & Bessarabov, 2014). Researchers examined the influence of embedding Pd nanoparticles into the pores of MIL-100(Al). Embedding Pd nanoparticles enhanced the H<sub>2</sub> adsorption capacity of MIL-100(Al) by a factor of 1.8 to 0.35 wt.% (298 K and 40 bar) (Zlotea et al., 2010).

Researchers incorporated metal hydrides into the pores of MOF framework to increase the achieved H<sub>2</sub> adsorption capacities. For instance, Mg nanocrystals were embedded into SNU-90' which enhanced the H<sub>2</sub> adsorption capacity of SNU-90' to 0.54 wt.%. (298 K and 90 bar). The enhanced H<sub>2</sub> adsorption capacity was due to the synergistic effect of physisorption and chemisorption (D.-W. Lim, Yoon, Ryu, & Suh, 2012).

In conclusion, MOFs possess high H<sub>2</sub> adsorption capacities (6 to 15 wt.%) at 77 K and high pressures with fast hydrogen release kinetics. However, for MOFs to be used as

hydrogen storage systems in light-duty fuel cell vehicles, the DOE target of hydrogen storage should be met at 298 K and lower pressures. Studies show that H<sub>2</sub> adsorption capacities of MOFs decrease drastically when the H<sub>2</sub> adsorption studies are conducted at 298 K. The reported H<sub>2</sub> adsorption capacities at 298 K (0.5 wt.% to 1 wt. % 298) are lower than the DOE targets. Therefore, researchers put significant effort on the strategies that can enhance the H<sub>2</sub> adsorption capacities of MOFs measured at 298 K. For instance, open metal sites were introduced, strategies that involve framework catenation/interpenetration were tested, effects of hydrogen spillover were investigated, guest metal ions that can provide unsaturated metal sites were introduced, Pd or Pt nanoparticles were loaded, bridged spillover was tested, and hybrid MOF composites were synthesized. All these strategies show promising results with an enhancement in H<sub>2</sub> adsorption capacities. However, the proposed strategies are not sufficient enough to synthesize MOFs that can achieve the DOE target of hydrogen storage. Despite the given effort by various researchers, there is still room for improvement for the H<sub>2</sub> adsorption capacities of MOFs measured at 298 K. Researchers should focus on to develop a strategy that would form cost-effective MOFs with high specific surface areas, and large pore volumes with high isosteric heats of adsorption that can show optimal H<sub>2</sub> adsorption performances at 298 K.

## **2.6. Hierarchical Porous MOFs**

Hierarchical porous MOFs are developed to obtain enhanced performances and superior properties. Hierarchical porous MOFs can be used in various application areas, including adsorption, batteries, catalysis, electrocatalysts, energy storage and conversion, separation, sensors, solar cells and supercapacitor electrodes (Yue Hu et al., 2015; G. Huang et al., 2014; Jing Jiang, Zhang, & Ai, 2016; X.-J. Kong, Lin, Zhang, Zhang, & Lin, 2016; Q. Lin et al., 2015; T. Liu et al., 2015; Salunkhe, Kaneti, Kim, Kim, & Yamauchi, 2016; Wenjing Wang & Yuan, 2014; Xin Wang et al., 2016; Xi et al., 2013; L. Yan et al., 2017). By synthesizing hierarchical porous MOFs, a wide range of benefits such as high surface area, high pore volume, accessible space, shortened diffusion paths, low density, and interconnected porosity can be achieved.

Having only micropores on the pore structure is considered as a crucial disadvantage since micropores limit the mass transfer and diffusion properties of the material while having



a two-pore system offers the advantages of both micro- and mesopores. For instance, while micropores provide a high surface area and high pore volume; mesopores enhance the mass transport and diffusion properties, thus guest molecules can reach the active sites, easily (Vallet-Regi, Rámila, del Real, & Pérez-Pariente, 2001). Therefore, researchers put significant effort to develop strategies to increase the pore size and have mesoporosity in the pore structure. The strategies to increase the pore size are: i) ligand extension (Chong Liu, Li, & Rosi, 2012; Lykourinou et al., 2011); ii) surfactant templating (Pal & Bhaumik, 2013; Qiu, Xu, et al., 2008); iii) microwave-assisted synthesis (D.-Y. Hong, Hwang, Serre, Férey, & Chang, 2009); iv) solvent evaporation diffusion (Fang et al., 2007); v) ionic liquid emulsion route (Yueju Zhao et al., 2011); and vi) CO<sub>2</sub> expanded liquids (L. Peng et al., 2014b). However, a stable porosity cannot be achieved.

Ligand extension method has several disadvantages such that it is limited with synthesis conditions, pore size cannot be increased more than a certain size, framework collapses as the guest molecules are removed, and a close packed structure is formed. Moreover, some frameworks issue interpenetration which in turn results in decreased pore sizes and surface areas (D. Zhao et al., 2011a).

Researchers investigated a modulator-induced strategy that forms hierarchical pores. A metal, insufficient amount of ligand and a modulator are used in the synthesis. The main principle behind the use of a modulator is to form mesopores by the structural defects formed by the coordination of the modulator with the metal ions (G. Cai & Jiang, 2017a).

In the case of surfactant templating method, a chelating agent is used whose removal cause collapse of the framework.

Another method to introduce mesopores to the pore structure of MOFs is by the nanoparticle encapsulation and etching process which show promising results (W. Zhang et al., 2015).

In brief, hierarchical porous MOFs benefit from their high surface areas and high pore volumes. Moreover, their high porosity is available for the large molecules to diffuse and tunable pore sizes and pore shapes offer various advantages while enhancing the commercialization of MOFs. However, it is still a great challenge to control the synthesis of hierarchical porous MOFs, and there is limited knowledge of the influence of the synthesis parameters. Moreover, for the commercialization of MOFs, a template-free, easy, low-cost, reproducible and scalable synthesis procedure is necessary.

In conclusion, as the amount of micropores increases, a larger surface area will be achieved and there will be more active sites for adsorption while as the amount of mesopores increases, mass transport properties will be enhanced. Thus, combining the benefits of micro- and mesopores, hierarchical porous MOFs are promising candidates for a wide range of application and the commercialization of MOFs.

## Chapter III

### Effect of iron to benzene-1,4-dicarboxylic acid ratio on and synthesis temperature on the textural properties of hierarchical porous MIL-88Bs

In this chapter, a surfactant and template-free synthesis strategy to synthesize hierarchically porous MIL-88Bs is reported. The aggregated MIL-88B nanorods form textural mesoporosity whose size can be finely controlled by iron to benzene-1,4-dicarboxylic acid ratio (Fe:TPA) and synthesis temperature. For the first time in the literature, we report a detailed pore size distribution analysis and a mechanism that controls the size of textural pores by utilizing Fe:TPA ratio and synthesis temperature. Last but not least, by introducing hierarchical pores to the pore structure, a BET surface area (enhanced by 2.7 times), and total pore volume (enhanced by 4.1 times) that is higher than those of reported BET surface area, and total pore volume for MIL-88B are reported.

#### 3.1. Background

Highly crystalline and porous metal-organic frameworks (MOFs) are firstly reported by Yaghi and his coworkers in 1995. These highly porous materials are formed by linking metal ion or metal ion clusters with an organic linker (O M Yaghi et al., 1995). Length and the functionality of the linkers determine pore size and structure (Rowsell & Yaghi, 2004a). MOFs significantly benefit and come to forefront with their easy synthesis routes, highly porous and crystalline structure, high surface area, tunable pore structure, and their ability to be loaded with other elements and components without any changes in their topology (Rowsell & Yaghi, 2004a). Depending on the starting materials, structure of MOFs varies, and pore size and shape can be easily tuned specific to the application area. This makes MOFs promising in various applications such as energy storage, adsorption and separation studies, catalysis, sensors, drug delivery and luminescence (Adams et al., 2010; Y. S. Bae & Snurr, 2011; Corma et al., 2010; García-García et al., 2016; Latroche, Surblé, Serre, Mellot-Draznieks, Llewellyn, Lee, Chang, Sung, et al., 2006a; Jeongyong Lee et al., 2009; J. R. Li

et al., 2009, 2011; Jiewei Liu et al., 2014; Rieth et al., 2017; Saha, Chandra, Garai, & Banerjee, 2012; Jung Soo Seo et al., 2000; Taylor-Pashow et al., 2010; T. Zhang & Lin, 2014).

Solvothermal synthesis follows the working principle of Lewis acid-base reactions at which metal salts and organic ligands are mixed in a solvent and heated in an oven at high temperatures. Metal ions act as Lewis acids and deprotonated ligands are considered as Lewis bases. Solvothermal reactions are conducted at high temperatures to form amines which will deprotonate carboxylic acids. Synthesis conditions possess significant role on the produced MOF structures which determine whether bulk precipitation or single crystals will be formed (D. Zhao, Timmons, Yuan, & Zhou, 2011b).

MOFs that are considered as open structures are microporous crystalline materials. The short diffusion pathway of mesopores extend the use of MOFs in various application areas. In the presence of mesopores, molecules can diffuse faster and reach to the storage site easier (Y. Yue, Fulvio, & Dai, 2015). Therefore, even though micropores contribute to the surface area, it is necessary to have mesopores in the pore structure as well as the micropores (Y. Yue, Fulvio, et al., 2015).

To synthesize MOFs that consist both micro- and mesopores several synthesis strategies: i) ligand extension; ii) template directing strategy have been investigated. However, the challenges that methods possess, limited their use. Apparently, ligand extension method caused MOFs that are synthesized from large ligands to collapse after the removal of guest molecules which decreases the pore size of MOFs (Reineke, Eddaoudi, Moler, O'Keeffe, & Yaghi, 2000; Omar M. Yaghi, Li, Davis, Richardson, & Groy, 1998; Y. Yue et al., 2014, 2013a; Y. Yue, Fulvio, et al., 2015). In the meanwhile, even though hierarchical porous MOF structures can be formed by the template directing strategy, the necessity to remove the template makes this strategy challenging (Y. Yue et al., 2014, 2013a; Y. Yue, Fulvio, et al., 2015). Therefore, several researches have been conducted to overcome the challenges of these methods. A template free synthesis strategy that creates hierarchical pores has been investigated by several studies (X. Liu et al., 2015; L. Peng et al., 2014a; Y. Yue et al., 2013a) and found to be a facile alternative to ligand extension method and template directing synthesis strategy that creates hierarchical pores.

In this study, MIL-88B type MOF crystallites were synthesized by a perturbation assisted nanofusion synthesis strategy and the effect of iron to benzene-1,4-dicarboxylic acid

ratio (Fe:TPA) on the morphology and the textural properties of MIL-88B type MOF crystallites were investigated. To the best of our knowledge there has been no report showing the effect of Fe:TPA ratio on the morphology and textural properties of MIL-88B type MOF crystallites. With the aim of filling the missing gap in the literature, we have investigated and imaged the changes in the morphology and textural properties of MIL-88B type MOF crystallites when these crystallites were synthesized with different Fe:TPA ratio, determined the effect of Fe:TPA ratio on textural porosity, pore size distribution, and percentage of textural mesoporosity quantitatively. Pore volumes were estimated by t-plot method, and NLDFT method and pore size distribution analysis was conducted by NLDFT method. Structural changes were shown by XRD and FTIR analysis and morphology of the synthesized MIL-88B type MOF crystallites were imaged by SEM.

In conclusion, MIL-88B type MOF crystallites were synthesized successfully by a perturbation assisted nanofusion synthesis strategy that forms hierarchical pores. It is found that Fe:TPA ratio has control over the morphology and the textural porosity of MIL-88B type MOF crystallites. A high Fe:TPA ratio causes interparticle voids to widen and fraction of textural mesopores to increase. By the perturbation assisted nanofusion synthesis strategy, a BET surface area and a total pore volume that is higher than those of reported MIL-88B is achieved. Once and for all, the perturbation assisted nanofusion synthesis strategy is a cost effective and facile alternative to synthesize MIL-88B type MOF crystallites that consist both micro- and mesopores within their pore structure with enhanced BET surface area (by 2.7 times) (C. Gao, Chen, Quan, Yu, & Zhang, 2017), and total pore volume (by 4.05 times) (C. Gao et al., 2017).

### **3.2. Experimental**

Reproducibility of our method was tested by the repetitive synthesis and characterization analysis. Each hierarchical porous MIL-88B was synthesized for five times. The characterization analyses were repeated for five times. Average results of BET surface area, ultramicro-, micro-, uppermeso-, mesopore, and total pore volumes with calculated standard deviations were reported. The fractions of micro- and mesoporosity were estimated by the ratio of micro- and mesopore volume (NLDFT method) to total pore volume estimated by NLDFT method.

### 3.2.1. Materials

Chemicals were used as received, no further purification was required. Chemicals were purchased from Merck Millipore and Sigma Aldrich. As the metal source 98% pure, ACS Reagent grade, iron(III) chloride hexahydrate was used; 99.9% pure, HPLC grade, *N,N*-Dimethylformamide (DMF) was the main solvent used during the synthesis and 99.8% pure methanol was used during solvent exchange processes.

### 3.2.2. Synthesis of Hierarchical Porous MIL-88Bs

A template and surfactant-free synthesis strategy was used in the synthesis of hierarchical porous MIL-88Bs (Cao et al., 2016; Y. Yue et al., 2013a). An iron source ( $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ ) (3.4 mmol) and benzene-1,4-dicarboxylic acid (TPA) were dissolved in 80 mL of *N,N*-dimethylformamide (DMF). Quantity of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$  and benzene-1,4-dicarboxylic acid used during the synthesis can be found in Table 1. Prepared solution was mixed vigorously via a magnetic stirrer with a stirring rate of 800 rpm for an hour at 25 °C and the solution was then distributed into glass vials. Glass vials were heated for 2 days in an isothermal oven. Then the mother liquor was poured into falcon tubes (50 mL). Solutions and the precipitates were firstly, washed with DMF (3 times) and then washed with methanol (3 times). At the end of each washing step, products were centrifuged and then washed again. Later the products were heated at 100 °C under vacuum for 30 hours. Figure 4 illustrates the synthesis procedure.

Table 1. Abbreviations for the hierarchical porous MIL-88Bs synthesized at different temperatures with different Fe:BDC ratio.

| Hierarchical porous MIL-88Bs | Heating temperature (°C) | FeCl <sub>3</sub> .6H <sub>2</sub> O (mmol) | Benzene-1,4-dicarboxylic acid (mmol) |
|------------------------------|--------------------------|---------------------------------------------|--------------------------------------|
| MIL-88B-110-1                | 110                      | 3.4                                         | 3.4                                  |
| MIL-88B-110-3                | 110                      | 3.4                                         | 1.13                                 |
| MIL-88B-110-5                | 110                      | 3.4                                         | 0.68                                 |
| MIL-88B-130-1                | 130                      | 3.4                                         | 3.4                                  |
| MIL-88B-130-3                | 130                      | 3.4                                         | 1.13                                 |
| MIL-88B-130-5                | 130                      | 3.4                                         | 0.68                                 |
| MIL-88B-150-1                | 150                      | 3.4                                         | 3.4                                  |
| MIL-88B-150-3                | 150                      | 3.4                                         | 1.13                                 |
| MIL-88B-150-5                | 150                      | 3.4                                         | 0.68                                 |

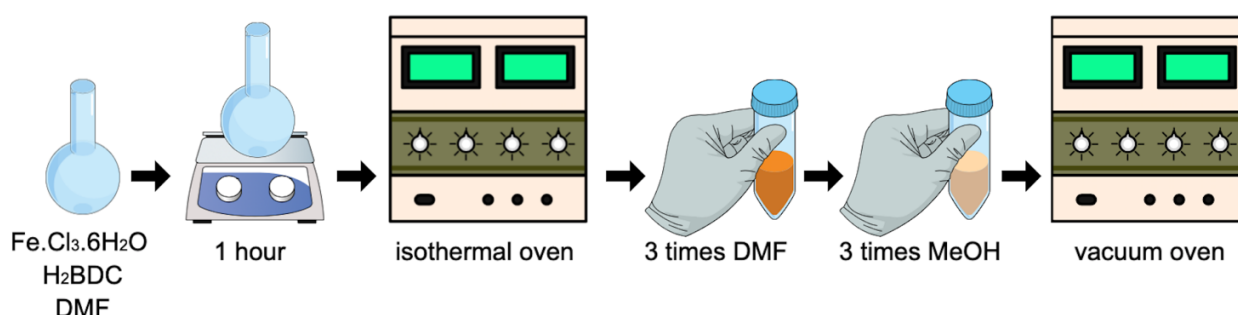


Figure 4. Schematic representation of experimental procedure.

### 3.2.2.1. Our approach

Different from the conventional crystallization process, a perturbation assisted nanofusion synthesis strategy was used in the synthesis of hierarchical porous MIL-88Bs. In a classic crystallization process a nuclei would form and then the unit-cell would replicate resulting in single crystal formation (Carné-Sánchez, Imaz, Stylianou, & MasPOCH, 2014). However, different from the conventional crystallization process FeCl<sub>3</sub>.6H<sub>2</sub>O, TPA and DMF

were vigorously stirred which prevented the single crystal growth. From the coordination of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$  and TPA, secondary building units (SBUs) form which later aggregate into nanosized MIL-88B type MOF crystallites (Cao et al., 2016; McNamara & Hicks, 2015; S. Yuan et al., 2017; Y. Yue et al., 2014, 2013a; Y. Yue, Fulvio, et al., 2015; Y. Yue, Zhang, et al., 2015). Interparticle voids present in between the aggregated nanosized MIL-88B type MOF crystallites form the textural mesoporosity. Figure 5 is a schematic of conventional crystallization process and nanofusion process.

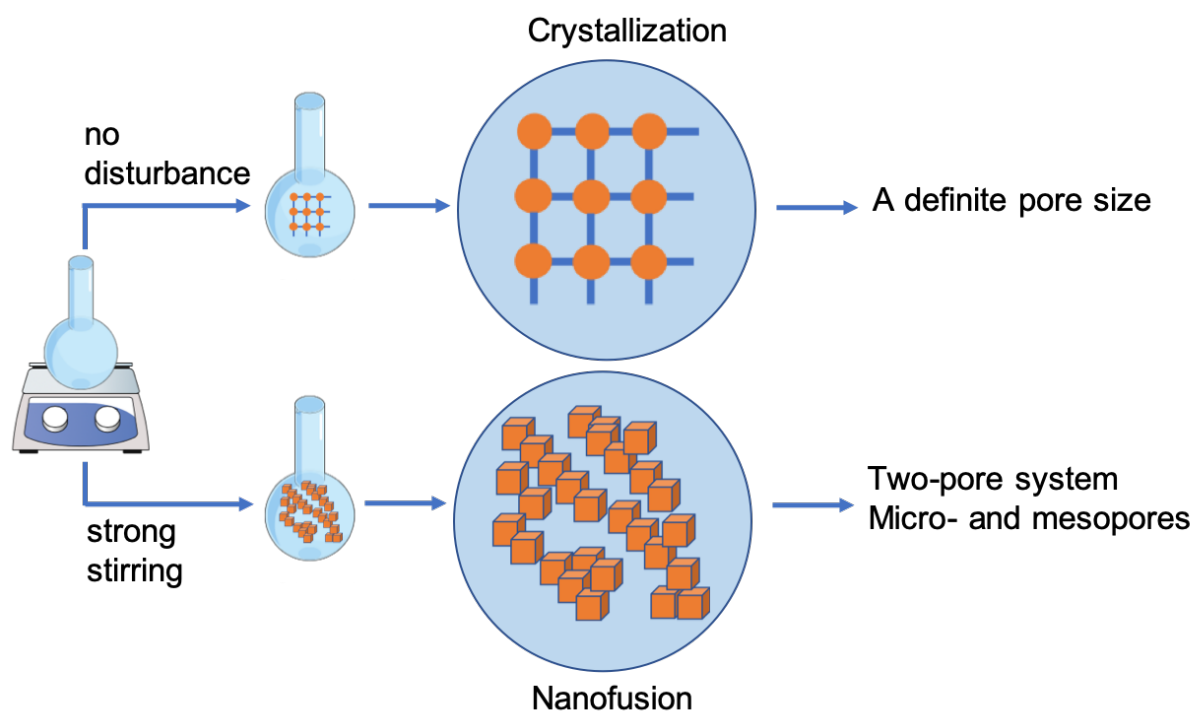


Figure 5. Schematic of conventional crystallization process and nanofusion

### 3.2.3. Characterization of Hierarchical Porous MIL-88Bs

$\text{N}_2$  sorption isotherms, pore size distribution analysis, powder x-ray diffraction (PXRD), thermogravimetric analysis (TGA), Fourier transform infrared spectroscopy (FTIR), and scanning electron microscopy (SEM) were used to characterize hierarchical porous MIL-88Bs. Gas sorption measurements were conducted by Intelligent Gravimetric Analyzer (IGA).



### **3.2.3.1.X-Ray diffraction**

X-ray diffraction (XRD) analysis was performed at room temperature with a Bruker D8 Diffractometer (XRD Bruker AXS GmbH D8 Advance, Karlsruhe, Germany). Analysis was held with 0.15406 nm Cu K $\alpha$  radiation. During the analysis X-ray generator voltage and current were set to 40 kV and 5 mA, respectively. A scan range of 2 to 90° in 2 $\theta$  range was used while the step size was set to 0.02° and counter-time was adjusted to 2 seconds per step.

### **3.2.3.2.Scanning Electron Microscopy (SEM)**

Leo Supra 35VP field emission scanning electron microscope was used for imaging. Voltage was kept constant in between 2 to 4 keV depending on the hierarchical porous MIL-88Bs and the analysis was conducted with secondary electron imaging technique.

### **3.2.3.3.Brunauer-Emmett-Teller (BET) surface area and pore size distribution analysis**

Surface area and pore size distribution analysis were performed by Micromeritics 3Flex Instrument. N<sub>2</sub> adsorption isotherms were obtained at 77 K. Prior to each analysis, samples were degassed to remove the present impurities at 120 °C for 6 hours. For each analysis 0.10 to 0.20 grams of sample was used. Surface area and pore size distribution analysis were performed by measuring liquid N<sub>2</sub> adsorption capacity at 77 K with a relative pressure range of 0.05 to 1 which monolayer coverage is assumed to be complete. For the measurement of surface area, BET model at which the main assumption is surface area is associated with the monolayer capacity, was used.

### **3.2.3.4.Fourier Transform Infrared Spectroscopy (FT-IR) Analysis**

FTIR analysis was conducted via Thermo Scientific Nicolet Is10 with a spectral resolution of 4 cm<sup>-1</sup> over a wavelength range of 600 to 4000 cm<sup>-1</sup>. Scans were repeated for 32 times and spectrum were corrected for the background noise.

### 3.2.3.5. Thermogravimetric Analysis (TGA)

Hierarchical porous MIL-88Bs were thermally analysed by Shimadzu DTG-60H simultaneous thermal analysis TG-DTA equipment. Hierarchical porous MIL-88Bs were kept under a continuous flow of 20 mL/min N<sub>2</sub> gas. Heating rate was set to 10 K/min and TGA curves were obtained by heating the samples from 25 °C to 1200 °C under 20 mL/min continuous flow of N<sub>2</sub> gas.

## 3.3. Results and Discussion

### 3.3.1. XRD Analysis

XRD patterns of hierarchical porous MIL-88Bs can be found below in Figure 6-20.

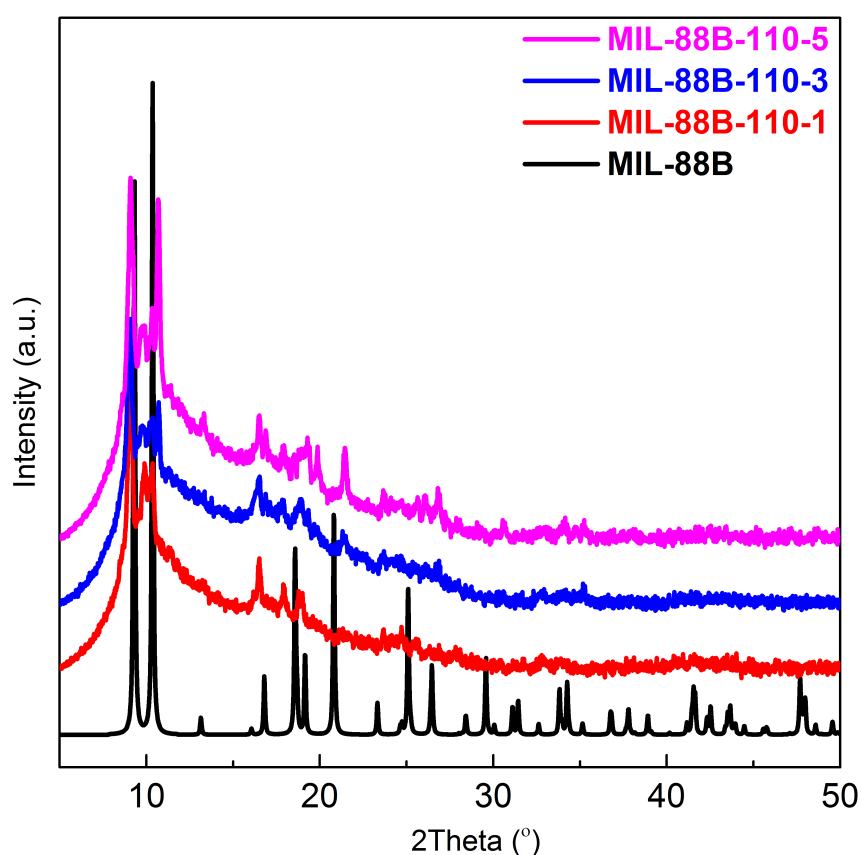


Figure 6. XRD patterns of the simulated MIL-88B, and the hierarchical porous MIL-88Bs synthesized at 110 °C.

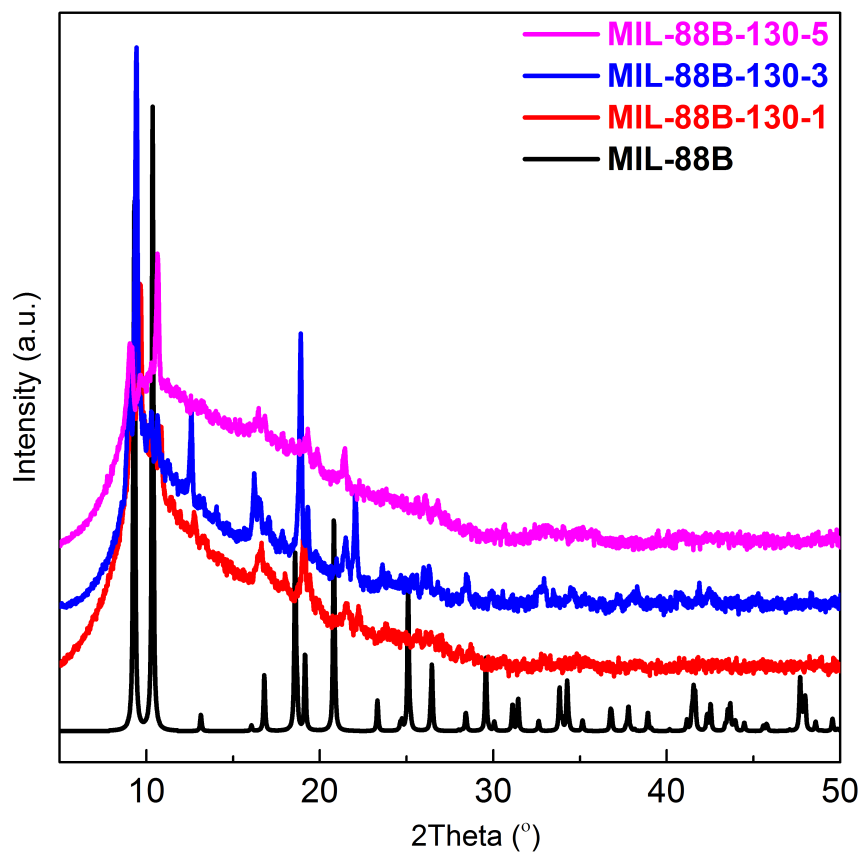


Figure 7. XRD patterns of the simulated MIL-88B, and the hierarchical porous MIL-88Bs synthesized at 130 °C.

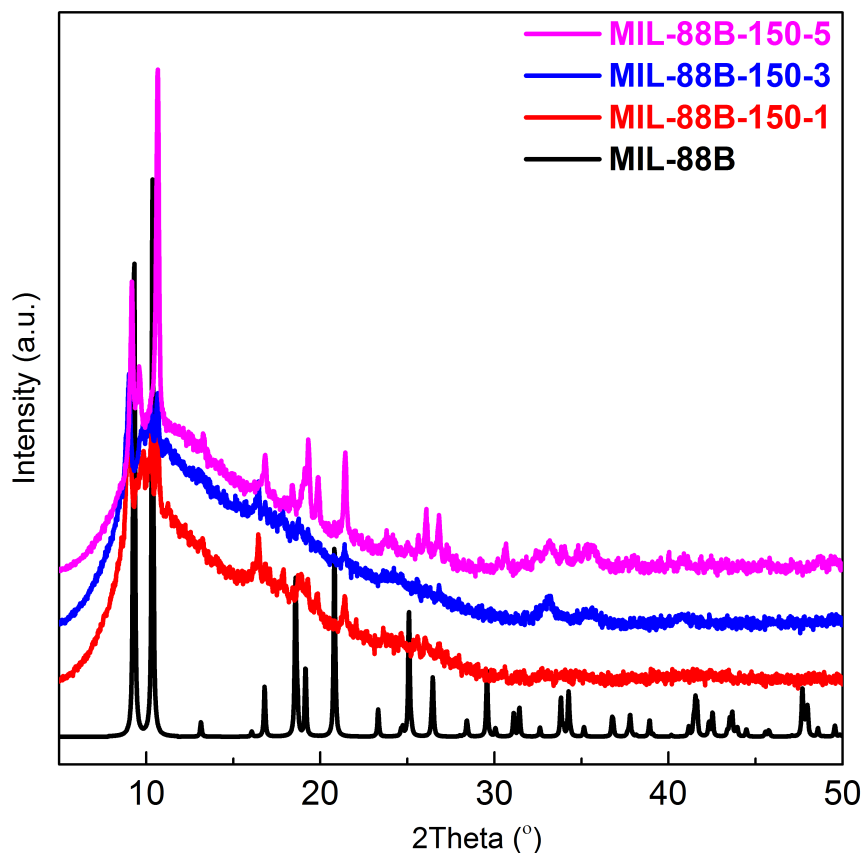


Figure 8. XRD patterns of the simulated MIL-88B, and the hierarchical porous MIL-88Bs synthesized at 150 °C.

3D crystal model of MIL-88B was simulated to obtain the powder XRD pattern of MIL-88B. XRD patterns of hierarchical porous MIL-88Bs synthesized via a perturbation assisted nanofusion strategy matched well with the XRD pattern of MIL-88B. Comparison of XRD patterns of the synthesized hierarchical porous MIL-88Bs and the XRD pattern of the simulated MIL-88B can be found below in Figure 9-20.

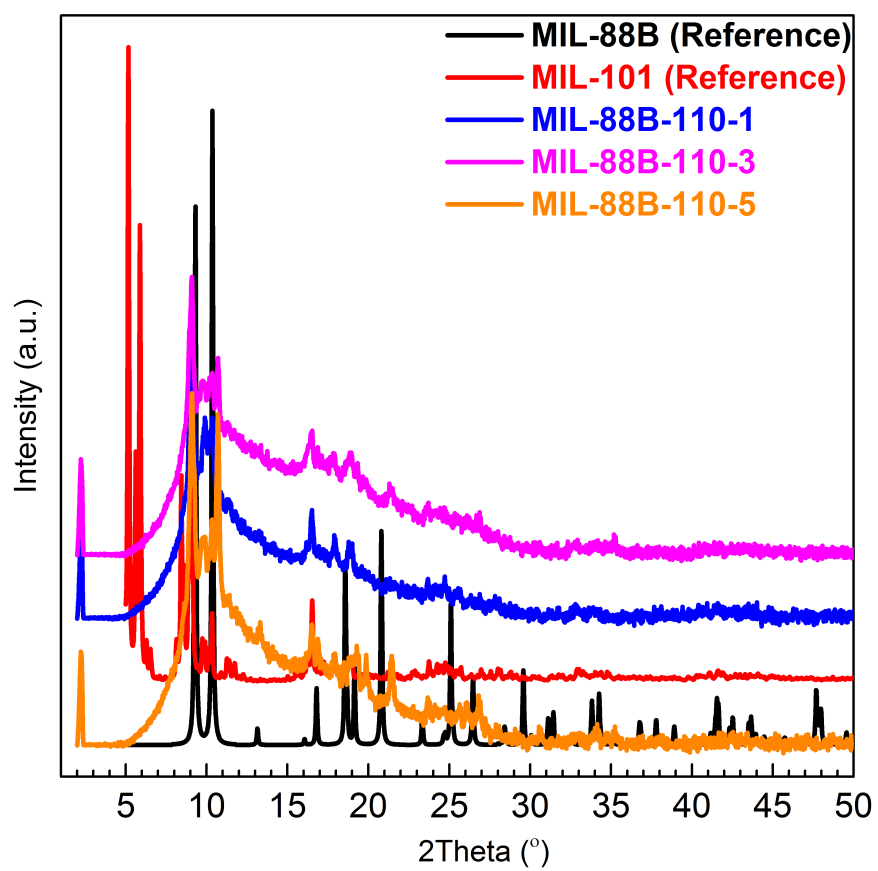


Figure 9. Comparison of XRD patterns of the simulated MIL-88B, MIL-101, and the hierarchical porous MIL-88Bs synthesized in this study.

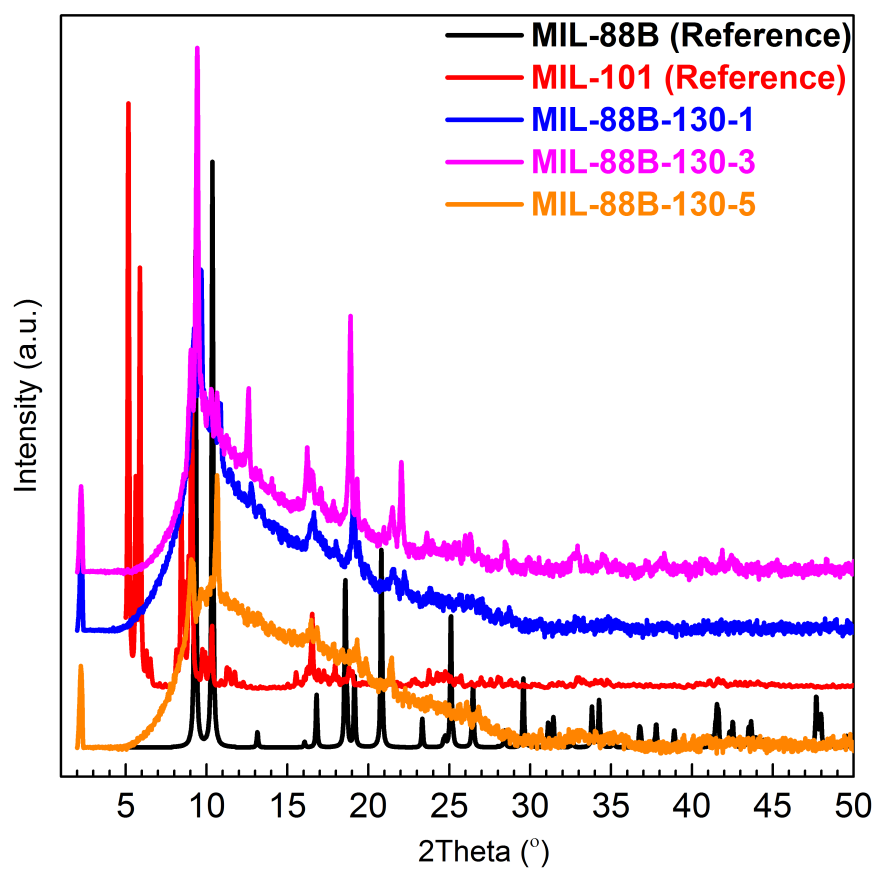


Figure 10. Comparison of XRD patterns of the simulated MIL-88B, MIL-101, and the hierarchical porous MIL-88Bs synthesized in this study.

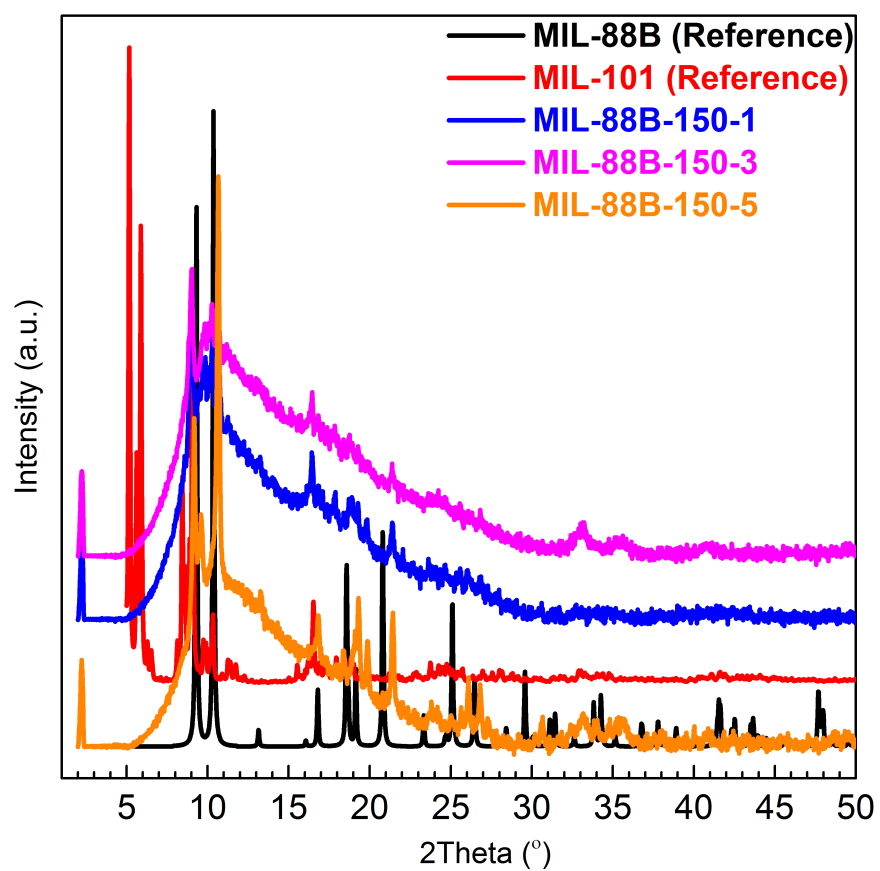


Figure 11. Comparison of XRD patterns of the simulated MIL-88B, MIL-101, and the hierarchical porous MIL-88Bs synthesized in this study.

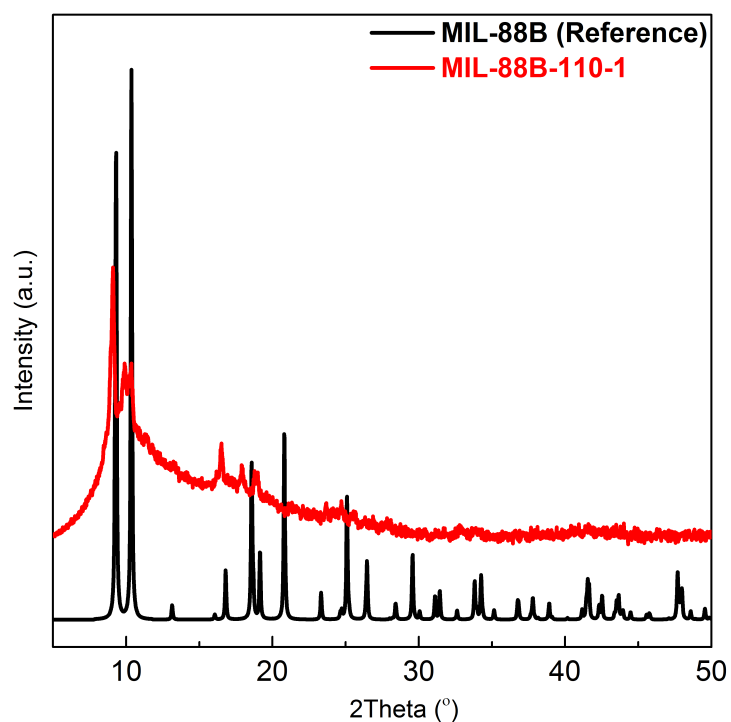


Figure 12. Comparison of XRD patterns of the simulated MIL-88B, and the hierarchical porous MIL-88B-110-1 synthesized in this study.

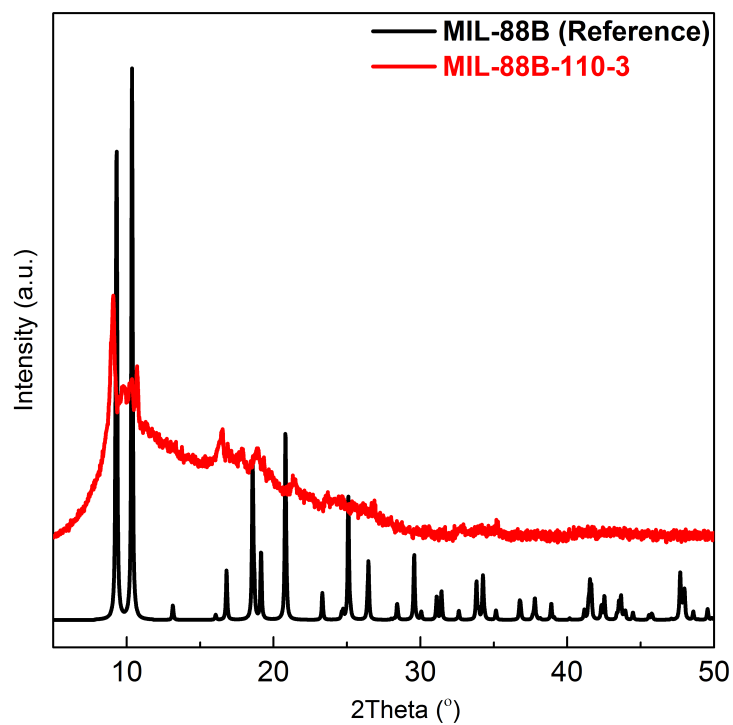


Figure 13. Comparison of XRD patterns of the simulated MIL-88B, and the hierarchical porous MIL-88B-110-3 synthesized in this study.



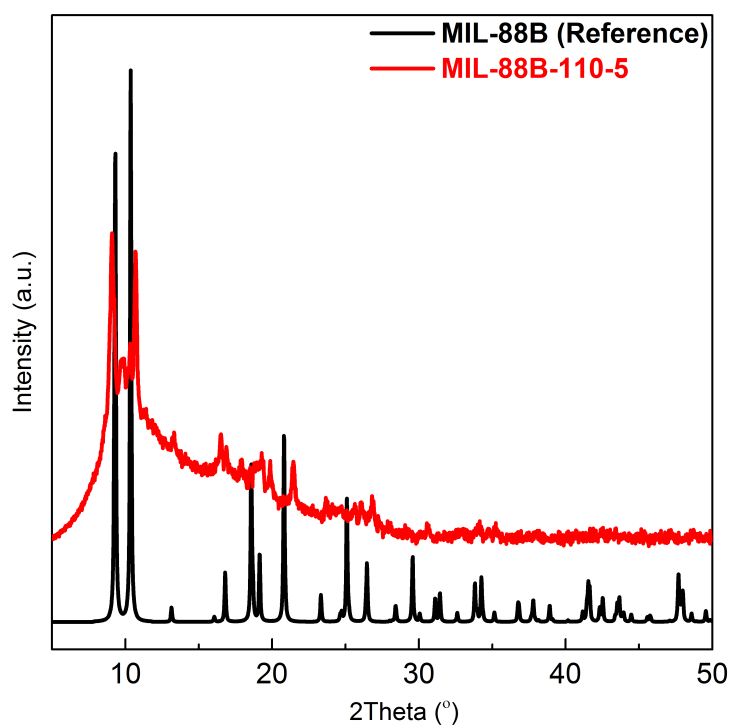


Figure 14. Comparison of XRD patterns of the simulated MIL-88B, and the hierarchical porous MIL-88B-110-5 synthesized in this study.

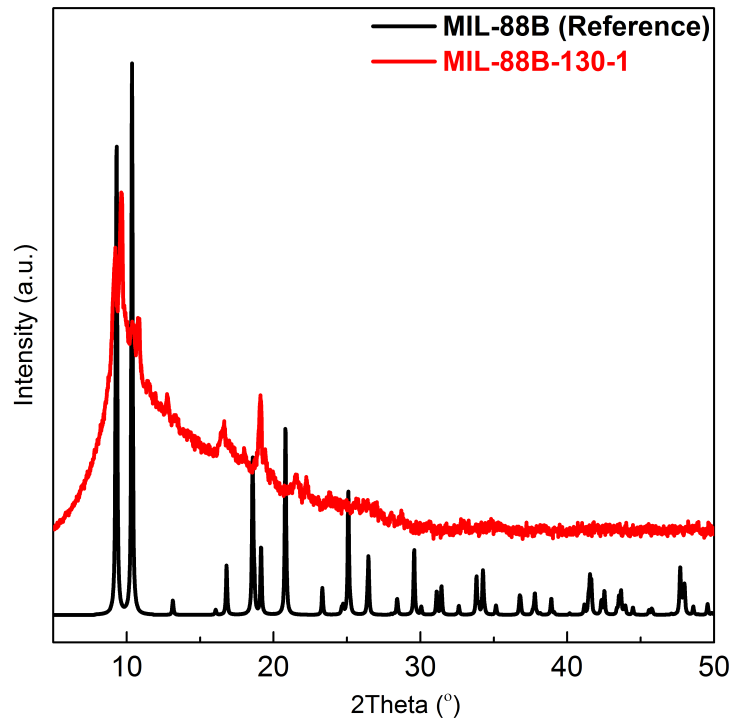


Figure 15. Comparison of XRD patterns of the simulated MIL-88B, and the hierarchical porous MIL-88B-130-1 synthesized in this study.

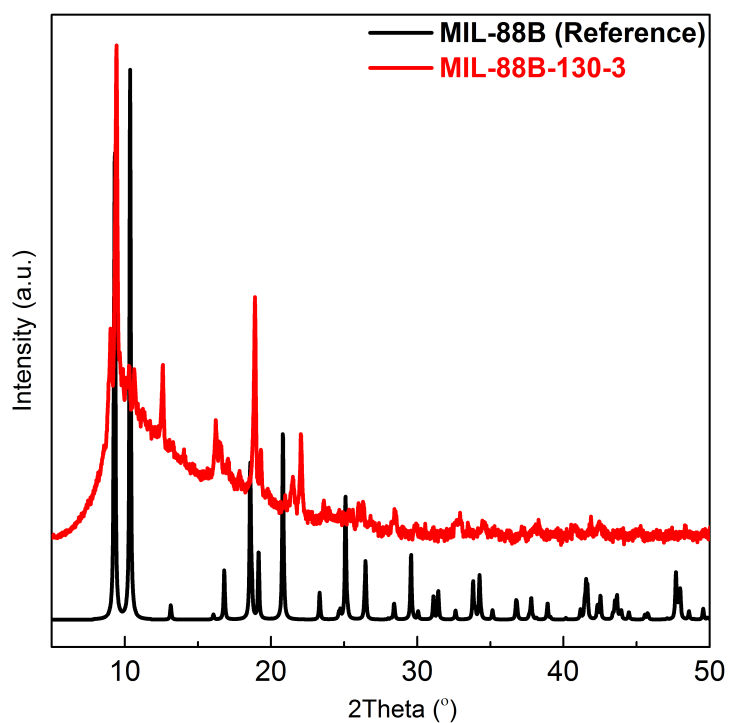


Figure 16. Comparison of XRD patterns of the simulated MIL-88B, and the hierarchical porous MIL-88B-130-3 synthesized in this study.

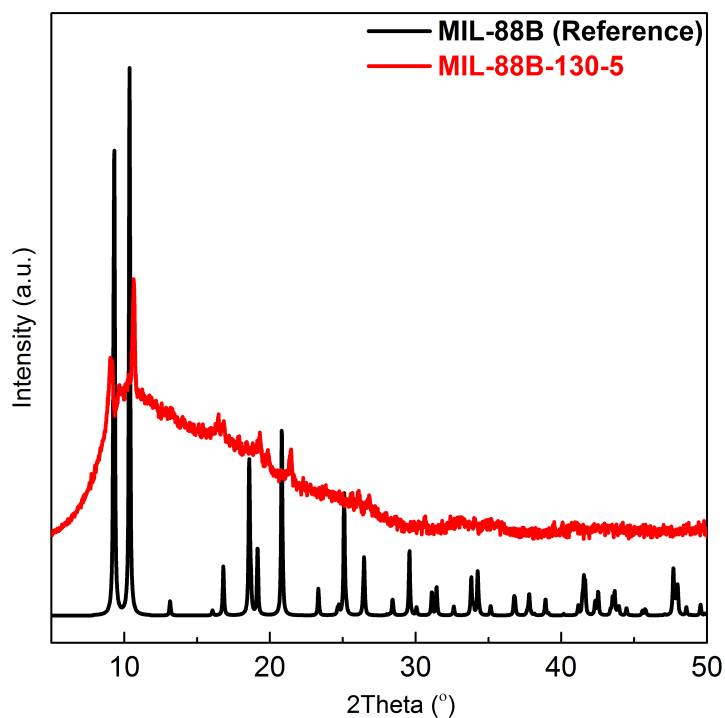


Figure 17. Comparison of XRD patterns of the simulated MIL-88B, and the hierarchical porous MIL-88B-130-5 synthesized in this study.

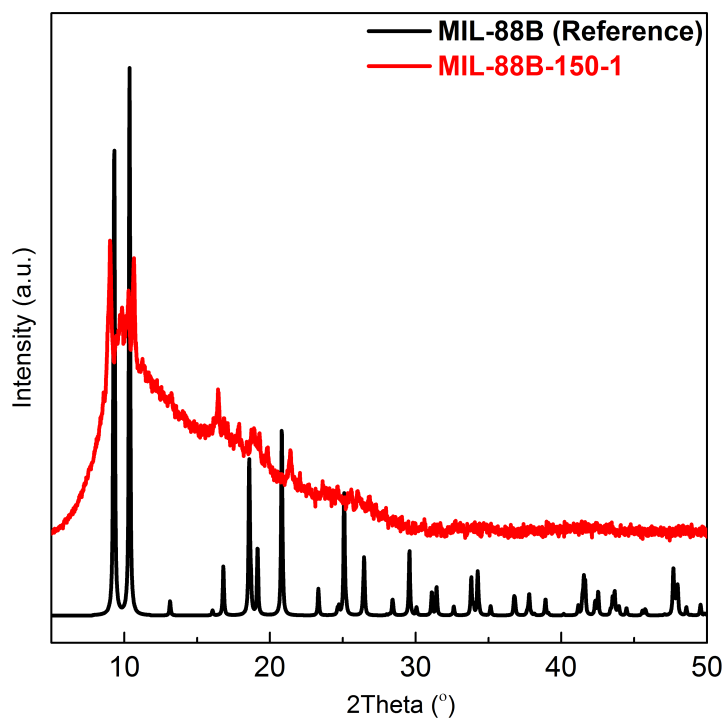


Figure 18. Comparison of XRD patterns of the simulated MIL-88B, and the hierarchical porous MIL-88B-150-1 synthesized in this study.

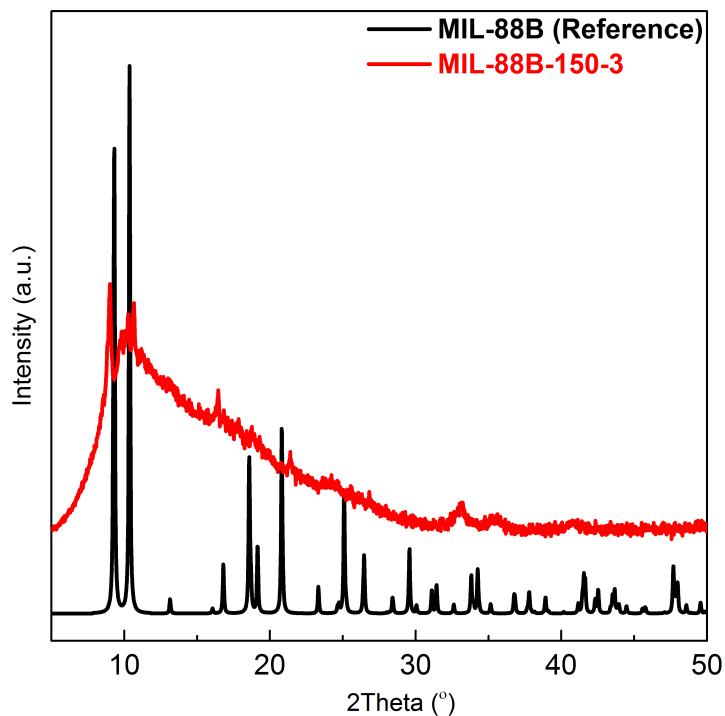


Figure 19. Comparison of XRD patterns of the simulated MIL-88B, and the hierarchical porous MIL-88B-150-3 synthesized in this study.

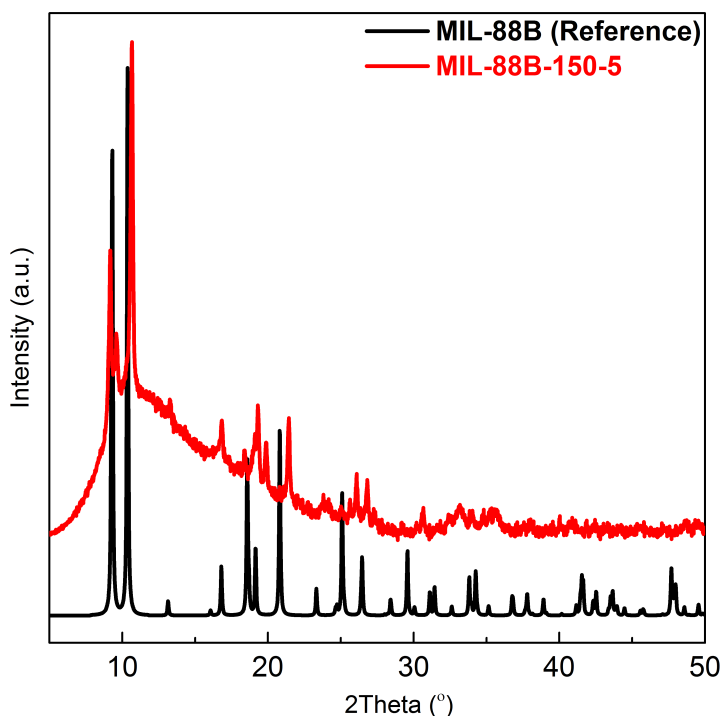


Figure 20. Comparison of XRD patterns of the simulated MIL-88B, and the hierarchical porous MIL-88B-150-5 synthesized in this study.

The well matched XRD patterns of hierarchical porous MIL-88Bs synthesized by the perturbation assisted nanofusion synthesis strategy and XRD pattern of the simulated MIL-88B confirm that by the perturbation assisted nanofusion synthesis strategy MIL-88B type MOF crystallites with hierarchical pores were synthesized successfully.

XRD patterns of hierarchical porous MIL-88Bs do not possess sharp peaks. Rather than sharp peaks, broadened Bragg peaks are observed. The perturbation assisted nanofusion synthesis strategy avoided the single crystal growth. Vigorous stirring of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ , TPA and DMF formed SBUs which later aggregated into nanosized MIL-88B type MOF crystallites. Broadening observed in Bragg peaks are attributed to the presence of nanosized MIL-88B rods which were embedded in an amorphous matrix (Cao et al., 2016).

A remarkable broadening was observed in the Bragg peaks of hierarchical porous MIL-88Bs synthesized with an Fe:TPA ratio of 5. This broadening is attributed to excess amount of iron salt present in the solution. By vigorously stirring  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ , TPA and DMF, SBUs were formed. Presence of excess amount of iron salt cause more iron oxide clusters to form which compete for TPA.

Hierarchically porous MIL-88Bs are formed by the aggregation of nanosized MIL-88B rods. Using a high Fe:TPA ratio cause more iron clusters to form which results in widened interparticle voids (textural mesopores). We have attributed the broadened Bragg peaks of hierarchically porous MIL-88Bs synthesized with an Fe:TPA ratio of 5 to the excess amount of iron salt present in the solution which causes more iron clusters to form and result in widened textural mesopores.

Moreover, single crystal X-ray crystallography analyses were conducted with a Bruker APEXII Quazar Diffractometer. Analyses showed that micro-sized single crystals were not formed and there were no metallic-iron present.

### **3.3.2. SEM Analysis**

SEM images of hierarchically porous MIL-88Bs can be found below in Figure 21-23. It is found that Fe:TPA ratio has control over the morphology of the hierarchically porous MIL-88Bs. Hierarchically porous MIL-88Bs are formed by the agglomeration of nanosized MIL-88B rods. The vigorous stirring of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ , TPA, and DMF formed nanosized MIL-88B rods. The amorphous matrix is formed by the Fe TPA coordination. SEM images clearly show the aggregated nanosized MIL-88Bs and the textural mesopores formed in between the aggregated particles.

As Fe:TPA ratio increases, higher number of iron oxide clusters form which aggregate into MIL-88B nanorods, and the interparticle voids (textural pores) widen. Particularly, interparticle voids created by the agglomeration of the MIL-88B nanorods are wider in H-150-5 which is attributed to the excess amount of iron salt present in the solution. Iron oxide clusters form just before the formation of SBUs and cause widened textural mesopores to form.

Figure 21 shows the SEM images of MIL-88B-110-1, MIL-88B-110-3, and MIL-88B-110-5. Figure 22 illustrates the SEM images of MIL-88B-130-1, MIL-88B-130-3, and MIL-88B-130-5 and figure 23 represents the SEM images of MIL-88B-150-1, MIL-88B-150-3, and MIL-88B-150-5.

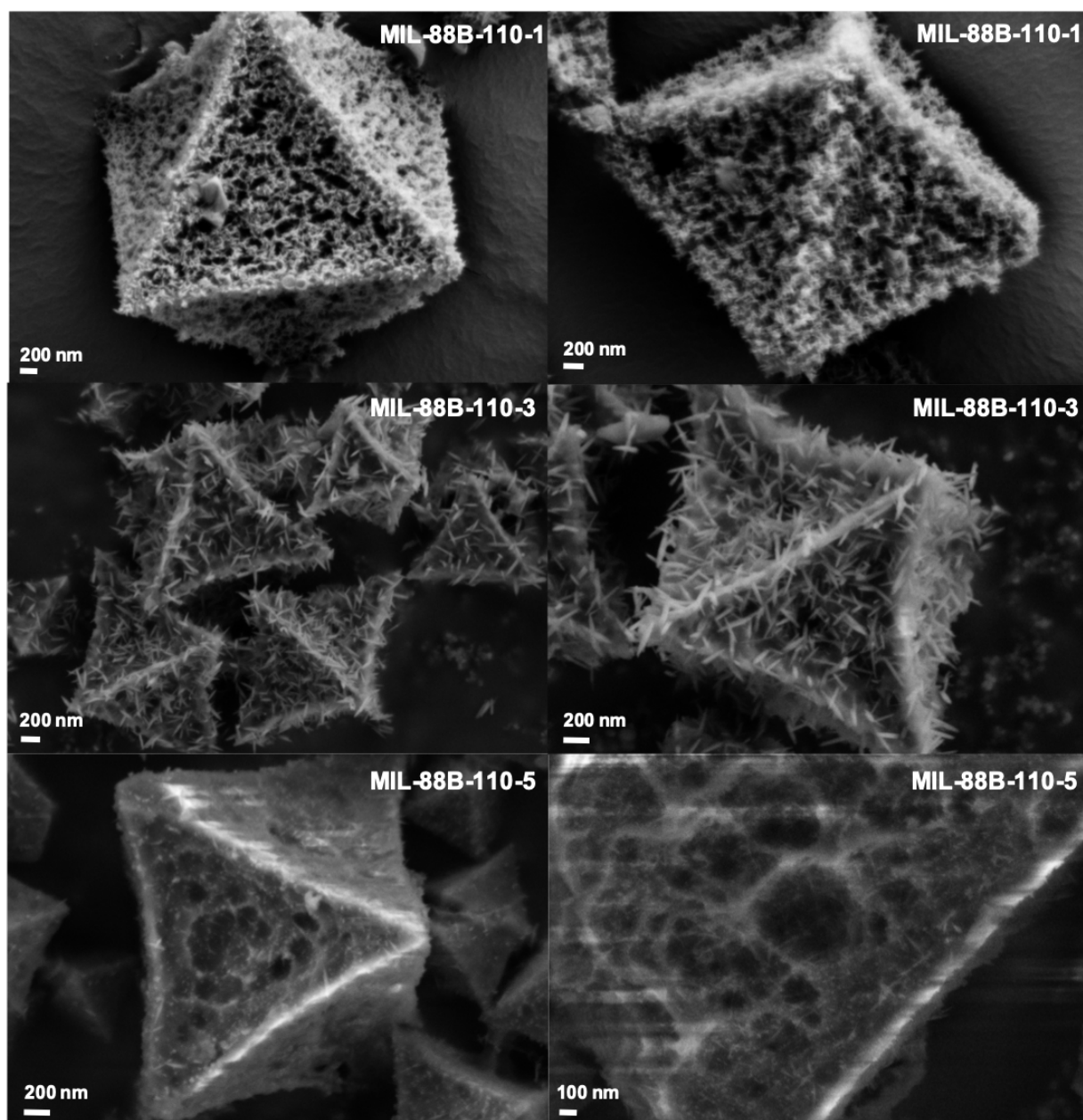


Figure 21. SEM images of MIL-88B-110-1, MIL-88B-110-3, and MIL-88B-110-5.

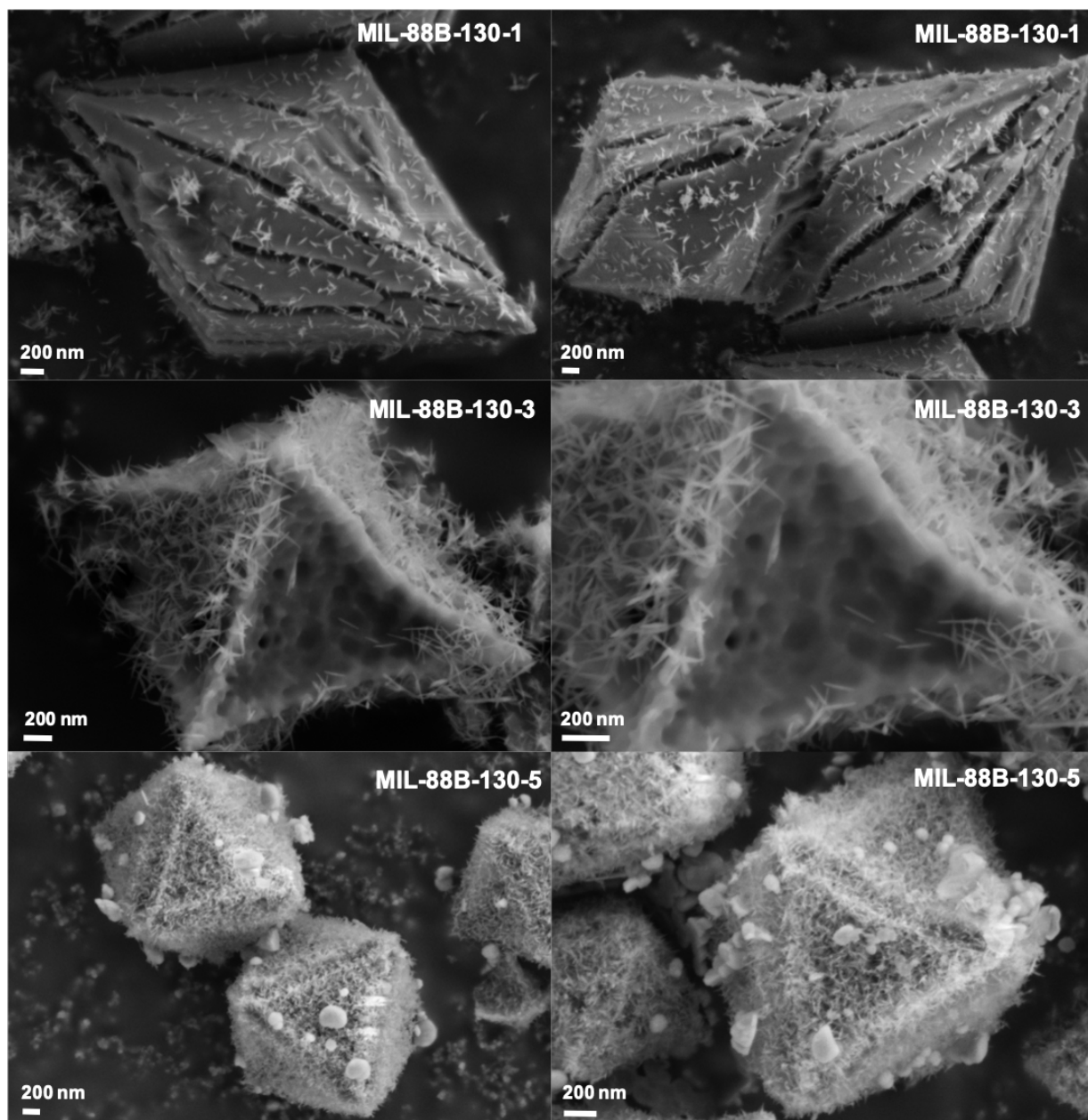


Figure 22. SEM images of MIL-88B-130-1, MIL-88B-130-3, and MIL-88B-130-5.

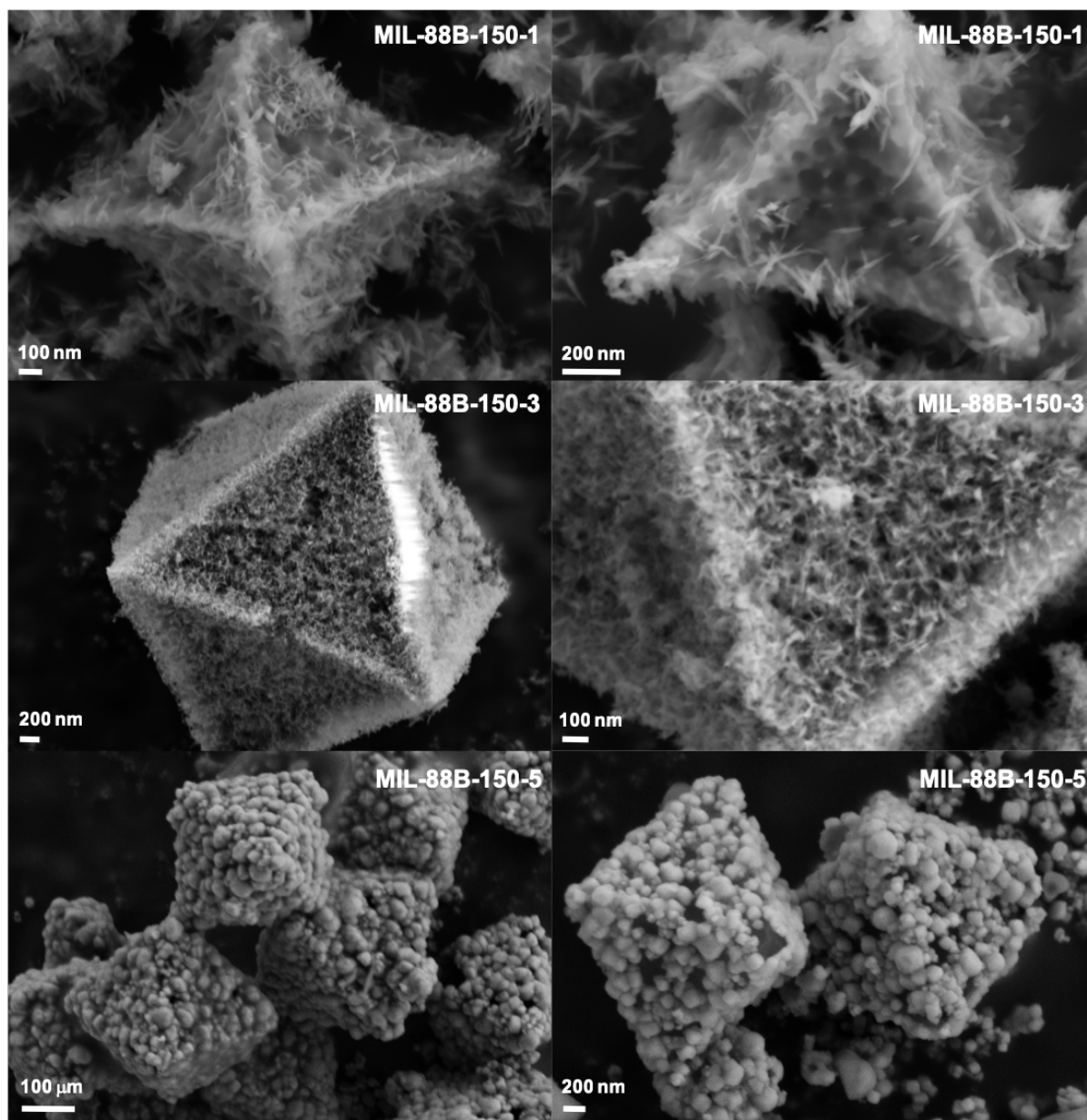


Figure 23. SEM images of MIL-88B-150-1, MIL-88B-150-3, and MIL-88B-150-5.

SEM images show the amorphous matrix at which nanosized MIL-88B nanorods were embedded in and the interparticle voids (textural mesopores) created in between the aggregated nanosized MIL-88Bs.

As Fe:TPA ratio increases, more iron clusters form which aggregates into nanosized MIL-88B rods, and the interparticle voids (textural pores) widen. Particularly, interparticle voids created by the agglomeration of nanosized MIL-88B rods are wider in MIL-88B-150-5 which is attributed to the excess amount of iron salt present in the solution. Iron oxide



clusters form just before the formation of SBUs and cause widened textural mesopores to form.

### 3.3.3. N<sub>2</sub> Sorption Isotherms

BET surface area estimations are made by the N<sub>2</sub> sorption analysis conducted at 77 K within the relative pressure range of 0.05 to 0.2. IUPAC classification of physisorption isotherms were used to classify the N<sub>2</sub> sorption isotherms (Thommes et al., 2015). N<sub>2</sub> sorption isotherms of hierarchically porous MIL-88Bs synthesized at different temperatures with different Fe:TPA ratio are shown below in Figure 24.

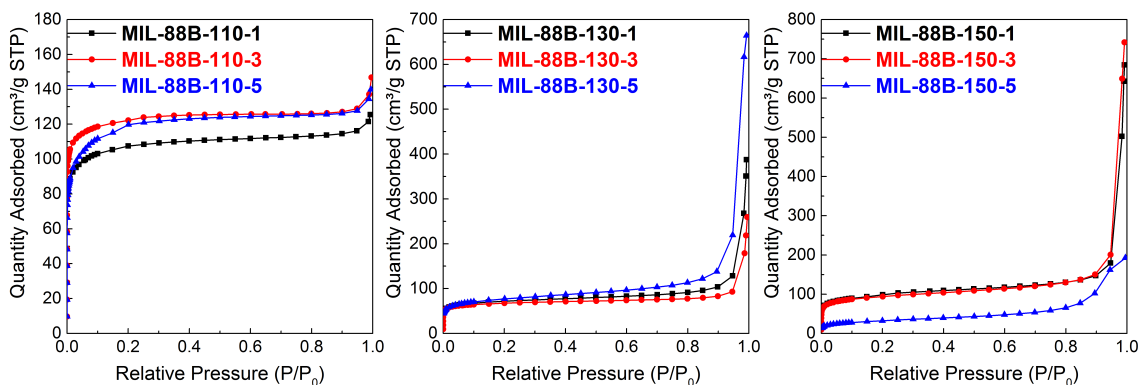


Figure 24. N<sub>2</sub> sorption isotherms of hierarchically porous MIL-88Bs.

Hierarchically porous MIL-88Bs synthesized at different temperatures with different Fe:TPA ratio show differences in their N<sub>2</sub> sorption behaviors. For a better analysis, we have divided the isotherm into following regions: (i)  $P/P_0 < 0.2$ , (ii)  $0.2 < P/P_0 < 0.9$ , and (iii)  $0.9 < P/P_0 < 1$ .

N<sub>2</sub> sorption isotherms of hierarchically porous MIL-88Bs synthesized at 110 °C with Fe:TPA ratio of 1, 3, and 5 represents typical features of IUPAC type I isotherms with some mesoporosity present. Figure 25 illustrates the N<sub>2</sub> sorption isotherms of MIL-88B-110-1, MIL-88B-110-3, and MIL-88B-110-5.

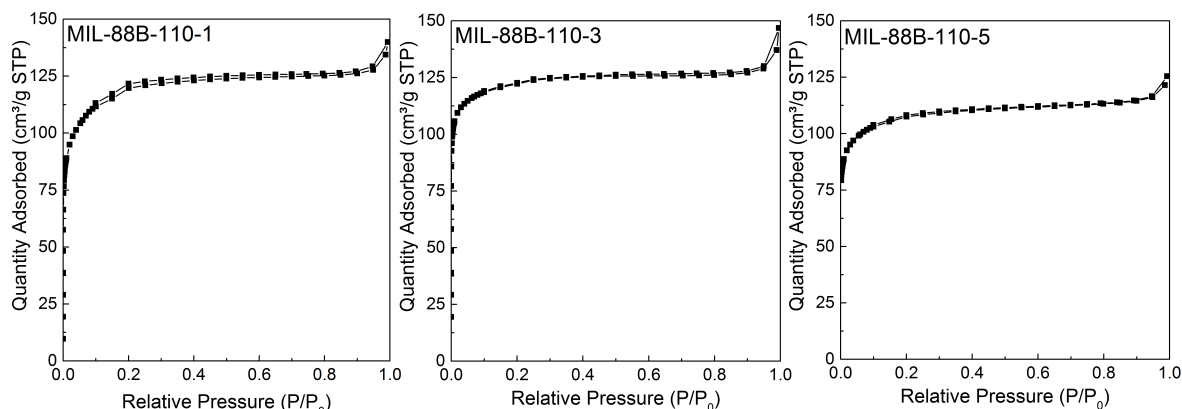


Figure 25. N<sub>2</sub> sorption isotherms of MIL-88B-110-1, MIL-88B-110-3, and MIL-88B-110-5.

N<sub>2</sub> sorption isotherms of hierarchically porous MIL-88Bs synthesized at 110 °C with an Fe:TPA ratio of 1, 3, and 5 differ from each other by their knee shapes, initial point of plateau, and amount of N<sub>2</sub> uptake at low relative pressures. At low relative pressures (i)  $P/P_0 < 0.1$ , N<sub>2</sub> uptake has a sharp increase which is a consequence of micropore filling. The sharpest increase is observed in MIL-88B-110-3, while MIL-88B-110-5 shows the lowest one. This steeper uptake is attributed to presence of narrower micropores. At region (ii) where relative pressure ranges between 0.2 and 0.9, isotherms become almost flat. Particularly, MIL-88B-110-3, has a flat horizontal plateau which confirms that micropores are completely filled and further N<sub>2</sub> uptake becomes limited. The isotherms of MIL-88B-110-1, and MIL-88B-110-5 still possess a relatively small slope within the region (ii) which is associated with mesopore filling. At region (iii) where relative pressure is close to saturation pressure, rise observed in N<sub>2</sub> uptake is attributed to presence of mesopores. Figure 26 shows the N<sub>2</sub> sorption isotherms of MIL-88B-130-1, MIL-88B-130-3, and MIL-88B-130-5.

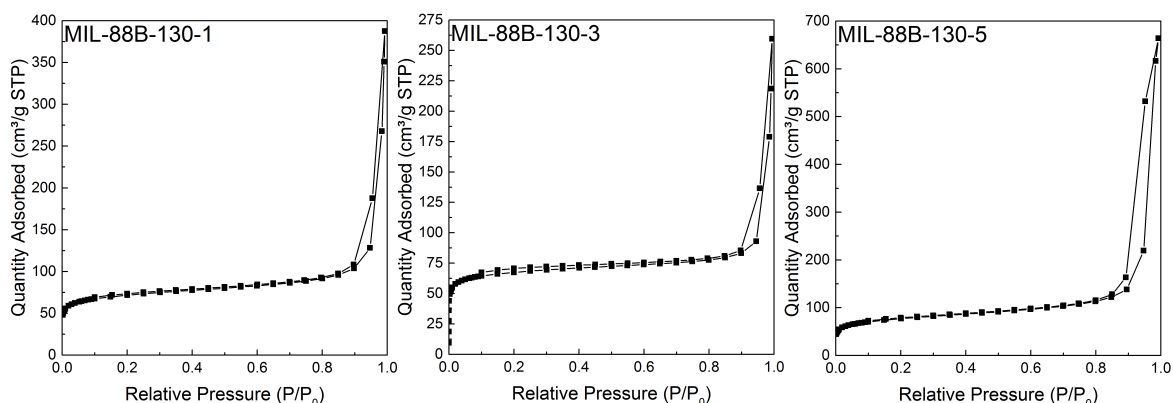


Figure 26. N<sub>2</sub> sorption isotherms of MIL-88B-130-1, MIL-88-130-3, and MIL-88B-130-5.

At low relative pressures, hierarchically porous MIL-88Bs synthesized at 130 °C possess sharp N<sub>2</sub> uptakes indicating the presence of micropores. MIL-88B-130-3 shows the steepest N<sub>2</sub> uptake which indicates the enhanced adsorbate-adsorbent interactions. At region (ii) N<sub>2</sub> sorption isotherm of MIL-88B-130-3 possesses a horizontal plateau which is neither observed in MIL-88B-130-1 nor observed in MIL-88B-130-5. Amount of N<sub>2</sub> uptake increases with increasing relative pressure which is a consequence of mesopore filling. At region (iii) steep increase observed in N<sub>2</sub> uptake is thought to be associated with interparticle capillary condensation. MIL-88B type MOF crystallites synthesized at 130 °C with Fe:TPA ratio of 1, 3, and 5 represents the major characteristics of IUPAC type IV isotherms with some micropores present. N<sub>2</sub> sorption isotherms of MIL-88B-150-1, MIL-88B-150-3, and MIL-88B-150-5 can be found in Figure 27.

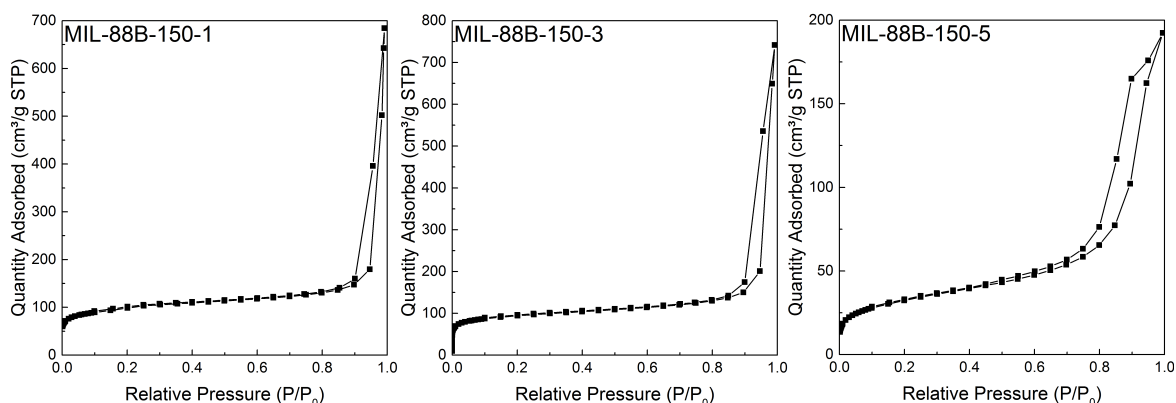


Figure 27. N<sub>2</sub> sorption isotherms of MIL-88B-150-1, MIL-88-150-3, and MIL-88B-150-5.

N<sub>2</sub> sorption isotherms of MIL-88B-150-1, MIL-88B-150-3, and MIL-88B-150-5 show the major characteristics of IUPAC type IV isotherms with some microporosity present. MIL-88B-150-1 and MIL-88B-150-3 have considerably higher N<sub>2</sub> uptakes at region

(i). These high nitrogen uptake capacities are associated with micropore filling suggesting the presence of micropores within the pore structure. At region (ii)  $N_2$  sorption isotherms of hierarchically porous MIL-88Bs synthesized with an Fe to TPA ratio of 1, 3, and 5 become nearly flat. However, a true horizontal plateau cannot be achieved. As relative pressure increases, a slope is observed which is associated with mesopore filling. At region (iii) a drastic increase in the amount of  $N_2$  adsorbed is observed in the  $N_2$  sorption isotherms of MIL-88B-150-1, and MIL-88B-150-3. This drastic increase at region (iii) is associated with interparticle capillary condensation and thereby confirms the presence of mesopores that possess sizes at the upper mesopore size range. The  $N_2$  sorption isotherm of MIL-88B-150-5 is very typical of mesoporous materials. At low pressures, monolayer-multilayer adsorption is observed. Then a plateau is achieved. This plateau is a consequence of limiting  $N_2$  uptake over a broad range of high relative pressure. At relative pressures lower than 0.6, a linear trend in  $N_2$  sorption isotherm is observed. A very significant hysteresis loop, which is associated with pore condensation, is observed as relative pressure increases from 0.4 to 1. Finally, a true horizontal plateau is achieved.

#### **3.3.4. t-plot Method**

t-plot given below (Figure 28-31) belongs to hierarchically porous MIL-88Bs synthesized at 110, 130, and 150 °C with different Fe:TPA ratio and represents the volume of  $N_2$  adsorbed with various statistical thickness.

Table 2. Micropore volume, slope, y-intercept, and correlation coefficient estimated by t-plot method.

| MOF           | Micropore Volume (cm <sup>3</sup> /g) | Slope (cm <sup>3</sup> /g.nm) <sup>[a]</sup> | Y intercept (cm <sup>3</sup> /g.nm) <sup>[a]</sup> | Correlation Coefficient |
|---------------|---------------------------------------|----------------------------------------------|----------------------------------------------------|-------------------------|
| MIL-88B-110-1 | 0.13±1.4E-2                           | 58.2±3.9                                     | 81.6±1.8                                           | 0.991                   |
| MIL-88B-110-3 | 0.15±3.4E-2                           | 54.9±2.0                                     | 98.2±8.0E-1                                        | 0.997                   |
| MIL-88B-110-5 | 0.114±3.2E-2                          | 101.6±7.5                                    | 74.1±3.0                                           | 0.989                   |
| MIL-88B-130-1 | 0.069±1.9E-2                          | 61.6±2.1                                     | 44.7±8.4E-1                                        | 0.998                   |
| MIL-88B-130-3 | 0.076±1.7E-2                          | 42.0±1.6                                     | 48.98±6.4E-1                                       | 0.997                   |
| MIL-88B-130-5 | 0.055±1.7E-2                          | 94.3±2.5                                     | 35.6±1.0                                           | 0.999                   |
| MIL-88B-150-1 | 0.063±1.7E-2                          | 131.8±1.8                                    | 40.9±7.0E-1                                        | 0.999                   |
| MIL-88B-150-3 | 0.077±1.7E-2                          | 101.5±2.5                                    | 49.5±1.0                                           | 0.999                   |
| MIL-88B-150-5 | 0.0054±1.0E-3                         | 13.0±6.3E-1                                  | 3.5±2.5E-1                                         | 0.995                   |

[a] At standard temperature and pressure (STP)

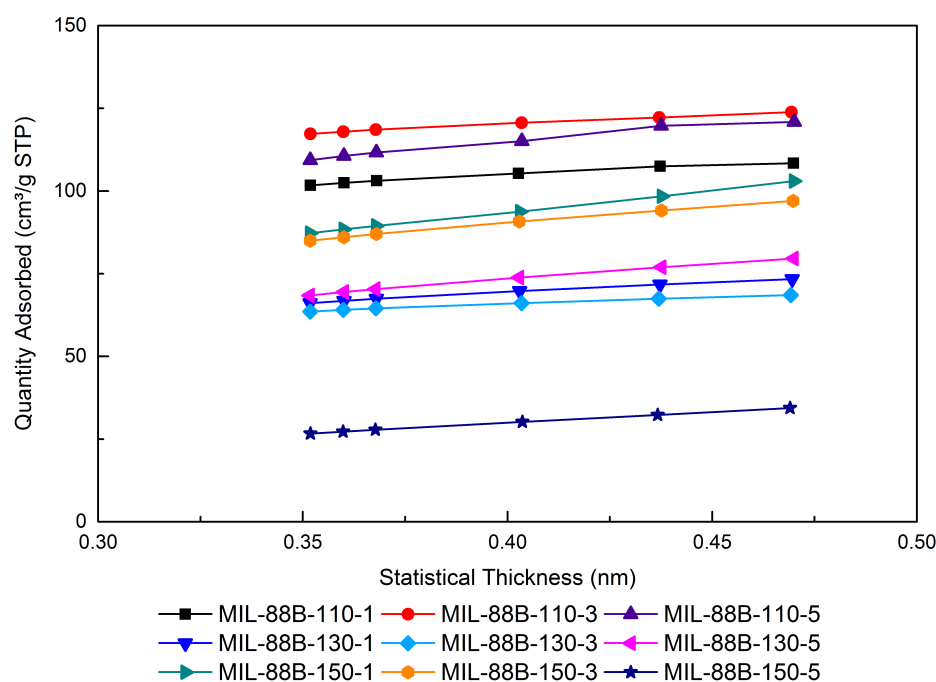


Figure 28. t-plots of hierarchically porous MIL-88Bs.

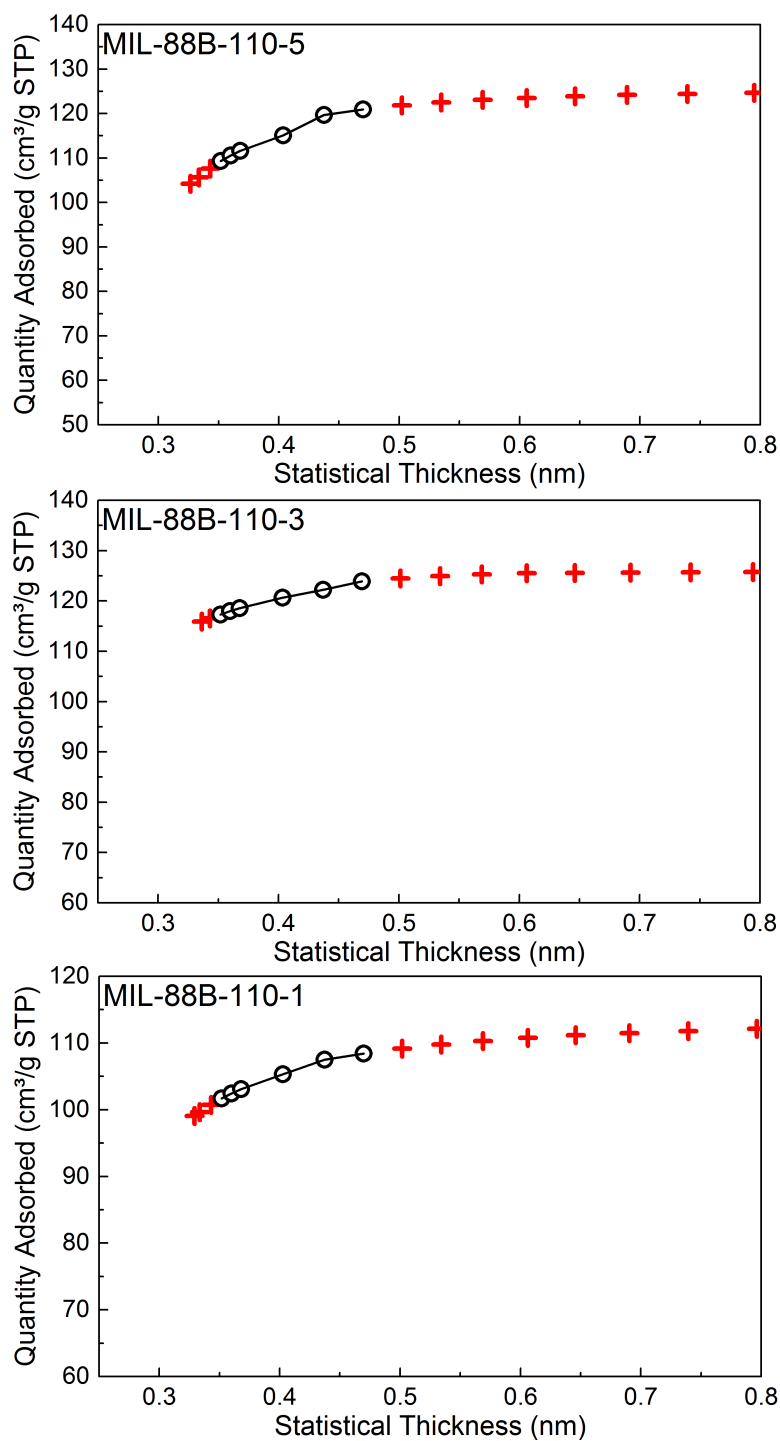


Figure 29. t-plots of MIL-88B-110-1, MIL-88B-110-3, and MIL-88B-110-5.

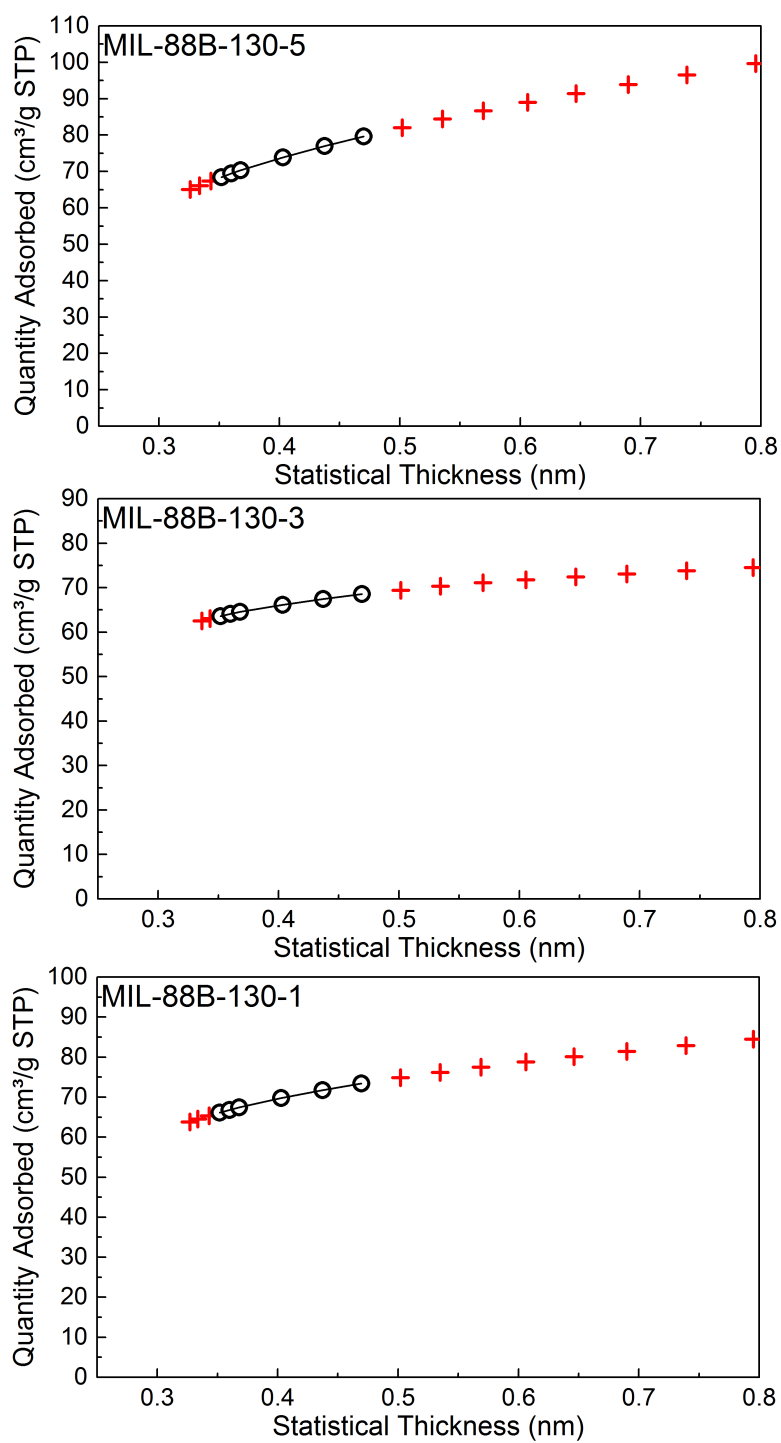


Figure 30. t-plots of MIL-88B-130-1, MIL-88B-130-3, and MIL-88B-130-5.

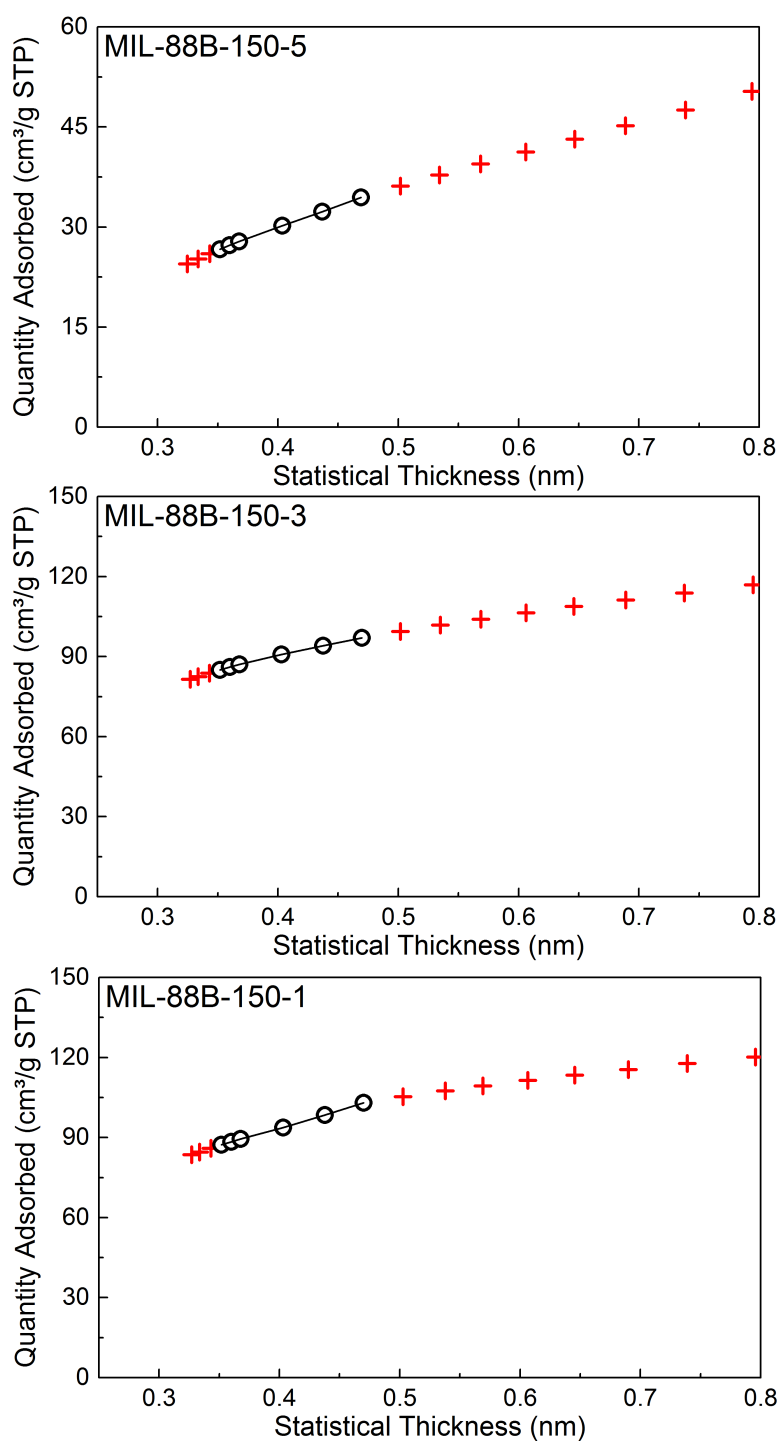


Figure 31. t-plots of MIL-88B-150-1, MIL-88B-150-3, and MIL-88B-150-5.

t-plots show significant differences in the micropore volumes of hierarchically porous MIL-88Bs synthesized at different temperatures with different Fe:TPA ratios. Hierarchically porous MIL-88Bs possess t-plots with positive intercepts which suggest that



micropores are present in the pore structure of these hierarchically porous MIL-88Bs. Dots deviate from the linear regime in the t-plots of hierarchically porous MIL-88Bs synthesized with an Fe:TPA ratio of 1, and 5 while t-plots of MIL-88B type MOF crystallites synthesized with an Fe:TPA ratio of 3 show a linear regime indicating that hierarchically porous MIL-88Bs synthesized with an Fe:TPA ratio of 3 are dominantly formed of micropores.

t-plots of hierarchically porous MIL-88Bs synthesized with an Fe:TPA ratio of 1, and 5 are formed of two linear parts which prove that mesopores are present as well as micropores. Intercept of hierarchically porous MIL-88Bs synthesized with an Fe:TPA ratio of 3 is significantly higher than the intercept of hierarchically porous MIL-88Bs synthesized with an Fe:TPA ratio of 1 and 5 indicating that hierarchically porous MIL-88Bs synthesized with an Fe:TPA ratio of 3 possess the highest micropore volume among the hierarchically porous MIL-88Bs synthesized with an Fe:TPA ratio of 1, 3, and 5. It is shown that textural mesoporosity increased drastically when the amount of linker used decreased.

### **3.3.5. NLDFT Method**

NLDFT method has a better description of the thermodynamics of the confined fluid and thereby, has the highest precision in pore size estimations (Lowell et al., 2004a). NLDFT plots of hierarchically porous MIL-88Bs show several increases within micro- and mesoporous region. In addition to the wide mesopores observed at 44.8 nm, some narrow mesopores are also tracked. Figure 32 and 33 illustrate the NLDFT plot of hierarchically porous MIL-88Bs synthesized at 110 °C.

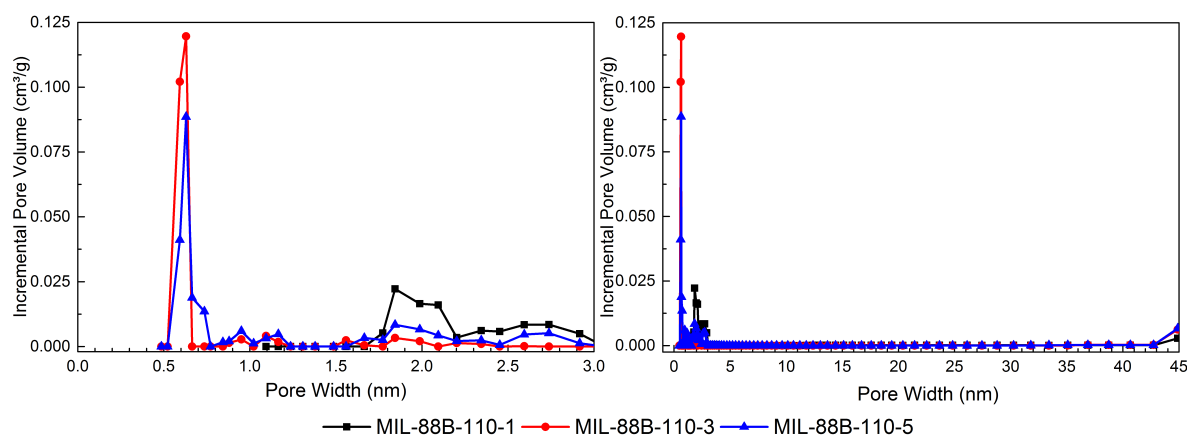


Figure 32. NLDFT plot of hierarchically porous MIL-88Bs synthesized at 110 °C.

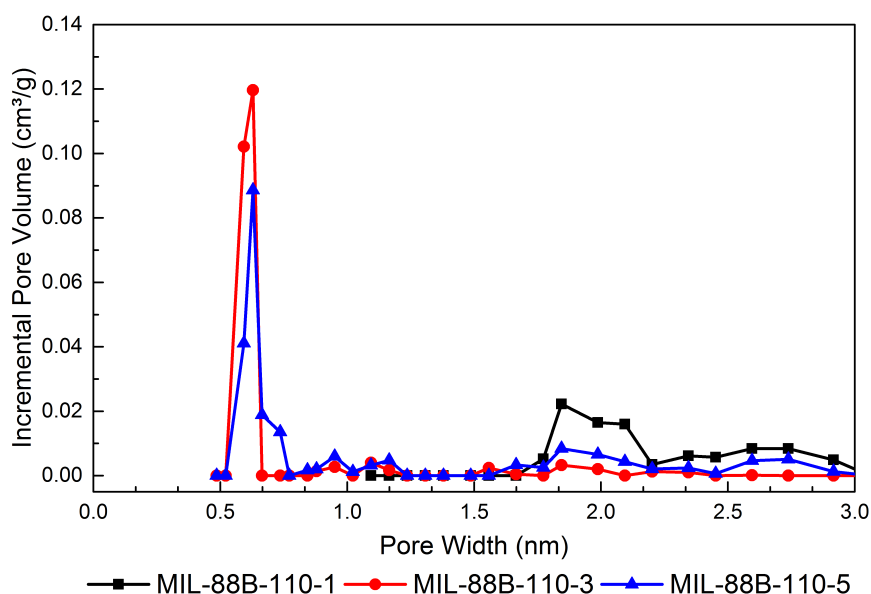


Figure 33. NLDFT plot of MIL-88B-110-1, MIL-88B-110-3, and MIL-88B-110-5.

NLDFT plots of hierarchically porous MIL-88Bs synthesized at 110 °C show sharp increases in microporous region while the increase in mesoporous region remains insignificant. The highest volume increase in microporous region is observed in MIL-88B-110-3 at which micropores contribute significantly to the total pore volume (96.1%). Total pore volume of MIL-88B-110-1 is measured to be 0.199 cm<sup>3</sup> in which micropores occupy 0.182 cm<sup>3</sup>/g of volume. Identical to MIL-88B-110-3, MIL-88B-110-5 has no pores narrower than 0.593 nm. Micropores present in MIL-88B-110-5 occupy a volume of 0.202 cm<sup>3</sup>/g which corresponds to 87.8% of the total pore volume while micropores of MIL-88B-110-3

possess  $0.24 \text{ cm}^3/\text{g}$  of volume that corresponds to 96.1% of the total pore volume. Figure 34 and 35 show the NLDFT plot of hierarchically porous MIL-88Bs synthesized at  $130^\circ\text{C}$ .

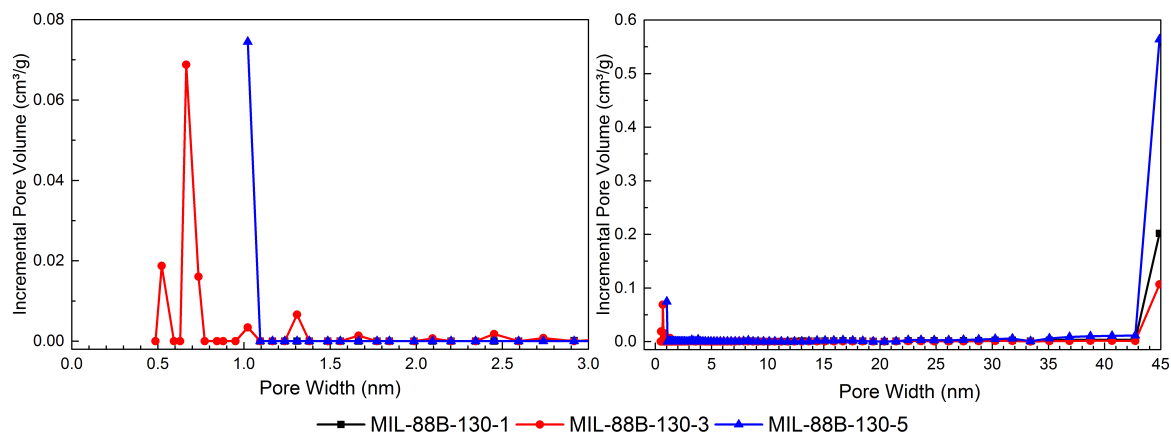


Figure 34. NLDFT plot hierarchically porous MIL-88Bs synthesized at  $130^\circ\text{C}$ .

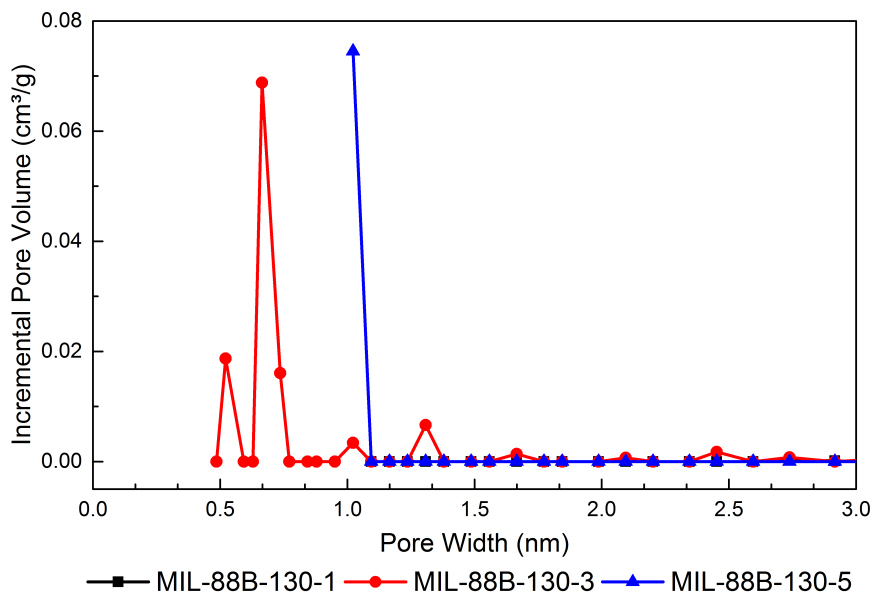


Figure 35. NLDFT plot of MIL-88B-130-1, MIL-88B-130-3, and MIL-88B-130-5.

MIL-88B-130-1 has no micropores wider than 1.094 nm which possess a volume of  $0.114 \text{ cm}^3/\text{g}$  and corresponds to 31.3% of the total pore volume. The highest volume increase which corresponds to 55.5% of the total pore volume belongs to pores with pore diameters of 44.8 nm. MIL-88B-130-3 has no pores narrower than 0.522 nm and pores with pore diameters of 0.629 nm possess the highest volume increase in the microporous region which corresponds to 11.6% of the total pore volume. MIL-88B-130-5 has the highest volume contribution from the pores with pore diameters of 44.8 nm which corresponds to 80.4% of the total pore volume and illustrates that MIL-88B-130-5 has uniform micropores. Contrary

to this, MIL-88B-130-3 has micropores with pore sizes ranging between 0.665 nm and 1.666 nm. The highest volume belongs to pores with pore diameters of 0.665 nm in MIL-88B-130-3 while MIL-88B-130-5 has the highest contribution from micropores with pore diameters of 1.022 nm. NLDFT plots of MIL-88B-150-1, MIL-88B-150-3, and MIL-88B-150-5 can be found below in Figure 36 and 37.

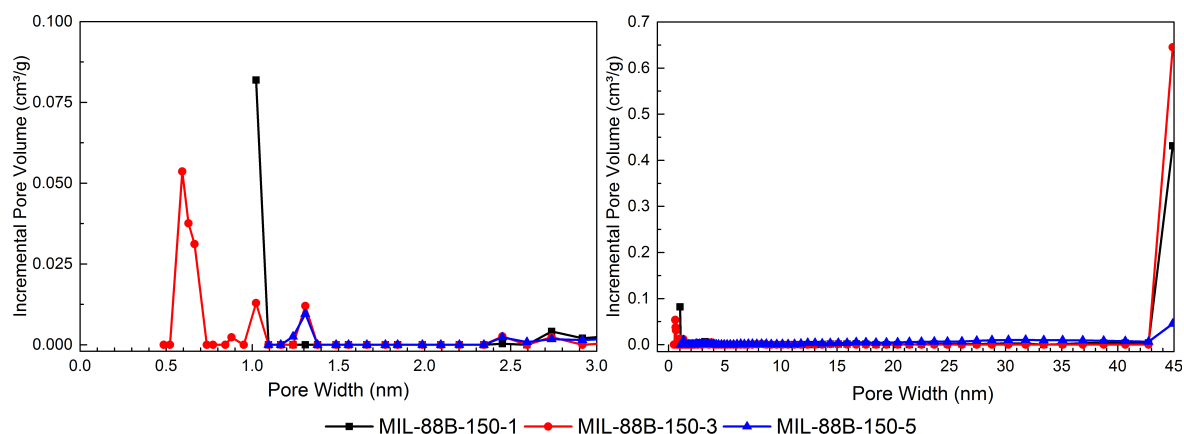


Figure 36. NLDFT plot MIL-88B type MOF crystallites synthesized at 150 °C.

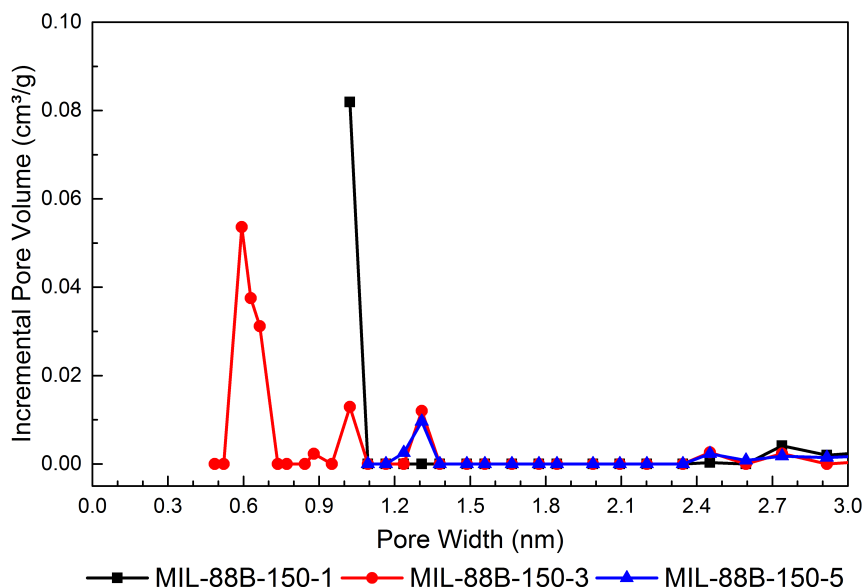


Figure 37. NLDFT plot of MIL-88B-150-1, MIL-88B-150-3, and MIL-88B-150-5.

MIL-88B-150-1 and MIL-88B-150-3 show considerable increase in their pore volumes at the upper mesoporous range. MIL-88B-150-1 possess 0.43 cm<sup>3</sup>/g of volume increase that corresponds to 68.1% of the total pore volume while MIL-88B-150-3 has 0.65 cm<sup>3</sup>/g of volume increase at the upper mesopore size range which corresponds to 79% of the

total pore volume. Total pore volume of MIL-88B-150-5 ( $0.28 \text{ cm}^3/\text{g}$ ) is considerably lower than MIL-88B-150-1 ( $0.634 \text{ cm}^3/\text{g}$ ) and MIL-88B-150-3 ( $0.82 \text{ cm}^3/\text{g}$ ). In the case of MIL-88B-150-1 micropores that contributes to micropore and total pore volume have diameters lower than 1.0 nm and their overall contribution to the total pore volume is as low as 12.9%. MIL-88B-150-3 has pores as narrow as 0.593 nm and there are no pores narrower than 0.593 nm. Apparently, MIL-88B-150-3 possess either micropores which have pore widths lower than 1.38 nm or mesopores at the upper mesoporous range.

MIL-88B-150-5 has a micropore volume of  $0.0355 \text{ cm}^3/\text{g}$  which corresponds to 12.6% of the total pore volume. Identical to MIL-88B-150-1 and MIL-88B-150-3, the highest volume increase is observed in pores with pore diameters of 44.8 nm. In addition, mesopores that contributes to the total pore volume occupies 87.4% of the total pore volume which is considerably higher than the contribution of micropores. Total pore volume of MIL-88B-150-3 is 2.9 times higher than the total pore volume of MIL-88B-150-5.

NLDFT analysis confirms that the surfactant and template-free synthesis strategy forms hierarchical porosity. The hierarchical porous MIL-88Bs possess a two-pore system. In line with  $\text{N}_2$  sorption isotherms and t-plot method, NLDFT analysis shows that Fe:TPA ratio has significant effect on the textural porosity. When hierarchically porous MIL-88Bs are synthesized with excess amount of iron salt, volume occupied by textural mesopores at the upper mesoporous range increases, fraction of the textural porosity increases. Table 3 presents the measured and calculated BET surface areas, micropore volume and total pore volume of hierarchically porous MIL-88Bs synthesized at 110, 130, 150 °C with different TPA amount.

Table 3. BET surface area( $\text{m}^2/\text{g}$ ), micropore volume ( $\text{m}^3/\text{g}$ ) and total pore volume ( $\text{cm}^3/\text{g}$ ) of hierarchically porous MIL-88Bs synthesized at 110, 130, 150 °C with different iron to TPA ratio.

|               | BET Surface Area ( $\text{m}^2/\text{g}$ ) | Micropore Volume ( $\text{cm}^3/\text{g}$ ) | Mesopore Volume ( $\text{cm}^3/\text{g}$ ) | Total Pore Volume ( $\text{cm}^3/\text{g}$ ) | Textural Mesoporosity (%) |
|---------------|--------------------------------------------|---------------------------------------------|--------------------------------------------|----------------------------------------------|---------------------------|
| MIL-88B-110-1 | 400.4 $\pm$ 1.1E01                         | 0.18 $\pm$ 1.4E-02                          | 0.017 $\pm$ 1.4E-2                         | 0.19 $\pm$ 2.0E-2                            | 8.3                       |
| MIL-88B-110-3 | 452.4 $\pm$ 1.9E01                         | 0.24 $\pm$ 3.2E-02                          | 0.0096 $\pm$ 7.0E-3                        | 0.25 $\pm$ 1.2E-2                            | 3.9                       |
| MIL-88B-110-5 | 445.9 $\pm$ 1.9E01                         | 0.20 $\pm$ 3.2E-02                          | 0.028 $\pm$ 1.7E-2                         | 0.23 $\pm$ 2.2E-2                            | 12.3                      |
| MIL-88B-130-1 | 265.4 $\pm$ 2.6E01                         | 0.11 $\pm$ 6.5E-03                          | 0.25 $\pm$ 9.7E-3                          | 0.36 $\pm$ 1.1E-1                            | 68.8                      |
| MIL-88B-130-3 | 249.4 $\pm$ 1.6E01                         | 0.12 $\pm$ 1.6E-02                          | 0.13 $\pm$ 5.5E-2                          | 0.24 $\pm$ 8.5E-2                            | 52.8                      |
| MIL-88B-130-5 | 283.1 $\pm$ 2.6E01                         | 0.11 $\pm$ 2.8E-03                          | 0.66 $\pm$ 4.3E-2                          | 0.77 $\pm$ 2.0E-2                            | 86.0                      |
| MIL-88B-150-1 | 357.1 $\pm$ 7.8E01                         | 0.14 $\pm$ 4.6E-02                          | 0.49 $\pm$ 3.1E-1                          | 0.63 $\pm$ 2.6E-1                            | 77.4                      |
| MIL-88B-150-3 | 346.3 $\pm$ 1.7E01                         | 0.15 $\pm$ 2.3E-02                          | 0.67 $\pm$ 3.6E-1                          | 0.81 $\pm$ 3.0E-1                            | 81.7                      |
| MIL-88B-150-5 | 117.7 $\pm$ 1.9E01                         | 0.036 $\pm$ 9.0E-03                         | 0.25 $\pm$ 2.7E-2                          | 0.28 $\pm$ 1.8E-2                            | 87.4                      |

### 3.3.6. FTIR Analysis

Assigning vibrational modes has crucial importance on the determination of the structure and structural changes of these frameworks. FTIR spectra of hierarchical porous MIL-88Bs synthesized at different temperatures with different Fe:TPA ratio, and observed bands and representative assigned modes are provided below.

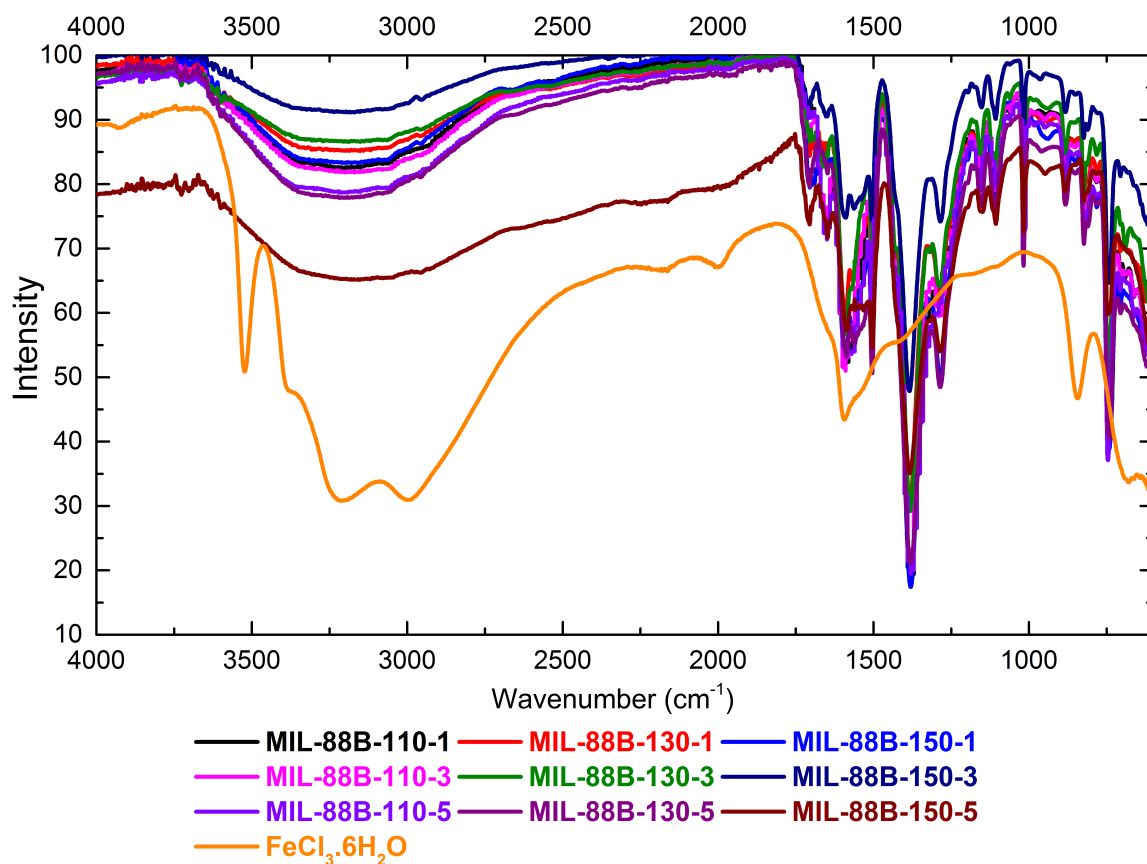


Figure 38. FTIR spectra of hierarchically porous MIL-88Bs and the FeCl<sub>3</sub>·6H<sub>2</sub>O.

FTIR spectrum is divided into following regions: (i) 3000-3600 cm<sup>-1</sup> (ii) 1650-2800 cm<sup>-1</sup> (iii) 1300-1650 cm<sup>-1</sup> and, (iv) 800-1300 cm<sup>-1</sup>. Three important conclusions are drawn: (I) None of the hierarchical porous MIL-88Bs synthesized at 110 °C possess peaks attributed to free TPA. (II) Firm hierarchical porous MIL-88Bs which possess successfully attached TPAs to metal center, were formed, and lastly (III) Bands attributed to H<sub>2</sub>O is present.

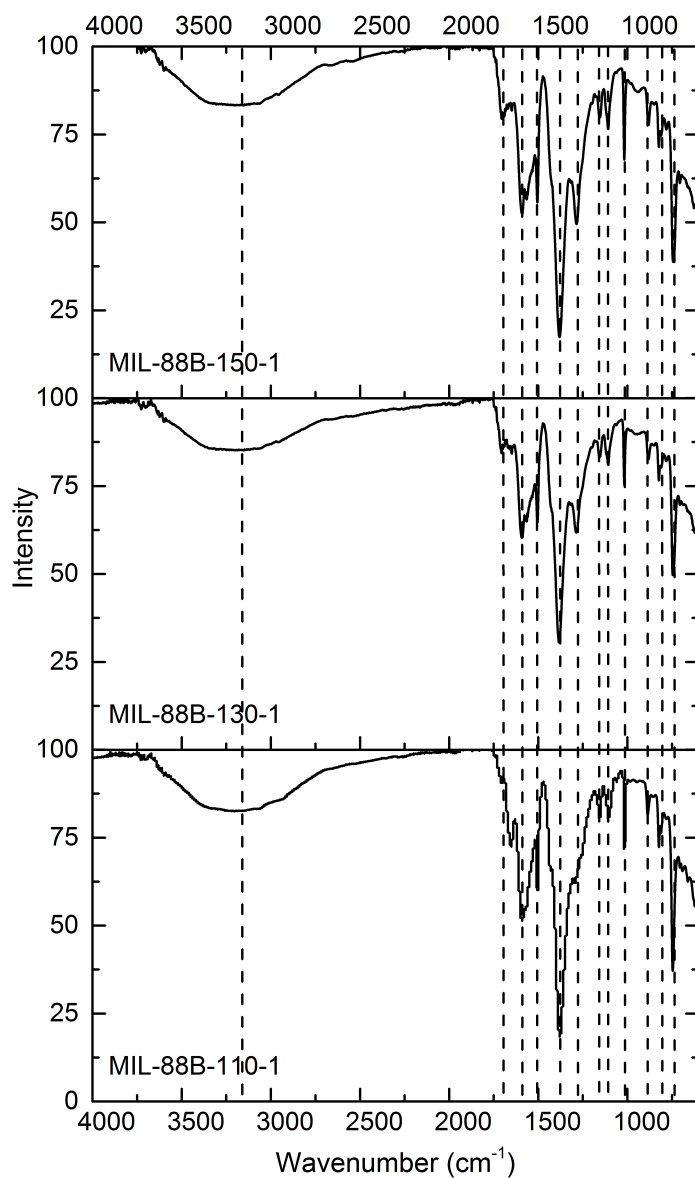


Figure 39. FTIR spectra of hierarchical porous MIL-88Bs synthesized with an Fe:BDC ratio of 1.



Table 4. Representative assigned modes of hierarchical porous MIL-88Bs synthesized at 110°C.

|                 | MIL-88B-110-1         | MIL-88B-110-3         | MIL-88B-110-5         | Assigned mode                                                      | References                                                                                                                                                                                |
|-----------------|-----------------------|-----------------------|-----------------------|--------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| 1 <sup>st</sup> | 3207 cm <sup>-1</sup> | 3197 cm <sup>-1</sup> | 3197 cm <sup>-1</sup> | O-H bond stretching                                                | (Torres et al., 2018)                                                                                                                                                                     |
| 2 <sup>nd</sup> | 1650 cm <sup>-1</sup> | 1650 cm <sup>-1</sup> | 1649 cm <sup>-1</sup> | C=O asymmetric stretching mode of DMF                              | (Dhumal, Singh, Anderson, Kiefer, & Kim, 2016)                                                                                                                                            |
| 3 <sup>rd</sup> | 1589 cm <sup>-1</sup> | 1591 cm <sup>-1</sup> | 1569 cm <sup>-1</sup> | 19b phenyl modes of H <sub>2</sub> BDC (skelatal modes of MIL-88B) | (Arenas & Marcos, 1979; Benbellat et al., 2006; Rowsell & Yaghi, 2006a; Tafipolsky, Amirjalayer, & Schmid, 2010; Téllez S., Hollauer, Mondragon, & Castaño, 2001; Tripathi & Sheng, 1979) |
| 4 <sup>th</sup> | 1503 cm <sup>-1</sup> | 1504 cm <sup>-1</sup> | 1503 cm <sup>-1</sup> | 19a phenyl modes of H <sub>2</sub> BDC (skelatal modes of MIL-88B) | (Arenas & Marcos, 1979; Téllez S. et al., 2001; Tripathi & Sheng, 1979)                                                                                                                   |
| 5 <sup>th</sup> | 1378 cm <sup>-1</sup> | 1380 cm <sup>-1</sup> | 1378 cm <sup>-1</sup> | Skelatal modes of MIL-88B                                          | (Benbellat et al., 2006; Rowsell & Yaghi, 2006a;                                                                                                                                          |

|                  |                       |                       |                       |                                              |                                                                         |
|------------------|-----------------------|-----------------------|-----------------------|----------------------------------------------|-------------------------------------------------------------------------|
|                  |                       |                       |                       |                                              | Tafipolsky et al., 2010)                                                |
| 6 <sup>th</sup>  | 1156 cm <sup>-1</sup> | 1156 cm <sup>-1</sup> | 1156 cm <sup>-1</sup> | skelatal modes of MIL-88B                    | (Arenas & Marcos, 1979; Téllez S. et al., 2001; Tripathi & Sheng, 1979) |
| 7 <sup>th</sup>  | 1106 cm <sup>-1</sup> | 1106 cm <sup>-1</sup> | 1106 cm <sup>-1</sup> | C-O-Fe stretching, skelatal modes of MIL-88B | (Arenas & Marcos, 1979; Téllez S. et al., 2001; Tripathi & Sheng, 1979) |
| 8 <sup>th</sup>  | 1016 cm <sup>-1</sup> | 1016 cm <sup>-1</sup> | 1016 cm <sup>-1</sup> | $\nu_{18a}$ ring mode of terephthalate       | (Arenas & Marcos, 1979; Téllez S. et al., 2001; Tripathi & Sheng, 1979) |
| 9 <sup>th</sup>  | 823 cm <sup>-1</sup>  | 823 cm <sup>-1</sup>  | 823 cm <sup>-1</sup>  | Fe-O stretching mode                         | (Ye Li et al., 2015)                                                    |
| 10 <sup>th</sup> | 746 cm <sup>-1</sup>  | 745 cm <sup>-1</sup>  | 745 cm <sup>-1</sup>  | Fe-O stretching mode                         | (Ye Li et al., 2015)                                                    |
| 11 <sup>th</sup> | 617 cm <sup>-1</sup>  | 621 cm <sup>-1</sup>  | 624 cm <sup>-1</sup>  | Central oxygen in single Fe <sub>3</sub> O   | (Vuong, Pham, & Do, 2013a)                                              |

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Broad bands observed in between 3000 to 3600 cm<sup>-1</sup> are assigned to OH groups of O-H bond stretching. The broadest band within region (i) belongs to MIL-88-110-5. We have attributed the observed broadening in region (i) to statistical distribution of OH over the available sites. In a study of Jacobs et. al. (Jacobs & Mortier, 1982), OH band broadening in zeolites was associated with the greater pore sizes. In line with the other characterization methods conducted so far, we suggest that the broadened band represents a larger pore size at which more OH groups are adsorbed. Having the broadest OH band with the lowest

intensity, hierarchically porous MIL-88Bs synthesized with an Fe:TPA ratio of 5 are thought to be formed of larger textural pores in comparison to hierarchically porous MIL-88Bs synthesized at 110 °C.

The band in between 3000 to 3100  $\text{cm}^{-1}$  deduces that a stable MOF structure was formed. DMF spectra consisted C–H (cis-methyl) stretching and symmetric C–H (cis-methyl) stretching mode within the wavelength range of 2500 to 3000  $\text{cm}^{-1}$ . Hierarchically porous MIL-88Bs synthesized at 110 °C do not consist peaks that are assigned to DMF within this wavelength range. Additionally, no other peaks are observed at 1063  $\text{cm}^{-1}$ . Having no peaks either at 1063 or at 2861  $\text{cm}^{-1}$  confirms the successful removal of DMF molecules from the pores.

The peaks in the wavelength range of 1650 and 2800  $\text{cm}^{-1}$  are assigned to the characteristic modes of iron-based MOFs. None of the hierarchically porous MIL-88Bs consist the peaks at 1704  $\text{cm}^{-1}$  illustrating that there were no free TPA left and most of the  $\text{H}_2\text{BDC}$  was deprotonated. A lower TPA amount used in the synthesis causes the band width to increase while the peak intensity decreases. None of the hierarchically porous MIL-88Bs synthesized at 110 °C consist the peak at 1704  $\text{cm}^{-1}$  which is an indicator of the free TPA linker. Having no peaks at 1704  $\text{cm}^{-1}$  suggests that most of the  $\text{H}_2\text{BDC}$  used during the synthesis was deprotonated. More importantly, using a  $\text{Cl}^-$  based metal salt provides a promising result as linker was deprotonated and there was no need to remove free acid present in the sample. Without any further treatment, hierarchically porous MIL-88Bs were synthesized acid free.

The peak at 1659  $\text{cm}^{-1}$  is assigned to C=O asymmetric stretching mode of DMF molecule and is present in the FTIR spectra of all hierarchically porous MIL-88Bs synthesized at 110 °C. We have confirmed that we have formed the skeletal of our hierarchically porous MIL-88Bs by the peaks obtained at region (iii) at which wavelength ranges between 1300 and 1650  $\text{cm}^{-1}$ . Peaks obtained at this region are typical of crystalline state carboxylic acids and are a confirmation of the successfully formed MOF structure.

Peaks observed at 1385 and 1589  $\text{cm}^{-1}$  illustrate the successful attachment of TPA to metal centre. Random distribution of DMF that was used as the main solvent during the heating process can be proved by the peaks at 1285 and 1504  $\text{cm}^{-1}$  in the FTIR spectra of all hierarchically porous MIL-88Bs. Peaks at 1017  $\text{cm}^{-1}$ , 1155  $\text{cm}^{-1}$ , 1504  $\text{cm}^{-1}$ , 1589  $\text{cm}^{-1}$  are

associated with a form of TPA and present in the FTIR spectra of all hierarchically porous MIL-88Bs.

We have proved that TPA is attached to the metal by C-O-Fe stretching by the peak at  $1107\text{ cm}^{-1}$ . In addition, the peaks at  $742$  and  $823\text{ cm}^{-1}$  are assigned to Fe-O stretching and prove that Fe was coordinated with TPA. Finally, the peak in between the wavelength range of  $600$  and  $626\text{ cm}^{-1}$  is assigned to central oxygen in single  $\text{Fe}_3\text{O}$  and is present in the FTIR spectra of all the hierarchically porous MIL-88Bs synthesized at  $110^\circ\text{C}$ . Table 5 shows the representative assigned modes of hierarchically porous MIL-88Bs synthesized at  $130^\circ\text{C}$ .

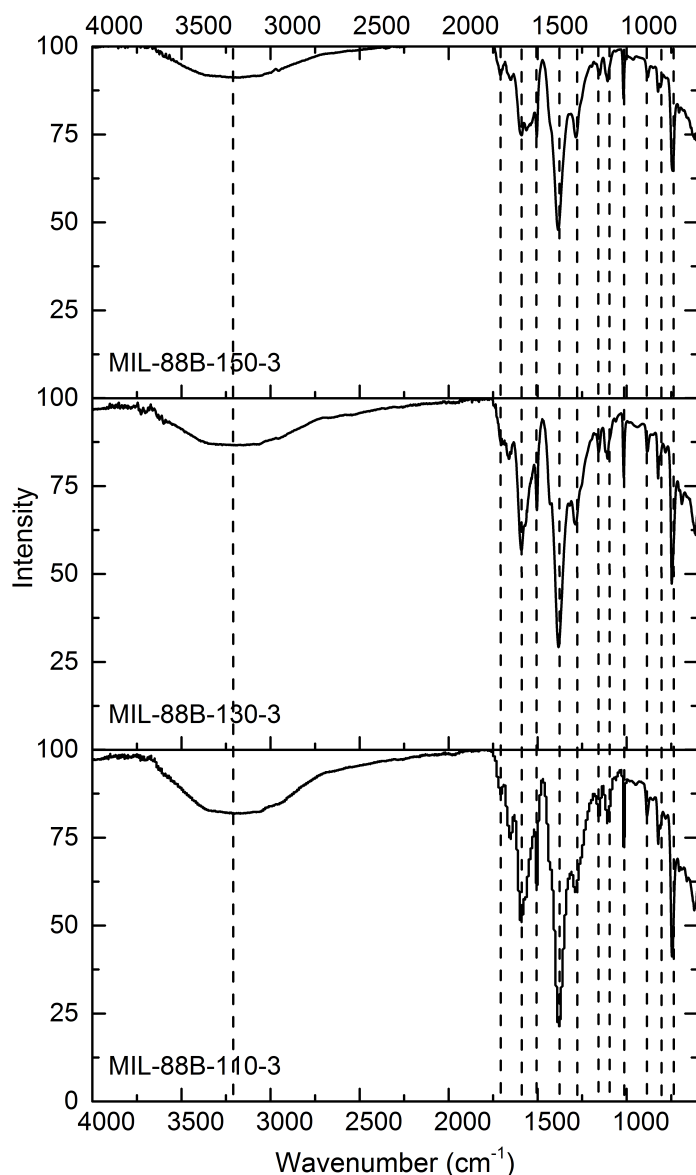


Figure 40. FTIR spectra of MIL-88B-110-3, MIL-88B-130-3, and MIL-88B-150-3.

Table 5. Representative assigned modes of hierarchically porous MIL-88Bs synthesized at 130°C.

|                 | MIL-88B-130-1         | MIL-88B-130-3         | MIL-88B-130-5         | Assigned mode                                                      | References                                                                                                                                       |
|-----------------|-----------------------|-----------------------|-----------------------|--------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------|
| 1 <sup>st</sup> | 3152 cm <sup>-1</sup> | 3188 cm <sup>-1</sup> | 3217 cm <sup>-1</sup> | O-H bond stretching                                                | (Torres et al., 2018)                                                                                                                            |
| 2 <sup>nd</sup> | 1705 cm <sup>-1</sup> | -                     | 1705 cm <sup>-1</sup> | C=O band of carboxylic acid                                        | (Aysu Yurduşen, Yürüm, & Yürüm, 2019)                                                                                                            |
| 3 <sup>rd</sup> | 1647 cm <sup>-1</sup> | 1661 cm <sup>-1</sup> |                       | C=O asymmetric stretching mode of DMF                              | (Dhumal et al., 2016)                                                                                                                            |
| 4 <sup>th</sup> | 1590 cm <sup>-1</sup> | 1590 cm <sup>-1</sup> | 1587cm <sup>-1</sup>  | 19b phenyl modes of H <sub>2</sub> BDC (skelatal modes of MIL-88B) | (Arenas & Marcos, 1979; Benbellat et al., 2006; Rowsell & Yaghi, 2006a; Tafipolsky et al., 2010; Téllez S. et al., 2001; Tripathi & Sheng, 1979) |
| 5 <sup>th</sup> | 1504 cm <sup>-1</sup> | 1503 cm <sup>-1</sup> | 1504 cm <sup>-1</sup> | 19a phenyl modes of H <sub>2</sub> BDC (skelatal modes of MIL-88B) | (Arenas & Marcos, 1979; Téllez S. et al., 2001; Tripathi & Sheng, 1979)                                                                          |
| 6 <sup>th</sup> | 1383 cm <sup>-1</sup> | 1382 cm <sup>-1</sup> | 1380 cm <sup>-1</sup> | skelatal modes of MIL-88B                                          | (Benbellat et al., 2006; Rowsell & Yaghi, 2006a; Tafipolsky et al., 2010)                                                                        |
| 7 <sup>th</sup> | 1156 cm <sup>-1</sup> | 1156 cm <sup>-1</sup> | 1155 cm <sup>-1</sup> | skelatal modes of MIL-88B                                          | (Arenas & Marcos, 1979; Téllez S. et al., 2001; Tripathi                                                                                         |

|                  |                       |                       |                       |                                              |                                                                         |
|------------------|-----------------------|-----------------------|-----------------------|----------------------------------------------|-------------------------------------------------------------------------|
|                  |                       |                       |                       |                                              | & Sheng, 1979)                                                          |
| 8 <sup>th</sup>  | 1107 cm <sup>-1</sup> | 1107 cm <sup>-1</sup> | 1107 cm <sup>-1</sup> | C-O-Fe stretching, skeletal modes of MIL-88B | (Arenas & Marcos, 1979; Téllez S. et al., 2001; Tripathi & Sheng, 1979) |
| 9 <sup>th</sup>  | 1017 cm <sup>-1</sup> | 1016 cm <sup>-1</sup> | 1017 cm <sup>-1</sup> | $\nu_{18a}$ ring mode of terephthalate       | (Arenas & Marcos, 1979; Téllez S. et al., 2001; Tripathi & Sheng, 1979) |
| 10 <sup>th</sup> | 823 cm <sup>-1</sup>  | 823 cm <sup>-1</sup>  | 823 cm <sup>-1</sup>  | Fe-O stretching mode                         | (Ye Li et al., 2015)                                                    |
| 11 <sup>th</sup> | 745 cm <sup>-1</sup>  | 746 cm <sup>-1</sup>  | 740 cm <sup>-1</sup>  | Fe-O stretching mode                         | (Ye Li et al., 2015)                                                    |
| 12 <sup>th</sup> | 612 cm <sup>-1</sup>  | 612 cm <sup>-1</sup>  | -                     | Central oxygen in single Fe <sub>3</sub> O   | (Vuong et al., 2013a)                                                   |

A broad band is observed within the first region. This broad band is attributed to OH groups with O-H bond stretching. In the case of hierarchically porous MIL-88Bs synthesized at 130 °C, no peaks that belong to DMF is observed. Furthermore, there are no peaks traced at 1063 cm<sup>-1</sup>. No peaks observed at 1063, 2861, or 2931 cm<sup>-1</sup> confirm the successful removal of DMF molecules from the pores. We have confirmed our stable hierarchically porous MIL-88B structures with the band in between 3000 to 3100 cm<sup>-1</sup>. In between the wavelengths of 1650 to 2800 cm<sup>-1</sup> characteristic modes of iron-based MOFs are traced. MIL-88B type MOF crystallites synthesized with an Fe:TPA ratio of 1 and 5 possess peaks at 1704 cm<sup>-1</sup> showing that free TPA linker was still present in the structure. However, there are no peaks at 1704 cm<sup>-1</sup> in MIL-88B-130-3. The peak at 1659 cm<sup>-1</sup> represents the C=O asymmetric stretching mode of DMF molecule. MIL-88B-130-1 and MIL-88B-130-3 consist the peaks at 1647 cm<sup>-1</sup> while MOFs synthesized with an Fe:TPA ratio of 5 do not.

At region (iii) where wavelength ranges between 1300 and 1650 cm<sup>-1</sup> characteristic peaks of crystalline state carboxylic acids are observed and confirm that the skeletal of the hierarchically porous MIL-88Bs were formed successfully. We proved that TPA is successfully attached to metal centre by the peaks present at 1385 and 1589 cm<sup>-1</sup>. The peaks

at 1285 and 1504  $\text{cm}^{-1}$  confirmed the randomly distributed DMF molecules. Besides, bands which are assigned to a form of TPA are observed at 1017  $\text{cm}^{-1}$ , 1155  $\text{cm}^{-1}$ , 1504  $\text{cm}^{-1}$ , 1589  $\text{cm}^{-1}$ . We showed the successful attachment of TPA to metal by the C-O-Fe stretching by the peak at 1107  $\text{cm}^{-1}$ . Additionally, the peaks obtained at 742 and 823  $\text{cm}^{-1}$  are assigned to Fe-O stretching mode which prove the successful coordination of Fe and TPA.

Different from hierarchically porous MIL-88Bs synthesized with an Fe:TPA ratio of 1 and 5, MIL-88B-130-3 possesses a peak at 690  $\text{cm}^{-1}$  which is also present in the FTIR spectra of neat TPA. Lastly, the peak at 612  $\text{cm}^{-1}$  is attributed to central oxygen in single  $\text{Fe}_3\text{O}$  which is only observed in MIL-88B-130-1, and MIL-88B-130-3. Table 6 illustrates the representative assigned modes of hierarchically porous MIL-88Bs synthesized at 150 °C. In the case of hierarchically porous MIL-88Bs synthesized at 150 °C, the following conclusions are drawn: (I) Free TPA is present in the samples, (II) Carboxylate ligand attaches successfully to metal center, and (III) Bands typical of  $\text{H}_2\text{O}$  is observed.

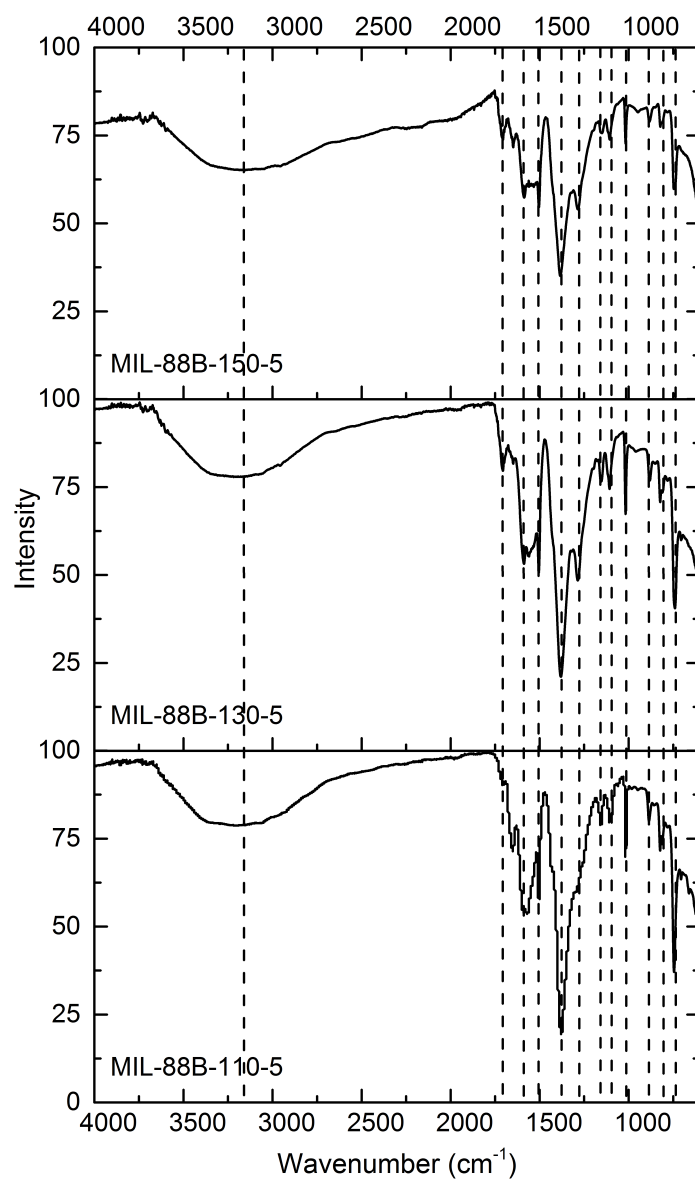


Figure 41. FTIR spectra of MIL-88B-110-5, MIL-88B-130-5, and MIL-88-150-5.



Table 6. Representative assigned modes of MOF crystallites synthesized at 150°C.

|                 | MIL-88B-150-1         | MIL-88B-150-3         | MIL-88B-150-5         | Assigned mode                                                      | References                                                                                                                                       |
|-----------------|-----------------------|-----------------------|-----------------------|--------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------|
| 1 <sup>st</sup> | 3152 cm <sup>-1</sup> | 3170 cm <sup>-1</sup> | 3153 cm <sup>-1</sup> | O-H bond stretching                                                | (Torres et al., 2018)                                                                                                                            |
| 2 <sup>nd</sup> | 1704 cm <sup>-1</sup> | 1708 cm <sup>-1</sup> | 1705 cm <sup>-1</sup> | C=O band of carboxylic acid                                        | (Aysu Yurduşen et al., 2019)                                                                                                                     |
| 3 <sup>rd</sup> |                       |                       | 1647cm <sup>-1</sup>  | C=O asymmetric stretching mode of DMF                              | (Dhumal et al., 2016)                                                                                                                            |
| 4 <sup>th</sup> | 1589 cm <sup>-1</sup> | 1589 cm <sup>-1</sup> | 1586 cm <sup>-1</sup> | 19b phenyl modes of H <sub>2</sub> BDC (skelatal modes of MIL-88B) | (Arenas & Marcos, 1979; Benbellat et al., 2006; Rowsell & Yaghi, 2006a; Tafipolsky et al., 2010; Téllez S. et al., 2001; Tripathi & Sheng, 1979) |
| 5 <sup>th</sup> | 1504 cm <sup>-1</sup> | 1504 cm <sup>-1</sup> | 1503 cm <sup>-1</sup> | 19a phenyl modes of H <sub>2</sub> BDC (skelatal modes of MIL-88B) | (Arenas & Marcos, 1979; Téllez S. et al., 2001; Tripathi & Sheng, 1979)                                                                          |
| 6 <sup>th</sup> | 1380 cm <sup>-1</sup> | 1384 cm <sup>-1</sup> | 1384 cm <sup>-1</sup> | Skelatal modes of MIL-88B                                          | (Arenas & Marcos, 1979; Benbellat et al., 2006; Rowsell & Yaghi, 2006a; Tafipolsky et al., 2010; Téllez S. et al., 2001; Tripathi & Sheng, 1979) |
| 7 <sup>th</sup> | 1155 cm <sup>-1</sup> | 1152 cm <sup>-1</sup> | 1149 cm <sup>-1</sup> | Skelatal modes of MIL-88B                                          | (Arenas & Marcos, 1979;                                                                                                                          |

|                  |                       |                       |                       |                                               |                                                                                     |
|------------------|-----------------------|-----------------------|-----------------------|-----------------------------------------------|-------------------------------------------------------------------------------------|
|                  |                       |                       |                       |                                               | Téllez S. et al.,<br>2001; Tripathi &<br>Sheng, 1979)                               |
| 8 <sup>th</sup>  | 1107 cm <sup>-1</sup> | 1107 cm <sup>-1</sup> | 1106 cm <sup>-1</sup> | C-O-Fe<br>stretching                          | (Arenas &<br>Marcos, 1979;<br>Téllez S. et al.,<br>2001; Tripathi &<br>Sheng, 1979) |
| 9 <sup>th</sup>  | 1017 cm <sup>-1</sup> | 1017 cm <sup>-1</sup> | 1017 cm <sup>-1</sup> | $\nu_{18a}$ ring mode<br>of terephthalate     | (Arenas &<br>Marcos, 1979;<br>Téllez S. et al.,<br>2001; Tripathi &<br>Sheng, 1979) |
| 10 <sup>th</sup> | 823 cm <sup>-1</sup>  | 823 cm <sup>-1</sup>  |                       | Fe-O stretching<br>mode                       | (Ye Li et al.,<br>2015)                                                             |
| 11 <sup>th</sup> | 742 cm <sup>-1</sup>  | 742 cm <sup>-1</sup>  | 746 cm <sup>-1</sup>  | Fe-O stretching<br>mode                       | (Ye Li et al.,<br>2015)                                                             |
| 12 <sup>th</sup> | 626 cm <sup>-1</sup>  |                       |                       | Central oxygen<br>in single Fe <sub>3</sub> O | (Vuong et al.,<br>2013a)                                                            |

Within the region (i) observed bands are attributed to OH groups involved in H-bonds. For an Fe:TPA ratio greater than 3, the band intensity decreases. Besides the decreased intensity, broadening in band width is observed. MIL-88B-150-3 has the narrowest band with the highest intensity within region (i). As already reported for zeolites, OH band broadens with increasing pore size (Jacobs & Mortier, 1982). Thus, a more broadened band can be attributed to a larger pore size at which more OH groups are adsorbed whereas the band would be narrower for a smaller pore diameter.

Even though neither MIL-88B-150-1 nor MIL-88B-150-3 consist the peak at 1647 cm<sup>-1</sup>, it is attributed to C=O asymmetric stretching mode of DMF. Having no peaks at 1647 cm<sup>-1</sup> is a consequence of the successful removal of DMF molecules from the pores of MIL-88B-150-1 and MIL-88B-150-3. However, MIL-88B-150-5 had some residual DMF molecule left in the pores of. Peak at 1659 cm<sup>-1</sup> is a typical peak of DMF molecules. MIL-88B-150-1 achieves the sharpest peak at 1380 cm<sup>-1</sup> with the lowest intensity. 1380 cm<sup>-1</sup> is within region (iii) and it is attributed to the symmetric stretching vibration of carboxylates.

Three of the hierarchically porous MIL-88Bs synthesized with different TPA amounts obtained different peak intensities for the peak at  $1380\text{ cm}^{-1}$ . Additional to  $1380\text{ cm}^{-1}$ , intensities of the peak at  $1017\text{ cm}^{-1}$  varies in accordance with the TPA amount used during the synthesis. The peak at  $1017\text{ cm}^{-1}$  has been previously attributed to  $\nu_{18a}$  ring mode of terephthalate. Thus, signifies the structural changes present in hierarchically porous MIL-88Bs (Leclerc et al., 2011; Serre et al., 2007). Another noticeable difference is observed in the intensity of the band at  $742\text{ cm}^{-1}$ . Hierarchically porous MIL-88Bs synthesized with an Fe:TPA ratio of 1 possess the sharpest peak with the lowest intensity. Additionally, peak intensity increases by the decreasing the linker amount used during synthesis. We have previously assigned the peak at  $742\text{ cm}^{-1}$  to Fe-O stretching mode as a consequence of the Fe and TPA coordination. Hierarchically porous MIL-88Bs synthesized with an Fe:TPA ratio of 1 possess the highest TPA amount among the hierarchically porous MIL-88Bs synthesized at  $150\text{ }^{\circ}\text{C}$ . For one Fe atom hierarchically porous MIL-88Bs synthesized with an Fe:TPA ratio of 5 has the lowest amount of TPA which we attribute the intensity of the peak at  $742\text{ cm}^{-1}$  for hierarchically porous MIL-88Bs synthesized with an Fe:TPA of 5 to be the most intense.

Although all the hierarchically porous MIL-88Bs are exposed to same heating and thermal activation procedure, band widths and peak intensities of their OH band vary significantly. In line with other characterization methods, FTIR analysis shows that MIL-88B type MOF crystallites synthesized with an Fe:TPA ratio of 3 are formed of smaller textural pores among the hierarchically porous MIL-88Bs synthesized with different Fe:TPA ratios. Additionally, we have shown that DMF is removed successfully from the pores of hierarchically porous MIL-88Bs synthesized with an Fe:TPA ratio of 1 and 3. Presence of peaks characteristic to TPA confirms the successful attachment of TPA to the metal centre. By using a  $\text{Cl}^-$  based metal salt, hierarchically porous MIL-88Bs that are free of TPA were synthesized, successfully. Lastly, FTIR spectrum of hierarchically porous MIL-88Bs were compared with the FTIR spectra of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ . None of the peaks observed in the FTIR spectra of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$  ( $842\text{ cm}^{-1}$ ,  $1594\text{ cm}^{-1}$ ,  $2993\text{ cm}^{-1}$ ,  $3212\text{ cm}^{-1}$ , and  $3523\text{ cm}^{-1}$ ) were observed in the FTIR spectrum of hierarchically porous MIL-88Bs which proves that there are no metallic iron present.

### 3.3.7. Thermogravimetric Analysis (TGA)

TGA curves of hierarchically porous MIL-88Bs synthesized at 110, 130, and 150 °C with different Fe:TPA ratio can be found below in Figure 42, 43 and 44 and Table 7-10 show the percentage of mass loss during TGA.

TGA analysis demonstrates that MIL-88B type MOF crystallites synthesized with different Fe:TPA ratio are thermally stable. Table 7 shows the percentage of residual mass left after TGA was completed. Differences were observed in the residual masses left after analysis and decomposition temperature differ with TPA amount. Percent residual masses left after the analysis can be found in Table 7. Remaining residual masses are attributed to remaining metal oxides.

Table 7. Percentage of residual mass left after TGA was completed, %.

|        | Fe:TPA 1 | Fe:TPA 3 | Fe:TPA 5 |
|--------|----------|----------|----------|
| 110 °C | 31.0     | 28.1     | 25.7     |
| 130 °C | 30.5     | 28.1     | 31.3     |
| 150 °C | 33.8     | 33.6     | 56.3     |

The first step of TGA curve corresponds to adsorbed and coordinated water and DMF molecules. The second step is associated with solvent molecules trapped in pores. The third step which forms the main step of TGA curve is attributed to linker decomposition and lastly, the last step corresponds to CO<sub>2</sub> release by decomposition of carboxylates.

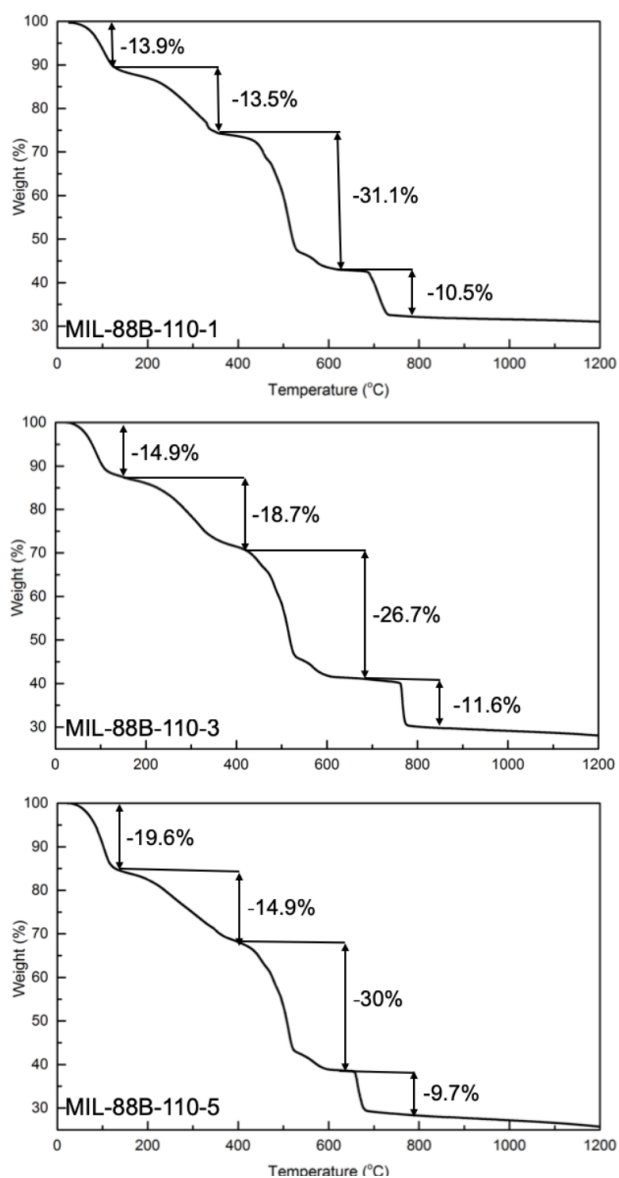


Figure 42. TGA curves of MIL-88B-110-1, MIL-88B-110-3, and MIL-88B-110-5.

MIL-88B-110-5 has the highest amount of mass loss in the first step. The highest fraction of mass loss at the second step is issued by MIL-88B-110-3.

Table 8. % mass loss during TGA analysis of MIL-88B-110-1, MIL-88B-110-3, and MIL-88B-110-5

| Temperature Range (°C) | MIL-88B-110-1 (%) | Temperature Range (°C) | MIL-88B-110-3 (%) | Temperature Range (°C) | MIL-88B-110-5 (%) |
|------------------------|-------------------|------------------------|-------------------|------------------------|-------------------|
| 25-185                 | -13.9             | 25-175                 | -14.9             | 25-169                 | -19.6             |
| 185-380                | -13.5             | 175-448                | -18.7             | 169-387                | -14.9             |
| 380-642                | -31.1             | 448-638                | -26.7             | 387-625                | -30               |
| 642-757                | -10.5             | 638-850                | -11.6             | 625-716                | -9.7              |

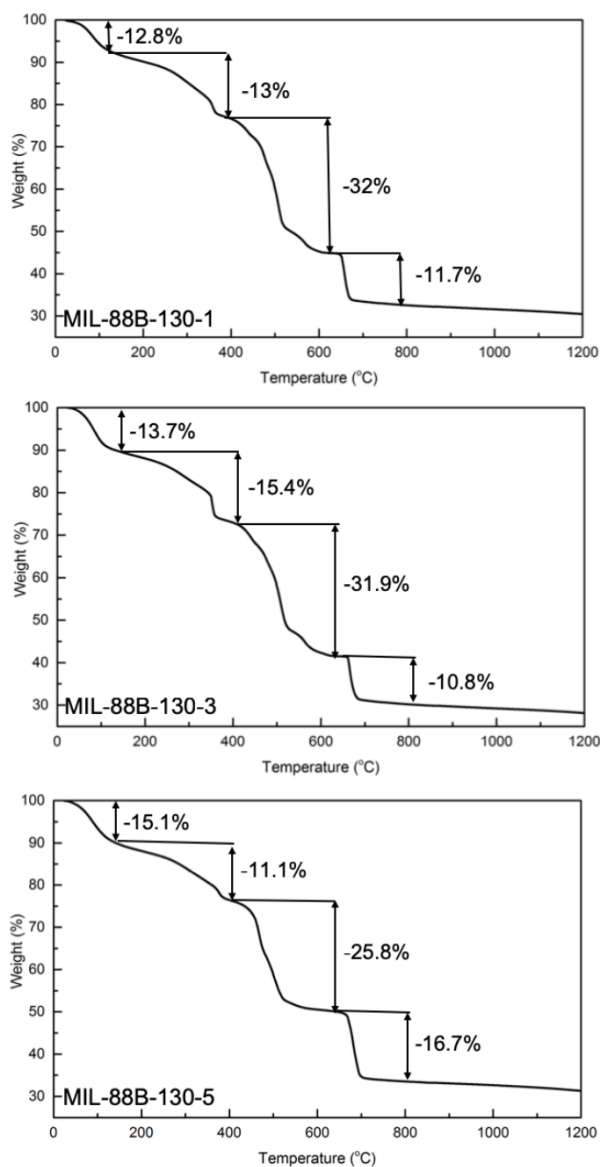


Figure 43. TGA curves of MIL-88B-130-1, MIL-88B-130-3, and MIL-88B-130-5.

Decomposition temperature of MIL-88B-130-5 is higher than MIL-88B-130-1, and MIL-88B-130-3. Percentage of mass lost by MIL-88B-130-5 is the least which may be attributed to the low amount of TPA used during synthesis.

Table 9. % mass loss during TGA analysis of MIL-88B-130-1, MIL-88B-130-3, and MIL-88B-130-5

| Temperature Range (°C) | MIL-88B-130-1 (%) | Temperature Range (°C) | MIL-88B-130-3 (%) | Temperature Range (°C) | MIL-88B-130-5 (%) |
|------------------------|-------------------|------------------------|-------------------|------------------------|-------------------|
| 25-208                 | -12.8             | 25-169                 | -13.7             | 25-226                 | -15.1             |
| 208-392                | -13               | 169-384                | -15.4             | 226-405                | -11.1             |
| 392-624                | -32               | 384-633                | -31.9             | 405-602                | -25.8             |
| 624-720                | -11.7             | 633-732                | -10.8             | 602-759                | -16.7             |



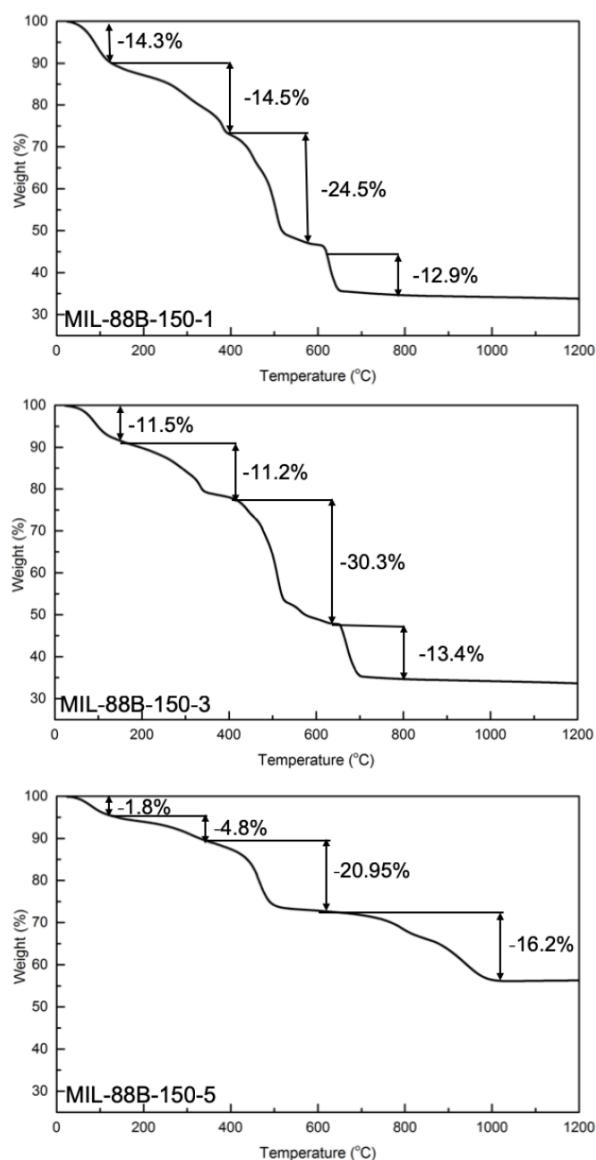


Figure 44. TGA curves of MIL-88B-150-1, MIL-88B-150-3, and MIL-88B-150-5.

Decomposition temperature of MIL-88B-150-3 is the highest among the hierarchically porous MIL-88Bs synthesized at 150 °C indicating its higher thermal stability. MIL-88B-150-1 possesses the highest residual mass left within the hierarchically porous MIL-88Bs synthesized at 150 °C.

Table 10. % mass loss during TGA analysis of MIL-88B-150-1, MIL-88B-150-3, and MIL-88B-150-5

| Temperature Range (°C) | MIL-88B-150-1 (%) | Temperature Range (°C) | MIL-88B-150-3 (%) | Temperature Range (°C) | MIL-88B-150-5 (%) |
|------------------------|-------------------|------------------------|-------------------|------------------------|-------------------|
| 25-201                 | -14.3             | 25-203                 | -11.5             | 25-236                 | -6.5              |
| 201-404                | -14.5             | 203-442.4              | -11.2             | 236-652                | -20.95            |
| 404-548                | -24.5             | 442.4-623              | -30.3             | 652-1070               | -10.6             |
| 548-698                | -12.9             | 623-759                | -13.4             |                        |                   |

Changing Fe:TPA ratio by varying the amount of linker used not only controlled the textural porosity but also changed the thermal stability of hierarchically porous MIL-88Bs. Hierarchically porous MIL-88Bs synthesized with different linker amounts possess different decomposition temperatures. By adjusting Fe:TPA ratio to 3, a higher thermal stability is achieved.

### 3.3.8. Possible Effect of Fe:TPA Ratio on the Textural Properties

MIL-88Bs are synthesized by the vigorous stirring of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ , TPA, and DMF. The vigorous stirring of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ , TPA, and DMF limited the growth of single crystals leading SBUs to aggregate and form nanosized MIL-88Bs. By the self-assembly of nanosized MIL-88Bs and Fe-TPA coordination, textural mesopores are formed spontaneously.

Moreover, to enhance the control over textural porosity during the synthesis of hierarchical porous MIL-88Bs, different Fe:TPA ratios are used. It is observed that textural properties of MIL-88Bs differ with Fe:TPA ratio used during the synthesis.

Hierarchical porous MIL-88Bs are synthesized by the aggregation of nanosized MIL-88B rods. In the presence of excess iron salt (a high Fe:TPA ratio), iron oxide clusters form prior to SBU formation. The interparticle voids (textural mesopores) in between the SBU aggregates widen which widens the textural mesopores. SEM images (Figure 21-23) clearly show the widened textural mesopores of MIL-88B-110-5, MIL-88B -130-5, and MIL-88B-150-5.

### **3.3.9. Possible Effect of Synthesis Temperature on the Textural Properties**

Hierarchical porous MIL-88Bs are synthesized by the aggregation of nanosized MIL-88B rods. Vigorous stirring of iron salt, TPA and DMF limits the growth of single crystals. The vigorous stirring forms SBUs which aggregate into MIL-88B nanorods. MIL-88B nanorods aggregate and form mesostructures.

In order to have control over textural porosity, the effect of synthesis temperature is investigated. It is shown that by utilizing the synthesis temperature the size of the textural mesopores can be finely controlled. At a synthesis temperature of 110 °C, pore structure of hierarchical porous MIL-88Bs are found to be formed dominantly of micropores, while at synthesis temperatures above 130 °C, textural mesopores dominate the pore structure. We have attributed this change in textural porosity to the influence of synthesis temperature on the size and the packing of the nanoparticles. When hierarchical porous MIL-88Bs are synthesized at 110 °C, smaller MIL-88B nanorods form. These smaller MIL-88B nanorods pack tightly and form narrower pores<sup>26</sup>. However, when hierarchical porous MIL-88Bs are synthesized at temperatures above 130 °C, larger MIL-88B nanorods form and then pack loosely which result wider pores to form.

## **3.4. Comparison with Literature**

Table 11 illustrates the BET surface area and total pore volume of MIL-88B that has been reported in the literature. Not only hierarchical pores are formed, but also a BET surface area higher than those of reported MIL-88Bs is achieved by the perturbation assisted nanofusion synthesis strategy. By the synthesis strategy used, we increased the BET surface area, and the total pore volume of hierarchical porous MIL-88Bs (MIL-88B-110-3) by 2.7, and 4.05 times, respectively.

Table 11. BET surface area and pore volume of MIL-88Bs reported in literature

| Heating temperature and duration | Solvent used in the synthesis | Drying temperature | BET Surface Area (m <sup>2</sup> /g) | Pore Volume (cm <sup>3</sup> /g) | Reference                   |
|----------------------------------|-------------------------------|--------------------|--------------------------------------|----------------------------------|-----------------------------|
| 145 °C 1.5 hour                  | DMF                           | -                  | 209.8                                | 0.42                             | (X. Cai, Lin, & Pang, 2016) |
| 100 °C 12 hour                   | DMF                           | 110 °C             | 165.4                                | 0.2                              | (C. Gao et al., 2017)       |
| 170 °C 24 hour                   | DMF                           | Room temperature   | 355                                  | 0.14                             | (Vuong, Pham, & Do, 2013b)  |
| Room temperature                 | EtOH                          | 80 °C              | 214                                  |                                  | (Hou et al., 2018)          |
| 110 °C 48 hour                   | DMF                           | 100 °C             | 452.4                                | 0.25                             | This Study (MIL-88B-110-3)  |
| 150 °C 48 hour                   | DMF                           | 100 °C             | 346.3                                | 0.81                             | This Study (MIL-88B-150-3)  |

### 3.5. Concluding Remarks

In this chapter the effect of Fe:TPA ratio and synthesis temperature on the textural porosity of hierarchically porous MIL-88Bs were investigated. Hierarchically porous MIL-88Bs with different pore size distribution were synthesized by a perturbation assisted nanofusion synthesis strategy that forms hierarchical pores. The perturbation assisted nanofusion synthesis strategy is a cost effective and a facile alternative to the synthesis of mesoporous materials with micropores. Vigorous stirring of FeCl<sub>3</sub>.6H<sub>2</sub>O, TPA, and DMF formed nanosized MIL-88B and embedded the formed nanosized MIL-88B into an

amorphous matrix. Interparticle voids were formed in between the aggregates of nanosized MIL-88B crystals which formed the textural mesopores.

It is found that Fe:TPA ratio controls the morphology and the textural porosity of hierarchically porous MIL-88Bs synthesized by a perturbation assisted nanofusion synthesis strategy. When synthesized at 110 °C with an Fe:TPA ratio of 3, micropore volume of MIL-88B-110-3 increases by a factor of 1.3 and a highly microporous pore structure (96%) is formed. In the meantime, synthesizing hierarchically porous MIL-88Bs with an Fe:TPA ratio of 5 provides a higher fraction of textural mesoporosity to hierarchically porous MIL-88Bs (MIL-88B-110-5: 12.3%, MIL-88B-130-5: 86%, and MIL-88B-150-5: 87.4%) providing hierarchically porous MIL-88Bs to consist both micro- and mesopores in their pore structure. In addition, by the perturbation assisted nanofusion synthesis strategy, a BET surface area and total pore volume that is higher than those of reported for MIL-88Bs are achieved. By the perturbation assisted nanofusion synthesis strategy, the BET surface area and total pore volume is enhanced by 2.7 and 4.05 times, respectively (C. Gao et al., 2017).

The increased fraction of textural mesoporosity of hierarchically porous MIL-88Bs synthesized with a high Fe:TPA ratio is due to excess iron salt present in the solution. Just before the formation of SBUs, iron oxide clusters form. Then in between the aggregates of nanosized MIL-88B, interparticle voids (textural mesopores) form spontaneously. These interparticle voids (textural mesopores) in between the SBU aggregates widen which increase the fraction of textural mesoporosity.

By this surfactant and template free synthesis strategy, this study reports an effortless way to produce hierarchical MOFs that consists both micro- and mesopores. The presence of micro- and mesopores in the pore structure will provide a great deal of opportunities in catalysis, and gas adsorption studies

## Chapter IV

### Carbon dioxide adsorption capacity of hierarchically porous MIL-88Bs and the crucial role of narrow micropores

In this chapter, we report a synthesis strategy that enhances the CO<sub>2</sub> adsorption capacity of hierarchically porous MIL-88Bs by the control of hierarchical pores via Fe/BDC ratio and synthesis temperature. Hierarchically porous MIL-88Bs synthesized at different temperatures with different Fe/BDC ratios are investigated for their CO<sub>2</sub> adsorption capacities. The crucial role of narrow micropores (pores with pore sizes smaller than 1 nm) on CO<sub>2</sub> adsorption capacity is shown. The highest CO<sub>2</sub> adsorption capacity of 5.58 wt.% (at 1 bar and 298 K) is achieved by hierarchically porous MIL-88Bs with a BET surface area of 400.4 m<sup>2</sup>/g. This CO<sub>2</sub> adsorption capacity is greater than those of reported commercially available MOFs (MOF-5 CO<sub>2</sub> adsorption capacity, 4.5 wt. %, and ZIF-8 CO<sub>2</sub> adsorption capacity, 4.3 wt. %). By the formation of hierarchical pores and control of textural mesoporosity via the Fe/BDC ratio and synthesis temperature, this research paves the way for the synthesis of hierarchically porous MOFs with enhanced CO<sub>2</sub> adsorption capacity (A. Yurduşen & Yürüm, 2019).

#### 4.1. Background

The Intergovernmental Panel on Climate Change reported that the increase in CO<sub>2</sub> concentrations is a consequence of excessive consumption of fossil fuels and deforestation (M. Gupta, Coyle, & Thambimuthu, 2003). From the preindustrial period until today CO<sub>2</sub> concentrations have increased to 412 ppm, which was the highest CO<sub>2</sub> concentration measured in the last 650 years (Bachu, 2000; IEA & OECD, 2004). Reaching its highest concentration level and very long lifetime of CO<sub>2</sub>, has brought this gas into the spotlight. Particularly, water vapor can only stay in the atmosphere for 10 days, methane leaves the atmosphere in 10 years, and it takes 100 years for nitrous oxides to leave. However, in the case of CO<sub>2</sub>, 40% of CO<sub>2</sub> emissions remain in the atmosphere for 100 years while 10% of

the emissions remain even after 10 thousand years (Ciais et al., 2013). The CO<sub>2</sub> emissions we produce today cannot be removed completely which means CO<sub>2</sub> remains in the atmosphere past our lifetimes. Therefore, the need for alternative technologies to eliminate the increase in CO<sub>2</sub> concentrations and technologies that decrease CO<sub>2</sub> emissions has become crucial. Several strategies have been suggested to decrease CO<sub>2</sub> emissions: (i) developing energy systems that decrease energy intensity; (ii) decreasing carbon intensity by using low carbon fuels; (iii) developing renewable energy sources; and lastly (iv) developing technologies for CO<sub>2</sub> sequestration and capture (CCS) (Hongqun Yang et al., 2008). The Intergovernmental Panel on Climate Change has emphasized on the need for the development and improvement of technologies for CCS and highlighted that CO<sub>2</sub> emissions can only be decreased by 80 to 90% if power plants use carbon dioxide capture and storage technologies (Metz et al., 2005). Accordingly, researchers have focused their research on the development and improvement of CCS technologies which are formed from three different processes: (i) carbon dioxide capture; (ii) carbon dioxide separation; and (iii) transportation to its permanent storage site. The last step of CCS technologies has already been improved to pilot scale (Wilson, E. ; Gerard, 2007). However, carbon dioxide capture (i), and carbon dioxide separation (ii) still require further research. To decrease the cost of CCS, a considerable amount of effort has to be given to carbon dioxide capture and separation processes, and the most effective scenario would be achieved only if a material used in carbon dioxide capture achieves maximum separation efficiency.

Post-combustion CO<sub>2</sub> capture by amine solvents, oxyfuel combustion and calcium looping (D'Alessandro et al., 2010), membrane based separation, and adsorption are the most commonly used processes in carbon dioxide capture technologies. All of the processes involving absorption and chemical adsorption form CO<sub>2</sub> based products, while the temperature increases during the regeneration of CO<sub>2</sub> and results in increased separation costs (Force, 2009). In order to lower the cost, the formation of by-products should be minimized and in the long run should be eliminated. At that point, physical sorbents come to the forefront with their lower energy requirement and lack of by-product formation (S. Choi, Drese, & Jones, 2009a). Among the physical sorbents, those with high CO<sub>2</sub>/N<sub>2</sub> selectivity with high CO<sub>2</sub> uptake capacity have emerged. For instance, activated carbon is the most commonly used physical sorbent with a high surface area and pore volume. However, the low CO<sub>2</sub>/N<sub>2</sub> selectivity of this material limits its performance. Zeolites with a high BET

surface area and pore volume possess high CO<sub>2</sub>/N<sub>2</sub> selectivity. However, their low CO<sub>2</sub> uptake capacity limits their use in carbon dioxide capture technologies (S. Choi et al., 2009a; Force, 2009). Similar to activated carbons, polymer membranes possess high CO<sub>2</sub> sorption capacities. However, their low CO<sub>2</sub>/N<sub>2</sub> selectivity limits their use in CCS technologies (Force, 2009).

Metal-organic frameworks (MOFs) are formed by linking a metal ion or metal ion cluster with an organic linker. The combination of the metal part with the organic linker provides one-, two-, or three- dimensional networks. Depending on how building blocks are chosen, the structure of MOF crystallites varies, and pores can be easily tuned specific to the application that will be used (D. Yuan, Zhao, Sun, & Zhou, 2010; D. Zhao, Yuan, Sun, & Zhou, 2009). In addition to their tunability, their high surface area and pore volume make these materials promising in various applications such as drug delivery, gas storage and separation, catalysis, and molecular separation (Y. S. Bae & Snurr, 2011; Chughtai, Ahmad, Younus, Laypkov, & Verpoort, 2015; Corma et al., 2010; Farrusseng, Aguado, & Pinel, 2009; Jeongyong Lee et al., 2009; J. R. Li et al., 2009; Jiewei Liu et al., 2014; J. S. Seo et al., 2000; Taylor-Pashow et al., 2010; Yoon, Srirambalaji, & Kim, 2012; T. Zhang & Lin, 2014). Their high surface areas, high pore volumes, and easy tunability have brought MOFs to the fore among the porous materials. When compared to porous inorganic solids such as zeolites, MOFs possess lower chemical and thermal stability as a consequence of their coordination bonds. High selectivity and reduced heat capacity provide MOFs an edge over other sorbent materials such that the volumetric CO<sub>2</sub> adsorption capacity of MOF-177 at 35 bar have been measured to be 9 times greater than that of zeolite 13X (Millward & Yaghi, 2005b). Additionally, high CO<sub>2</sub> uptake capacities can only be achieved at low pressures when the surface of the pores has been functionalized accordingly. Therefore, synthesizing MOFs with moderate or high surface areas, high CO<sub>2</sub> selectivity and high CO<sub>2</sub> uptake capacities with decreased regeneration energy would provide a promising sorbent material for CCS technologies.

Constructed from oxo centered corner-sharing trimers of iron (III) (Horcajada et al., 2011), MIL-88B is a nontoxic, biodegradable MOF whose CO<sub>2</sub> uptake capacity has not been reported yet. Additionally, researchers mainly focused either on BET surface area or functional groups to enhance measured CO<sub>2</sub> uptake capacities. However, there is a few



efforts spent to understand the effect of narrow micropores (pore sizes < 1 nm) and pore size distribution on the adsorbed CO<sub>2</sub> amount.

In this study, we report of the role of narrow micropores (pore diameters < 1 nm) on CO<sub>2</sub> adsorption capacity. Hierarchical pores were formed by vigorously stirring iron salt, linker and DMF prior to solvothermal synthesis. Textural porosity of hierarchically porous MIL-88Bs is systematically tuned via Fe:BDC ratio and synthesis temperature. With the control of Fe:BDC ratio and synthesis temperature hierarchically porous MIL-88Bs with different pore size distribution were synthesized. CO<sub>2</sub> uptake measurements were conducted in between 0 and 5 bar at 298 K gravimetrically. The results were correlated with BET surface area, narrow micropore (pore diameter < 1 nm), micropore, mesopore and total pore volume. CO<sub>2</sub> adsorption capacity of hierarchically porous MIL-88Bs synthesized in our laboratories (BET: 400.4 m<sup>2</sup>/g, narrow micropore volume: 0.177 cm<sup>3</sup>/g) was compared with the CO<sub>2</sub> uptake capacities of commercially available MOFs. With our controlled synthesis strategy, the volume of narrow micropores was increased by 1.3 times (0.177 cm<sup>3</sup>/g) and the CO<sub>2</sub> uptake capacity was enhanced by a factor of 1.3.

Hierarchically porous MIL-88Bs synthesized in our laboratories (BET surface area: 400.4 m<sup>2</sup>/g) achieved a 5.58 wt.% of CO<sub>2</sub> uptake capacity (at 298 K and 1 bar), which is greater than the CO<sub>2</sub> adsorption capacities of commercially available MOFs and ZIFs. For instance, MOF-5 (BET surface area: 2833 m<sup>2</sup>/g CO<sub>2</sub> uptake capacity: 4.5 wt.% (Millward & Yaghi, 2005b)), MOF-177 (BET surface area: 5400 m<sup>2</sup>/g CO<sub>2</sub> uptake capacity: 3.6 wt.% (Mason, Sumida, Herm, Krishna, & Long, 2011a)) and lastly UMCM-1 (BET surface area: 4034 m<sup>2</sup>/g CO<sub>2</sub> uptake capacity: 3.8 wt.% (A. Ö. Yazaydin et al., 2009)), IRMOF-6 (Millward & Yaghi, 2005b), MIL-101(Cr) (B. Wang, Côté, Furukawa, O’Keeffe, & Yaghi, 2008), MIL-102 (Phan et al., 2010), MOF-2 (Millward & Yaghi, 2005b), ZIF-8 (Mason et al., 2011a), ZIF-71 (A. O. Yazaydin et al., 2009), ZIF-95 (Frost, Düren, & Snurr, 2006a), ZIF-97 (Frost et al., 2006a), and ZIF-100 (Trickett et al., 2017). The enhanced CO<sub>2</sub> adsorption capacity of hierarchically porous MIL-88Bs obtained in this study is attributed to relatively high fraction and volume of narrow micropores provided by the controlled synthesis strategy that tunes the textural mesoporosity of hierarchically porous MIL-88Bs via Fe:BDC ratio and synthesis temperature.

Here we report a controlled synthesis strategy that tunes the textural porosity and thereby, enhances the CO<sub>2</sub> adsorption capacity of hierarchically porous MIL-88Bs. Our

results are an experimental evidence that CO<sub>2</sub> uptake capacities can be controlled by the volume and distribution of narrow micropores (pore diameter < 1 nm).

## **4.2. Experimental**

Reproducibility of hierarchically porous MIL-88Bs was tested by the repetitive synthesis and characterization analysis. Each hierarchically porous MIL-88Bs was synthesized for five times. The characterization analysis of each synthesized hierarchically porous MIL-88Bs was repeated for five times. Average results of BET surface area, ultramicro-, micro-, uppermeso-, mesopore, and total pore volumes with calculated standard deviations were reported. The fractions of micro- and mesoporosity were estimated by the ratio of micro- and mesopore volume (NLDFT method) to total pore volume estimated by NLDFT method.

### **4.2.1. Materials**

All chemicals were used without the need of further purification. 98% pure (ACS Reagent grade) iron(III) chloride hexahydrate (FeCl<sub>3</sub>·6H<sub>2</sub>O) was purchased from Merck Millipore while 99.9% pure N, N-Dimethylformamide (DMF) (HPLC grade), and 99.8% pure methanol were purchased from Sigma Aldrich.

### **4.2.2. Synthesis of Hierarchically Porous MIL-88Bs**

Different from the regular MIL-88B synthesis (Bazin et al., 2013; C. Gao et al., 2017; Horcajada et al., 2011), NaOH was not used. 3.1 mmol of FeCl<sub>3</sub>·6H<sub>2</sub>O and (3.1 mmol, 1 mmol, 0.62 mmol) terephthalic acid were stirred vigorously via a magnetic stirrer with a stirring rate of 800 rpm in 80 mL of N, N-dimethylformamide (DMF) for an hour at 25 °C. Prepared solution and the precipitate were poured into 20 mL glass vials capped with Teflon caps. The prepared solutions were heated at 110, 130, and 150 °C in an isothermal oven for 2 days and then washed with DMF and methanol. Washing procedure lasted for 6 days and at the end of each 24-hour solvent was changed. After completing the solvent exchange

process, samples were thermally activated in vacuum oven at 100 °C for 30 hours. The following abbreviations listed in Table 12 are used for hierarchically porous MIL-88Bs synthesized at different temperatures with different Fe:BDC ratio.

Table 12. Abbreviations for the hierarchically porous MIL-88Bs synthesized at different temperatures with different Fe:BDC ratio.

| Sample Abbreviation | Synthesis Temperature (°C) | Fe:BDC ratio |
|---------------------|----------------------------|--------------|
| MIL-88B-110-1       | 110                        | 1            |
| MIL-88B-110-3       | 110                        | 3            |
| MIL-88B-110-5       | 110                        | 5            |
| MIL-88B-130-1       | 130                        | 1            |
| MIL-88B-130-3       | 130                        | 3            |
| MIL-88B-130-5       | 130                        | 5            |
| MIL-88B-150-1       | 150                        | 1            |
| MIL-88B-150-3       | 150                        | 3            |
| MIL-88B-150-5       | 150                        | 5            |

#### 4.2.3. Characterization of Hierarchically Porous MIL-88Bs

N<sub>2</sub> sorption isotherms, pore size distribution analysis, powder x-ray diffraction (PXRD), thermogravimetric analysis (TGA), Fourier transform infrared spectroscopy (FTIR), and scanning electron microscopy (SEM) were used to characterize MIL-88B type MOF crystallites. Gas sorption measurements were conducted by Intelligent Gravimetric Analyzer (IGA).

#### **4.2.3.1.X-Ray diffraction**

X-ray diffraction (XRD Bruker AXS GmbH D8 Advance, Karlsruhe, Germany) analysis was conducted with a 0.15406 nm Cu K $\alpha$  radiation, under a 40 kV X-ray generator voltage and 5 mA current in between a 2 $\theta$  range of 2 to 90° with a step size of 0.02°.

#### **4.2.3.2.Scanning Electron Microscopy (SEM)**

Leo Supra 35VP field emission scanning electron microscope was used for imaging. Voltage and working distance vary with the MIL-88B type MOF crystallite imaged.

#### **4.2.3.3.Brunauer-Emmett-Teller (BET) surface area and pore size distribution analysis**

Surface area and pore size distribution analysis were conducted by Micromeritics 3Flex Instrument. Prior to each analysis, hierarchically porous MIL-88Bs were degassed at 120 °C for 6 hours. For each analysis, 0.10 to 0.15 grams (g) of MIL-88B type MOF crystallites were used. N<sub>2</sub> sorption isotherms were obtained in between a relative pressure of 0 to 1 while for surface area analysis, BET model was used at which relative pressure ranged between 0.05 and 0.2. Pore size distribution analysis was conducted by NLDFT method.

#### **4.2.3.4.Fourier Transform Infrared Spectroscopy (FT-IR) Analysis**

FTIR analysis was conducted via Thermo Scientific Nicolet Is10 with a spectral resolution of 4 cm<sup>-1</sup> over a wavelength range of 600 to 4000 cm<sup>-1</sup>. Scans were repeated for 32 times and spectrum were corrected for background noise.

#### **4.2.3.5.Thermogravimetric Analysis (TGA)**

TGA was conducted with Shimadzu DTG-60H simultaneous thermal analysis TG-DTA equipment. A heating rate of 10 K was used, and analysis was conducted under a continuous flow of 20 mL/min N<sub>2</sub> gas in between 25 and 1200 °C.

#### **4.2.3.6.CO<sub>2</sub> Uptake Capacity Measurement**

Gravimetric gas sorption capacities were measured with Intelligent Gravimetric Analyzer (IGA). For accuracy, a microbalance head with  $\pm 1.0 \mu\text{g}$  sensitivity was placed in a stainless-steel vacuum pressure reactor. The CO<sub>2</sub> sorption studies were conducted for hierarchically porous MIL-88Bs with tuned pore sizes. Prior to each analysis, 25 to 30 mg of sample was outgassed at 120 °C for 6 hours. Static CO<sub>2</sub> sorption isotherms were measured at 25 °C within a relative pressure range of 0 to 5 bar.

### **4.3. Results and Discussion**

#### **4.3.1. XRD Analysis**

XRD patterns of hierarchically porous MIL-88Bs can be found below in Figure 45. Sharp peaks obtained at low angles match well with the characteristic peaks of MIL-88B. By vigorously stirring metal salt, linker and DMF prior to solvothermal synthesis, hierarchical pores were introduced by the aggregation of small sized crystallites. Aggregation of small sized crystallites show themselves by the broadened PXRD patterns.

PXRD patterns of hierarchically porous MIL-88Bs synthesized at different temperatures with different Fe:BDC ratio consist peaks located at similar peak positions. However, intensities of the peaks differed with Fe:BDC ratio and synthesis temperature. A high Fe:BDC ratio results in broadened Bragg peaks and synthesizing hierarchically porous MIL-88Bs with an Fe:BDC ratio of 1 result in decreased peak intensity. The differences observed in Bragg peak intensities are attributed to the changes in textural porosity.

Lastly, single crystal X-ray crystallography analyses confirmed that micro-sized single crystals were not formed and there were no metallic-iron present.

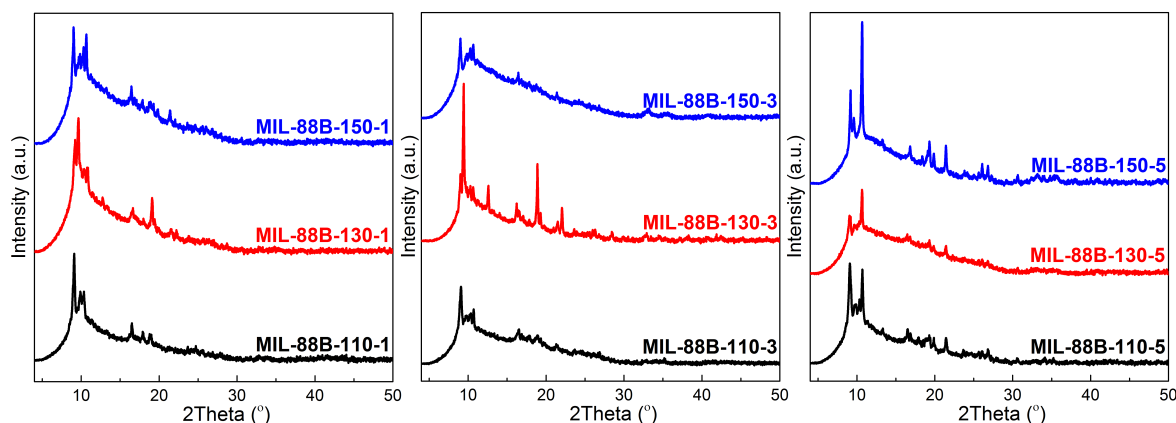


Figure 45. XRD pattern of hierarchically porous MIL-88Bs.

#### 4.3.2. SEM Imaging

Representative SEM images can be found in Figure 46. It is observed that morphology of hierarchically porous MIL-88Bs differs with Fe:BDC ratio and synthesis temperature. MIL-88B-110-1 possesses a rough surface while MIL-88B-130-1 has some cracks. By vigorously stirring the metal salt, linker and DMF, textural mesopores are formed. These textural mesopores are formed by the aggregation of small MOF crystallites. The nanosized rods of MIL-88B can be seen in the SEM images. Aggregated nanosized MIL-88Bs formed a hierarchical structure at which textural mesopores are present. The aggregated MOF crystallites can be seen clearly in the SEM images of MIL-88B-150-5. Formed majorly of organic linkers, MOF crystallites was not be imaged by TEM analysis.

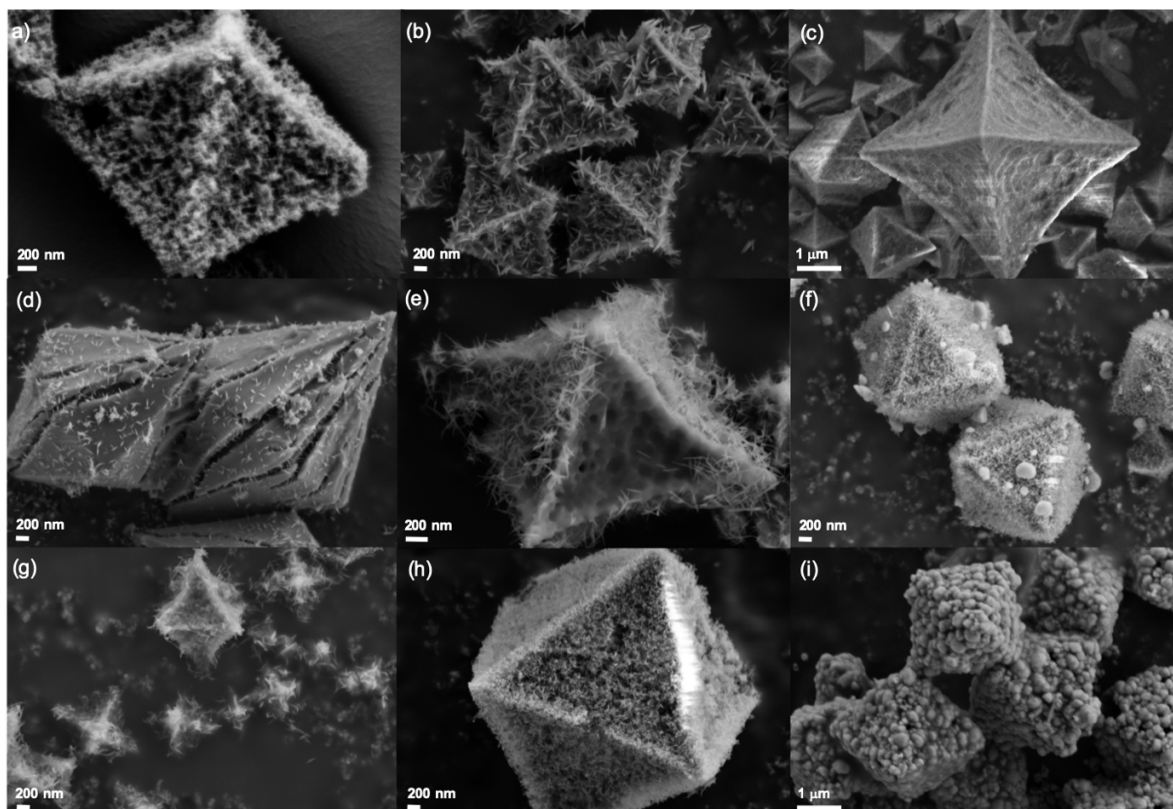


Figure 46. SEM images of hierarchically porous MIL-88Bs (a) MIL-88B-110-1, (b) MIL-88B-110-3, (c) MIL-88B-110-5, (d) MIL-88B-130-1, (e) MIL-88B-130-3, (f) MIL-88B-130-5, (g) MIL-88B-150-1, (h) MIL-88B-150-3, and (i) MIL-88B-150-5.

#### 4.3.3. Textural Properties

Different synthesis temperatures and different Fe:BDC ratios result differences in BET surface area, and textural porosity to be observed. Representative BET surface area, micro- and mesopore volume, total pore volume, and mesopore fraction are presented at Table 13.

Table 13. BET surface area, micropore area, micropore volume, and fraction of mesoporosity

| MOF           | BET Surface Area (m <sup>2</sup> /g) | Micropore Volume (cm <sup>3</sup> /g) | Mesopore Volume (cm <sup>3</sup> /g) | Total Pore Volume (cm <sup>3</sup> /g) | V <sub>meso</sub> (%) |
|---------------|--------------------------------------|---------------------------------------|--------------------------------------|----------------------------------------|-----------------------|
| MIL-88B-110-1 | 400.4±1.1E1                          | 0.182±1.4E-2                          | 0.017±1.4E-2                         | 0.19±2.0E-2                            | 8.3                   |
| MIL-88B-110-3 | 452.4±1.9E1                          | 0.239±3.2E-2                          | 0.0096±7.0E-3                        | 0.25±1.2E-2                            | 3.9                   |
| MIL-88B-110-5 | 445.9±1.9E1                          | 0.202±3.2E-2                          | 0.028±1.7E-2                         | 0.23±2.2E-2                            | 12.3                  |
| MIL-88B-130-1 | 265.4±2.6E1                          | 0.114±6.5E-3                          | 0.25±9.7E-3                          | 0.36±1.1E-1                            | 68.8                  |
| MIL-88B-130-3 | 249.4±1.6E1                          | 0.115±1.6E-2                          | 0.13±5.5E-2                          | 0.24±8.5E-2                            | 52.8                  |
| MIL-88B-130-5 | 283.1±2.6E1                          | 0.108±2.8E-3                          | 0.66±4.3E-2                          | 0.77±2.0E-2                            | 86.0                  |
| MIL-88B-150-1 | 357.1±7.8E1                          | 0.143±4.6E-2                          | 0.49±3.1E-1                          | 0.63±2.6E-1                            | 77.4                  |
| MIL-88B-150-3 | 346.3±1.7E1                          | 0.149±2.3E-2                          | 0.67±3.6E-1                          | 0.81±3.0E-1                            | 81.7                  |
| MIL-88B-150-5 | 117.7±1.9                            | 0.0355±9.0E-3                         | 0.25±2.7E-2                          | 0.28±1.8E-2                            | 87.4                  |

#### 4.3.3.1. N<sub>2</sub> sorption isotherms

Representative N<sub>2</sub> sorption isotherms of hierarchically porous MIL-88Bs are illustrated at Figure 47-50. Hierarchically porous MIL-88Bs synthesized at different temperatures with different Fe:BDC ratio show significant changes in their N<sub>2</sub> sorption isotherms.



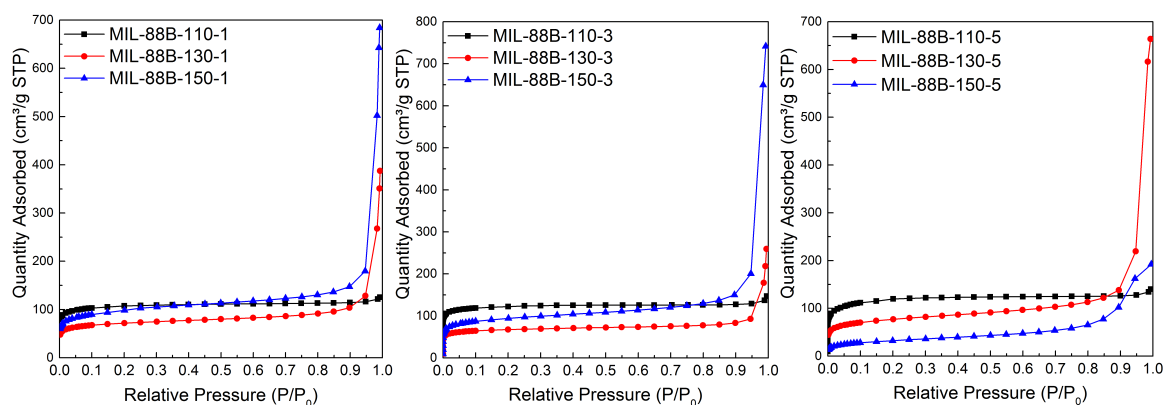


Figure 47. N<sub>2</sub> sorption isotherms of hierarchically porous MIL-88Bs.

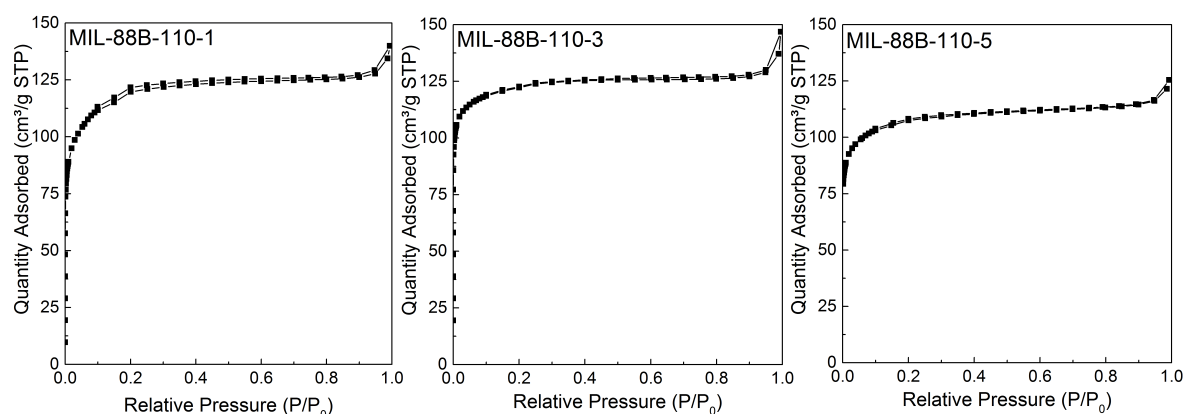


Figure 48. N<sub>2</sub> sorption isotherms of MIL-88B-110-1, MIL-88B-110-3, and MIL-88B-110-5.

N<sub>2</sub> sorption isotherms of MIL-88B-110-1, MIL-88B-110-3, and MIL-88B-110-5 (Figure 48) follow characteristic features of IUPAC type I isotherms with some amount of mesoporosity present. N<sub>2</sub> sorption isotherms possess high N<sub>2</sub> uptakes at low relative pressures. For relative pressures ranging between 0.2 and 0.9 almost horizontal plateau parallel to relative pressure axis is achieved. Lastly, at pressures close to saturation pressure a steep N<sub>2</sub> uptake is observed.

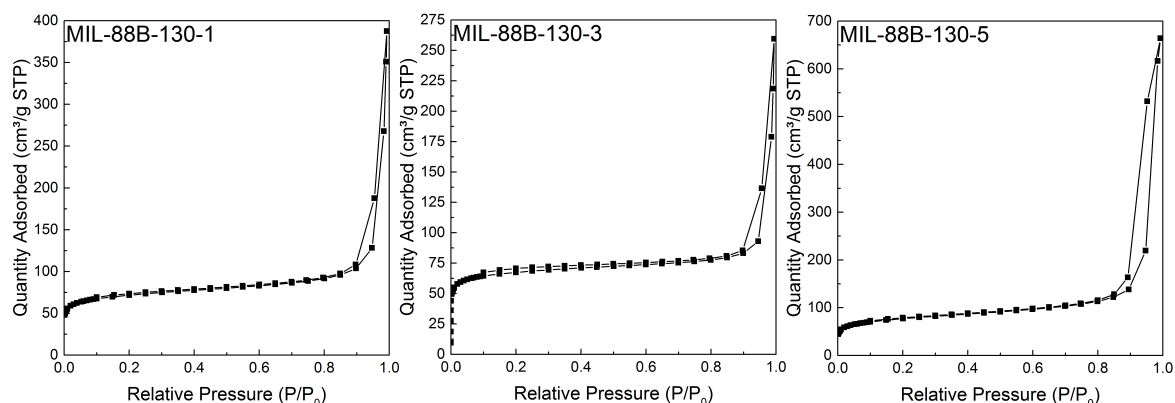


Figure 49. N<sub>2</sub> sorption isotherms of MIL-88B-130-1, MIL-88B-130-3, and MIL-88B-130-5.

MIL-88B-130-1, MIL-88B-130-3, and MIL-88B-130-5 possess the characteristic IUPAC type IV isotherms with some microporosity present (Figure 49). Presence of hysteresis loop points out the presence of mesopores. The high N<sub>2</sub> sorption capacities at low relative pressures reveals that micropores are present in the pore structure of MIL-88B-130-1, MIL-88B-130-3, and MIL-88B-130-5. Slope observed in between the relative pressure range of 0.2 and 0.9 is associated with mesopore filling. The steep increase observed close to saturation pressure is associated with mesopores at the upper mesopore size range.

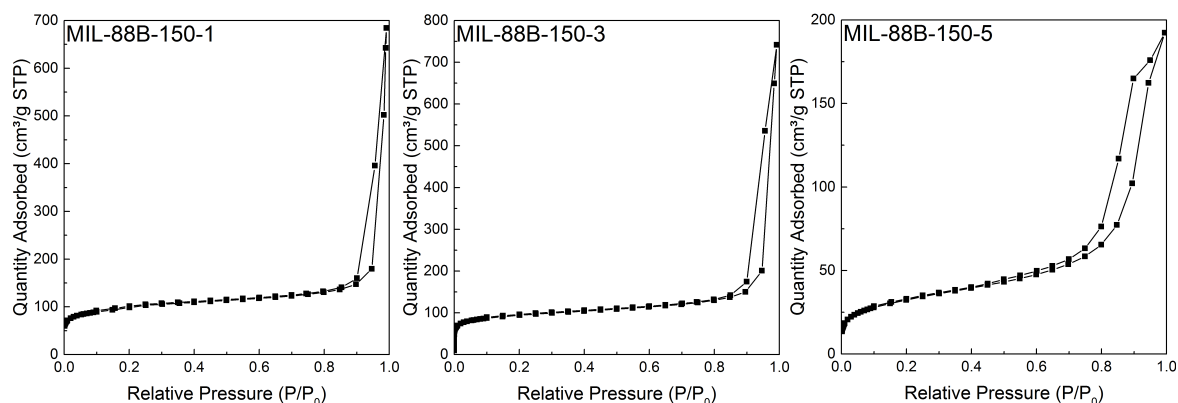


Figure 50. N<sub>2</sub> sorption isotherms of MIL-88B-150-1, MIL-88B-150-3, and MIL-88B-150-5.

Hierarchically porous MIL-88Bs synthesized at 150 °C show the typical features of IUPAC type IV isotherms with some microporosity present (Figure 50). Hysteresis loops present in the N<sub>2</sub> sorption isotherms are due to pore condensation and therefore is attributed to the presence of mesopores. Steep N<sub>2</sub> uptake at low relative pressures illustrates that the micropores are present. Slope obtained in between the relative pressure range of 0.2 and 0.9

and the steep uptake close to saturation pressure demonstrates that MIL-88B-150-1, MIL-88B-150-3, and MIL-88B-150-5 are formed of mesopores.

As synthesis temperature and Fe:BDC ratio differ, significant changes in N<sub>2</sub> sorption isotherms are observed. These changes are attributed to changes occurred in textural mesoporosity. N<sub>2</sub> sorption isotherms show some typical features of mesopores when hierarchically porous MIL-88Bs were synthesized at temperatures higher than 110 °C illustrating the developed textural mesoporosity. In order to assess micropore volumes, t-plot method is used at which amount of N<sub>2</sub> adsorbed is plotted with respect to statistical thickness. Representative t-plots are shown in Figure 51.

#### 4.3.3.2.t-plot method

For micropore volume estimations statistical thickness is used. Harkins and Jura thickness equation is used at which “*t*” represents statistical thickness and “*P/P<sub>0</sub>*” stands for relative pressure (Lowell et al., 2004a). Table 14 illustrates micropore volumes, slope, y-intercept values and correlation coefficients for respective t-plot method estimations.

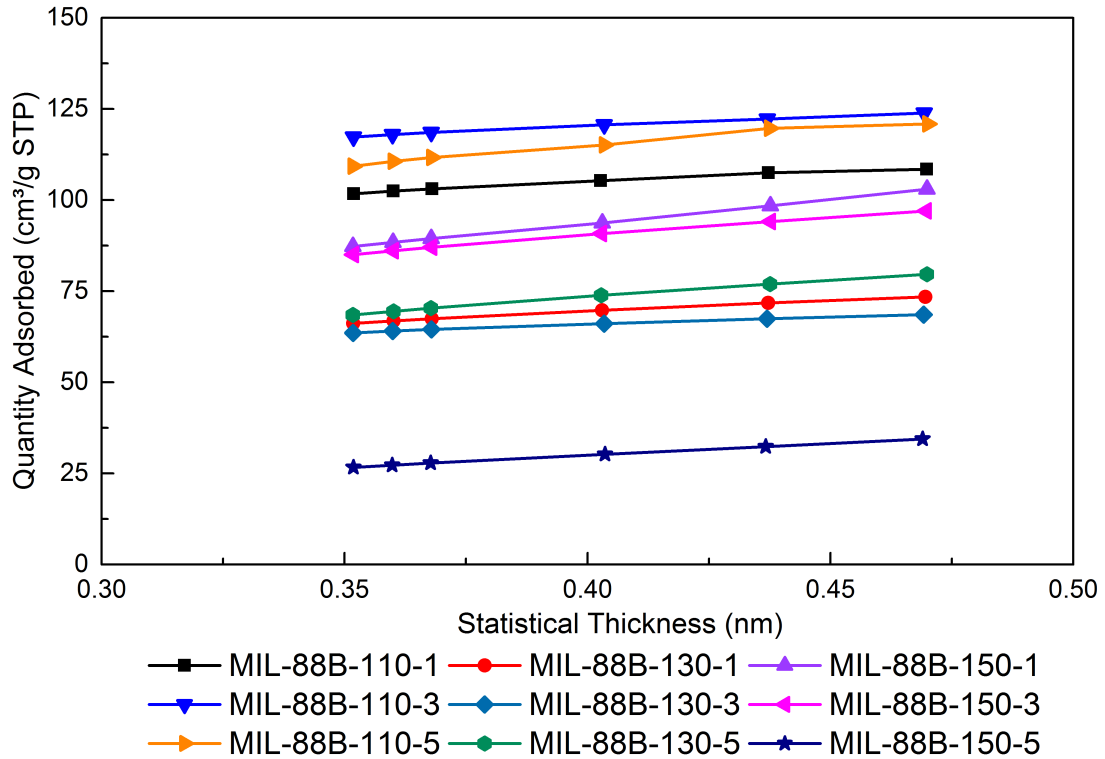


Figure 51. t-plots of hierarchically porous MIL-88Bs

Table 14. Micropore volume, slope, y-intercept, and correlation coefficient estimated by t-plot method.

| MOF           | Micropore Volume (cm <sup>3</sup> /g) | Slope (cm <sup>3</sup> /g.nm) <sup>[a]</sup> | Y intercept (cm <sup>3</sup> /g.nm) <sup>[a]</sup> | Correlation Coefficient |
|---------------|---------------------------------------|----------------------------------------------|----------------------------------------------------|-------------------------|
| MIL-88B-110-1 | 0.13±1.4E-2                           | 58.2±3.9                                     | 81.6±1.8                                           | 0.991                   |
| MIL-88B-110-3 | 0.15±3.4E-2                           | 54.9±2.0                                     | 98.2±8.0E-1                                        | 0.997                   |
| MIL-88B-110-5 | 0.114±3.2E-2                          | 101.6±7.5                                    | 74.1±3.0                                           | 0.989                   |
| MIL-88B-130-1 | 0.069±1.9E-2                          | 61.6±2.1                                     | 44.7±8.4E-1                                        | 0.998                   |
| MIL-88B-130-3 | 0.076±1.7E-2                          | 42.0±1.6                                     | 48.98±6.4E-1                                       | 0.997                   |
| MIL-88B-130-5 | 0.055±1.7E-2                          | 94.3±2.5                                     | 35.6±1.0                                           | 0.999                   |
| MIL-88B-150-1 | 0.063±1.7E-2                          | 131.8±1.8                                    | 40.9±7.0E-1                                        | 0.999                   |
| MIL-88B-150-3 | 0.077±1.7E-2                          | 101.5±2.5                                    | 49.5±1.0                                           | 0.999                   |
| MIL-88B-150-5 | 0.0054±1.0E-3                         | 13.0±6.3E-1                                  | 3.5±2.5E-1                                         | 0.995                   |

*[a] At standard temperature and pressure (STP)*

Dots that deviated towards downwards illustrate the presence of micropores. In the meantime, deviations from the linear regime reveal the presence of mesopores. Presence of two linear parts confirm both micro- and mesopores exist in pore structure. The highest intercept value belongs to MIL-88B-110-3.

#### 4.3.3.3.NLDFT method

Figure 52 to 60 represents NLDFT plots of hierarchically porous MIL-88Bs. Volume of narrow micropores (pore diameters < 1 nm), micro-, and mesopores can be found below at Table 15. Additionally, volume of mesopores at the upper mesopore size range and their distribution within mesopores and the whole pore size range are illustrated at Table 16.

Table 15. Micro- and mesopore volume, fraction of micro- and mesoporosity estimated by NLDFT method

| MOF           | Volume of pores<br>< 1 nm (cm <sup>3</sup> /g) | Micropore<br>Volume (cm <sup>3</sup> /g) | Mesopore<br>Volume (cm <sup>3</sup> /g) | Vmicro<br>(%) | Vmeso<br>(%) |
|---------------|------------------------------------------------|------------------------------------------|-----------------------------------------|---------------|--------------|
| MIL-88B-110-1 | 0.177±1.7E-2                                   | 0.182±1.4E-2                             | 0.016±1.4E-2                            | 91.7          | 8.3          |
| MIL-88B-110-3 | 0.226±1.2E-2                                   | 0.239±3.2E-2                             | 0.0096±7.0E-3                           | 96.1          | 3.9          |
| MIL-88B-110-5 | 0.172±1.7E-2                                   | 0.202±3.2E-2                             | 0.028±1.7E-2                            | 87.7          | 12.3         |
| MIL-88B-130-1 | 0.113±1.6E-2                                   | 0.1137±6.5E-3                            | 0.25±9.7E-3                             | 31.2          | 68.8         |
| MIL-88B-130-3 | 0.107±2.6E-2                                   | 0.115±1.6E-2                             | 0.13±5.5E-2                             | 47.2          | 52.8         |
| MIL-88B-130-5 | 0.108±1.1E-2                                   | 0.108±2.8E-3                             | 0.66±4.3E-2                             | 14.0          | 86.0         |
| MIL-88B-150-1 | 0.142±3.7E-2                                   | 0.143±4.6E-2                             | 0.49±3.0E-1                             | 22.6          | 77.4         |
| MIL-88B-150-3 | 0.137±3.2E-2                                   | 0.149±2.2E-2                             | 0.67±3.6E-1                             | 18.3          | 81.7         |
| MIL-88B-150-5 | 0.023±1.8E-2                                   | 0.0355±9.0E-3                            | 0.25±2.7E-2                             | 12.6          | 87.4         |

Table 16. Volume of mesopores at the upper mesopore size range, and their distribution within mesopores and the whole pore size range.

| MOF           | Vupper (cm <sup>3</sup> /g) <sup>[a]</sup> | Vmesopore (cm <sup>3</sup> /g) | Vupper/Vmeso <sup>[b]</sup> | Vupper/Vtotal <sup>[c]</sup> |
|---------------|--------------------------------------------|--------------------------------|-----------------------------|------------------------------|
| MIL-88B-110-1 | 0.0060±5.7E-05                             | 0.017±1.4E-2                   | 0.36                        | 0.030                        |
| MIL-88B-110-3 | 0.0062±5.0E-3                              | 0.0096±7.0E-3                  | 0.64                        | 0.024                        |
| MIL-88B-110-5 | 0.0066±1.2E-3                              | 0.028±1.7E-2                   | 0.23                        | 0.029                        |
| MIL-88B-130-1 | 0.20 ±1.3E-1                               | 0.25±9.7E-3                    | 0.81                        | 0.55                         |
| MIL-88B-130-3 | 0.11±7.0E-2                                | 0.13±5.5E-2                    | 0.83                        | 0.43                         |
| MIL-88B-130-5 | 0.56 ±5.0E-3                               | 0.66±4.3E-2                    | 0.85                        | 0.73                         |
| MIL-88B-150-1 | 0.43 ±2.9E-1                               | 0.49±3.1E-1                    | 0.87                        | 0.68                         |
| MIL-88B-150-3 | 0.65 ±3.4E-1                               | 0.67±3.6E-1                    | 0.96                        | 0.79                         |
| MIL-88B-150-5 | 0.045±2.0E-2                               | 0.25±2.7E-2                    | 0.185                       | 0.16                         |

[a] Volume of mesopores at the upper mesopore size range (cm<sup>3</sup>/g)

[b] Volume ratio of mesopores at the upper mesopore size range to mesopores

[c] Volume ratio of mesopores at the upper mesopore size range to total pore volume

### Hierarchically porous MIL-88Bs synthesized at 110 °C

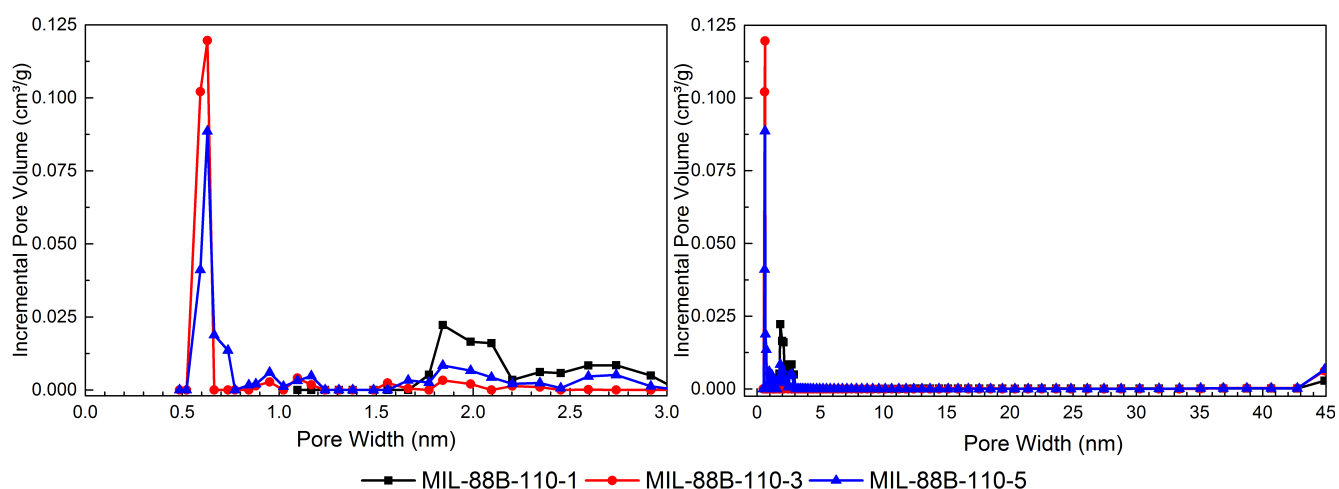


Figure 52. NLDFT plot of hierarchically porous MIL-88Bs synthesized at 110 °C.

Hierarchically porous MIL-88Bs synthesized at 110 °C are formed mostly of micropores. The lowest fraction of textural mesoporosity belongs to MIL-88B-110-3. The volume of narrow micropores and their distribution through the micropore size distribution differ with Fe:BDC ratio. Fraction of narrow micropores ( $V_{\text{pores} < 1 \text{ nm}} / V_{\text{pores} < 2 \text{ nm}}$ ) is the highest in MIL-88B-110-1 and the lowest in MIL-88B-110-5. In the meantime, mesopore volume increases by a factor 2.9 when MIL-88B type MOF crystallites were synthesized with an Fe:BDC ratio of 5.

### Hierarchically porous MIL-88Bs synthesized at 130 °C

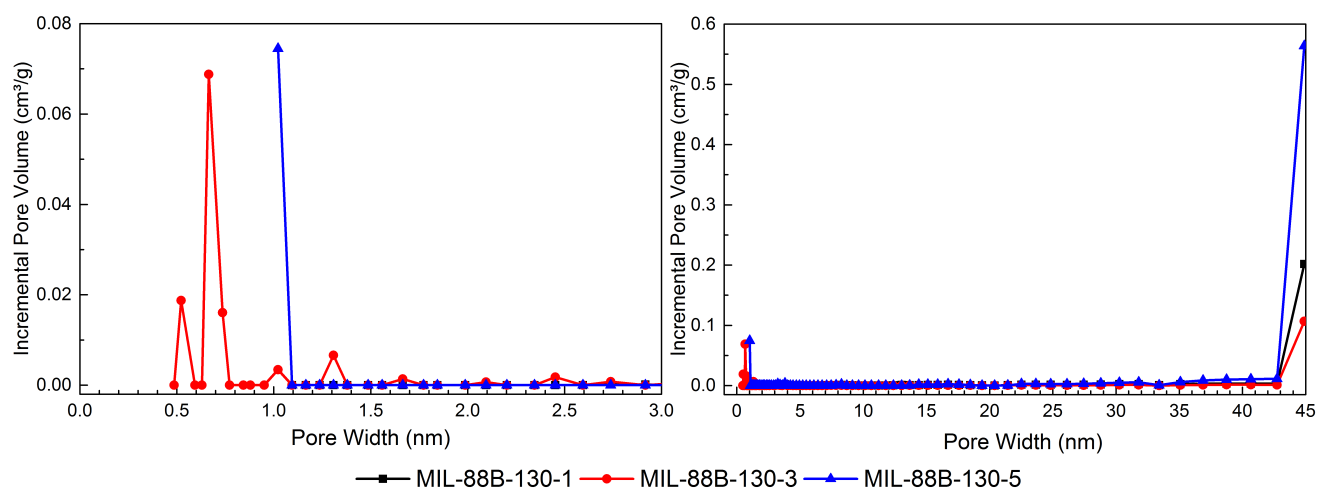


Figure 53. NLDFT plot of hierarchically porous MIL-88Bs synthesized at 130 °C.

The highest volume increase in the upper mesopore size range is attained by MIL-88B-130-5 while MIL-88B-130-3 obtained the lowest. Mesopore volume of MIL-88B-130-5 is 5.1 and 2.9 times higher than the mesopore volume of MIL-88B-130-1 and MIL-88B-130-3, respectively.

The fraction of pores with pore diameters narrower than 1.0 nm corresponds to 31.3% of the total pore volume in MIL-88B-130-1. Additionally, mesopore volume of MIL-88B-130-1 is 15 times higher than the mesopore volume of MIL-88B-110-1 illustrating that the synthesis temperatures higher than 110 °C resulted in pore widening.

### Hierarchically porous MIL-88Bs synthesized at 150 °C

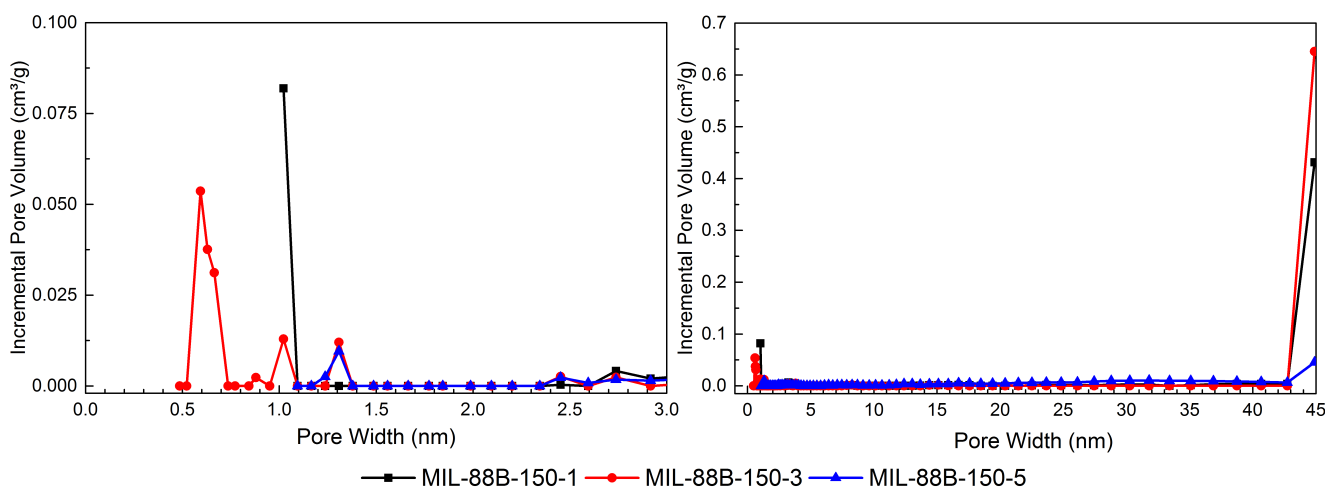


Figure 54. NLDFT plot of hierarchically porous MIL-88Bs synthesized at 150 °C.

MIL-88B-150-1, MIL-88B-150-3, and MIL-88B-150-5 are formed mostly of mesopores, 77.4%, 81.7%, and 87.4%, respectively. Volume of narrow micropores (pore diameter < 1 nm) corresponds to 22.5% of the total pore volume in MIL-88B-150-1 while mesopores at the upper mesopore size range (42 nm < pore diameter < 44 nm) occupy 0.43 cm<sup>3</sup>/g of volume and form 68.1% of the total pore volume. Similar to MIL-88B-150-1, the volume increment in the upper mesopore size range corresponds to 79% of the total pore volume which make us conclude that the major volume contribution of pores arises from mesopores at the upper mesopore size range. Even though mesopores form 87.4% of the total pore volume in MIL-88B-150-5, volume contribution of mesopores at the upper mesopore range is relatively low.

Similar to the trend observed in hierarchically porous MIL-88Bs synthesized at 110, and 130 °C, among the hierarchically porous MIL-88Bs synthesized at 150 °C, MIL-88B-150-5 possesses the highest fraction of textural mesoporosity. Micropore volume of MIL-88B-150-5 is 4.0, and 4.2 times lower than the micropore volume of MIL-88B-150-1, and MIL-88B-150-3, respectively.



### Hierarchically porous MIL-88Bs synthesized with an Fe:BDC ratio of 1

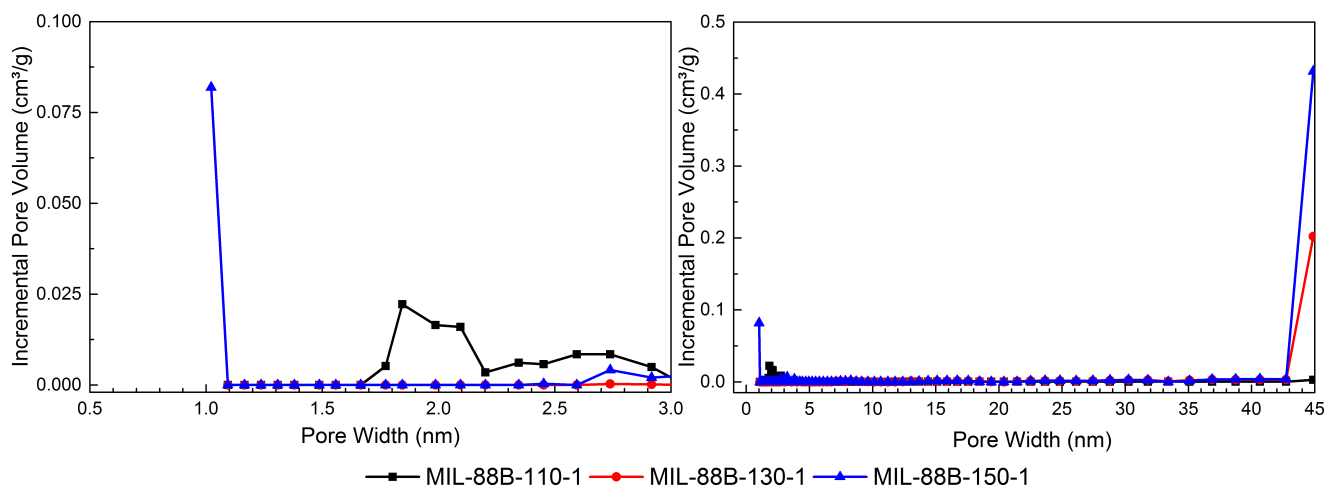


Figure 55. NLDFT plot of hierarchically porous MIL-88Bs synthesized with an Fe:BDC ratio of 1.

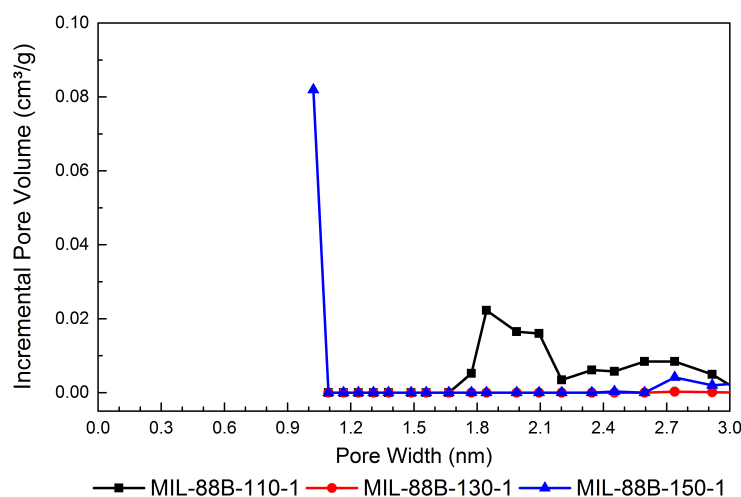


Figure 56. NLDFT plot of MIL-88B-110-1, MIL-88B-130-1, and MIL-88B-150-1.

The highest total pore volume belongs to MIL-88B-150-1. However, its micropore fraction is significantly lower than MIL-88B-110-1. Higher pore volume of MIL-88B-150-1 is associated with its relatively high mesopore volume. MIL-88B-110-1 is formed 91.7% of micropores while MIL-88B-130-1, and MIL-88B-150-1 possess 31.3% and 22.5% microporosity, respectively. A remarkable decrease in textural mesopore volume occurs when hierarchically porous MIL-88Bs were synthesized at lower synthesis temperatures (110 °C). This drastic decrease in mesopore fraction indicates that mesopore formation is promoted at temperatures higher than 110 °C. Mesopore volume of MIL-88B-110-1 is 30

times lower than the mesopore volume of MIL-88B-150-1. MIL-88B-110-1 possesses 8.3% of mesoporosity which is significantly lower than the mesopore fraction of MIL-88B-130-1, and MIL-88B-150-1. It is found that mesopores are the main contributors to the total pore volume in MIL-88B-130-1, MIL-88B-150-1 while micropores dominated the pore structure in MIL-88B-110-1.

### Hierarchically porous MIL-88Bs synthesized with an Fe:BDC ratio of 3

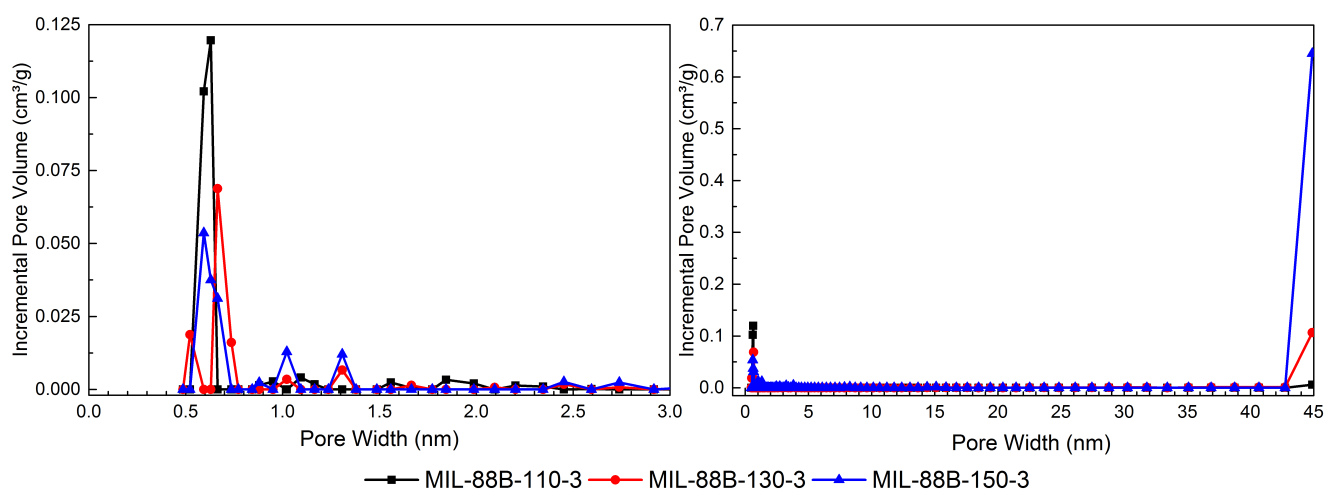


Figure 57. NLDFT plot of hierarchically porous MIL-88Bs synthesized with an Fe:BDC ratio of 3.

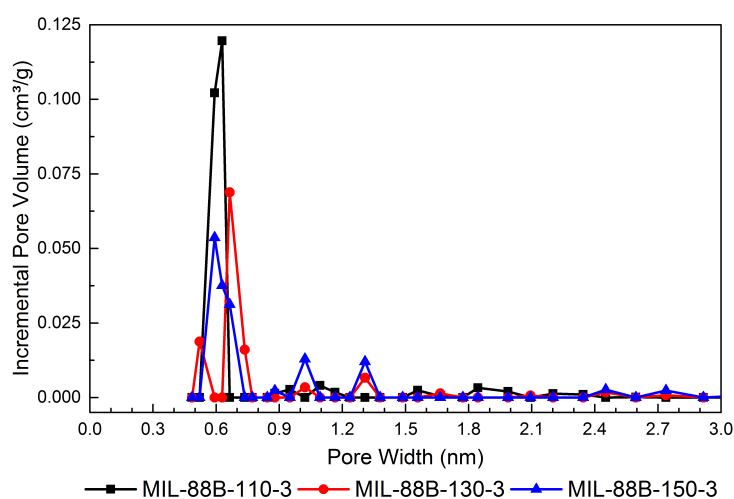


Figure 58. NLDFT plot of MIL-88B-110-3, MIL-88B-130-3, and MIL-88B-150-3.

Hierarchically porous MIL-88Bs synthesized with an Fe:BDC ratio of 3 are formed of pores as small as 0.59 nm. Pores smaller than 0.59 nm contribute to 40.9, 10.2, and 6.6%

increase in total pore volume in MIL-88B-110-3, MIL-88B-130-3, and MIL-88B-150-3, respectively. MIL-88B-110-3, MIL-88B-130-3, and MIL-88B-150-3 are formed 96.1, 36.7, and 18.3% of micropores, respectively. MIL-88B-130-3, and MIL-88B-150-3 are dominantly formed of mesopores and show remarkable increase in their pore volume within mesoporous pore size range. Particularly, MIL-88B-130-3, and MIL-88B-150-3 are formed 52.8% and 81.7% of mesopores, respectively. The highest volume increase in the mesoporous range occurs at the upper mesopore size range ( $42\text{ nm} < \text{pore diameter} < 44\text{ nm}$ ). For instance, the highest volume increase which corresponds to 79% of the total pore volume of MIL-88B-150-3 belongs to pores with pore diameters ranging between 42.7 and 44.9 nm. Identical to MIL-88B-150-3, MIL-88B-130-3 experiences a volume increase at the upper mesopore range that corresponds to 43.0% of the total pore volume while volume increase in upper mesopore size range of MIL-88B-10-3 is insignificant in comparison to the volume increase observed in MIL-88B-130-3, and MIL-88B-150-3. In conclusion, when hierarchically porous MIL-88Bs were synthesized at temperatures higher than  $110\text{ }^{\circ}\text{C}$ , pore widening is observed, mesopore volume and fraction of mesopores at the upper mesopore size range increases.

#### Hierarchically porous MIL-88Bs synthesized with an Fe:BDC ratio of 5

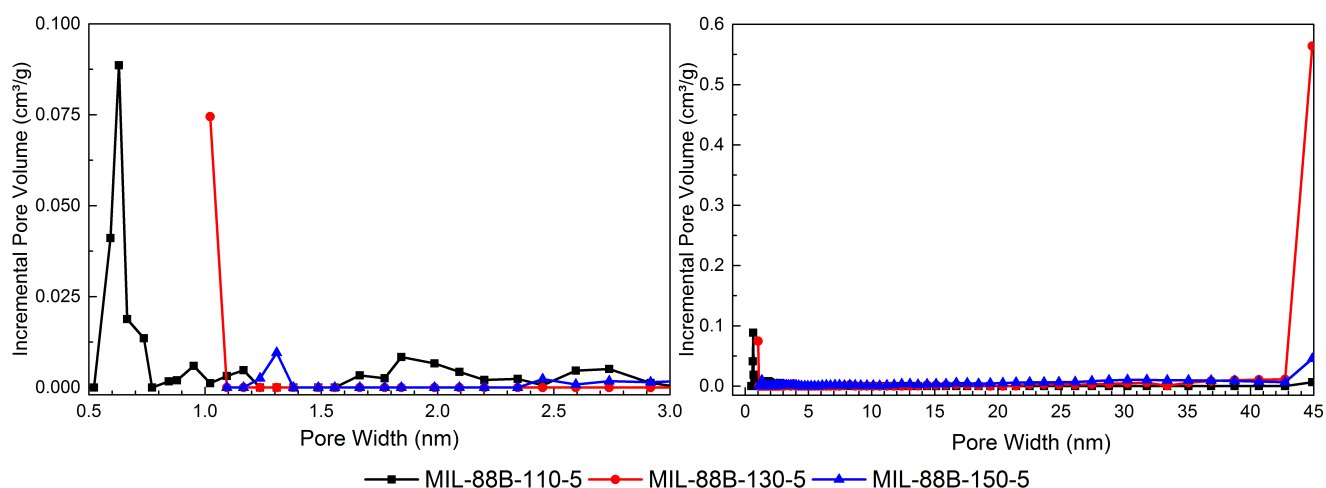


Figure 59. NLDFT plot of hierarchically porous MIL-88Bs synthesized with an Fe:BDC ratio of 5.

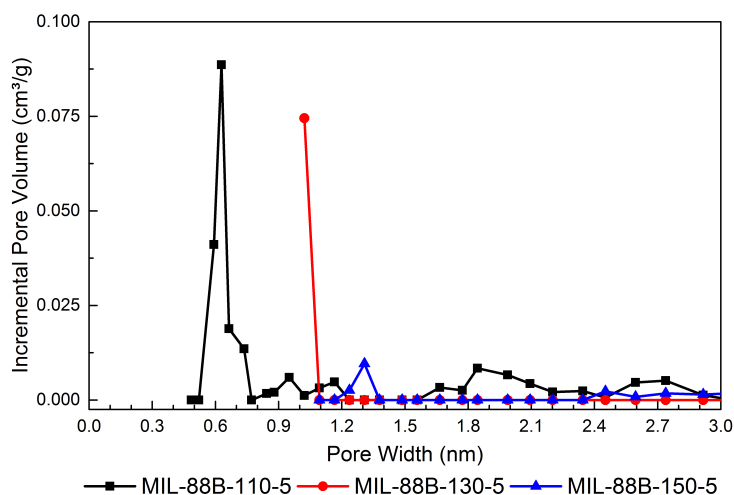


Figure 60. NLDFT plot of MIL-88B-110-5, MIL-88B-130-5, and MIL-88B-150-5.

The highest volume increase in microporous range belongs to MIL-88B-110-5 which is  $0.20 \text{ cm}^3/\text{g}$ . The micropore volume of MIL-88B-110-5 is 2 and 5.7 times more than the micropore volume of MIL-88B-130-5, and MIL-88B-150-5, respectively. In the same manner of hierarchically porous MIL-88Bs synthesized at 110, and 130 °C, the highest fraction of mesopores (87.4%) belongs to MIL-88B-150-5.

#### 4.3.3.4. Impact of Fe/BDC ratio on the pore size distribution

Pore size distribution analysis shows that fraction of mesopores increases with increasing Fe:BDC ratio. Among the MIL-88B type MOF crystallites synthesized at three different temperatures (110, 130, and 150 °C), MOF crystallites synthesized with an Fe:BDC ratio of 5 possess the highest fraction of textural mesoporosity. We have attributed the increased mesoporosity to the presence of excess amount of iron salt which competes for BDC. In a study conducted by Choi et al., it was shown that excess Zn clusters compete for the ligand that has already played a role in MOF-5 crystal formation which results in decreased crystallinity and decreased BET surface area (J. S. Choi, Son, Kim, & Ahn, 2008). In another study conducted by Wu et. al., it was showed that in the absence of the linkers, positively charged vacancy sites would be balanced by -OH groups (H. Wu et al., 2013). From this point of view, we have attributed the increased textural mesoporosity to the presence of excess iron salts competing for BDC. As the iron amount increases, iron oxide clusters start to form which would later compete for BDC.

#### **4.3.3.5. Impact of synthesis temperature on pore size distribution**

Prouzet and Pinnavaia showed the temperature dependence of pore structures in MSU-X silicas. Synthesizing MSU-X silicas at high temperatures resulted pore sizes to increase, and disorganized pore structures with broader pore size distribution to form (Prouzet & Pinnavaia, 1997). Similarly, Mahata et. al. showed that synthesizing MOFs at high temperatures cause number of water molecules present in the MOF structure (coordinated and uncoordinated) to decrease and coordination around the central metal ions to change (Mahata et al., 2008).

In another study conducted by Cao et. al., the size of mesopores were found to be dependent on the synthesis temperature. High synthesis temperatures resulted nanoparticles to pack loosely and larger mesopores to form. On the contrary, conducting the synthesis at relatively low synthesis temperatures resulted nanoparticles to pack tightly and smaller pores to form (Cao et al., 2016).

In line with what has been reported in the literature, NLDFT pore size distribution analysis illustrates that conducting the synthesis at relatively low temperatures (110 °C) limited the growth of mesopores, cause nanoparticles to pack tightly leading to an increase in the fraction of microporosity whereas synthesizing hierarchically porous MIL-88Bs at high synthesis temperatures (temperatures greater than 130 °C) results nanoparticles to pack loosely, pores to widen and fraction of mesopores to increase.

By synthesizing hierarchically porous MIL-88Bs at 110°C, the lowest fraction of textural mesoporosity is achieved. In the meantime, synthesizing hierarchically porous MIL-88Bs at temperatures higher than 110 °C formed MOF crystallites with increased fraction of mesoporosity with wider pores dominating the pore structure.

NLDFT analysis reveals that synthesis temperature plays a key role in the textural porosity formation mechanism in MIL-88B type MOF crystallites. Synthesizing MIL-88B type MOF crystallites at high temperatures (synthesis temperature > 130 °C) increased the fraction of textural mesoporosity.

#### 4.3.4. FTIR Analysis

Changes in wavelength intensities reveals the structural changes in hierarchically porous MIL-88Bs. FTIR spectra of hierarchically porous MIL-88Bs can be found in Figure 61, 62, and 63.

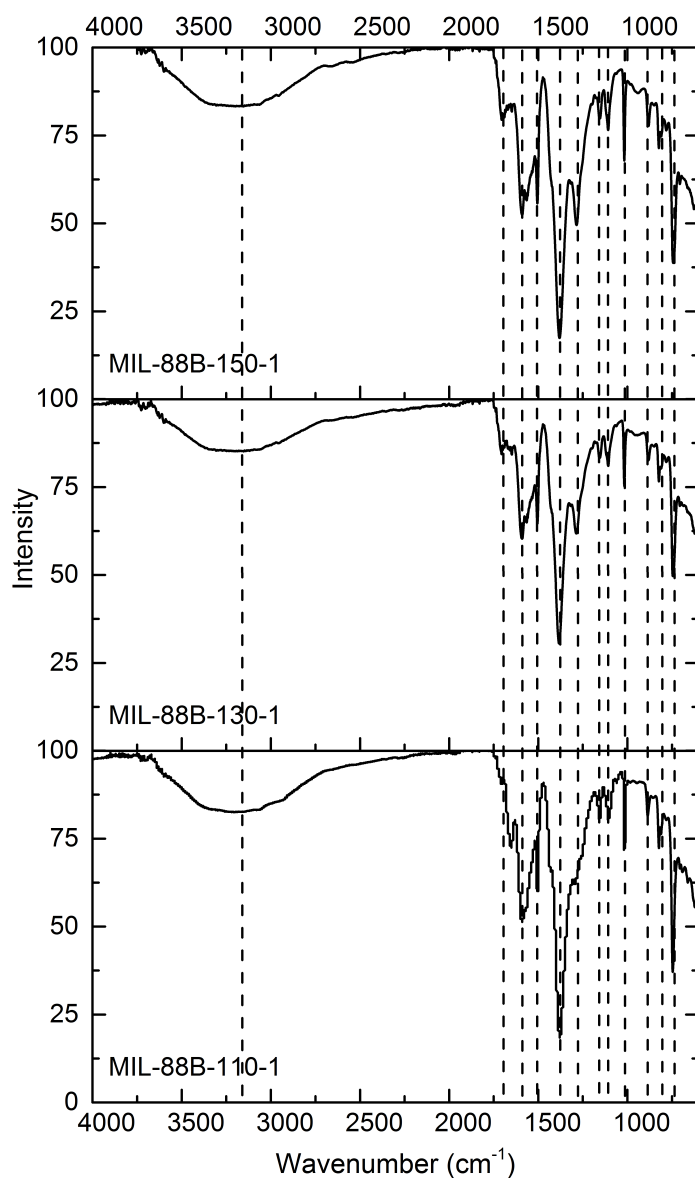


Figure 61. FTIR spectra of hierarchically porous MIL-88Bs synthesized with an Fe:BDC ratio of 1.

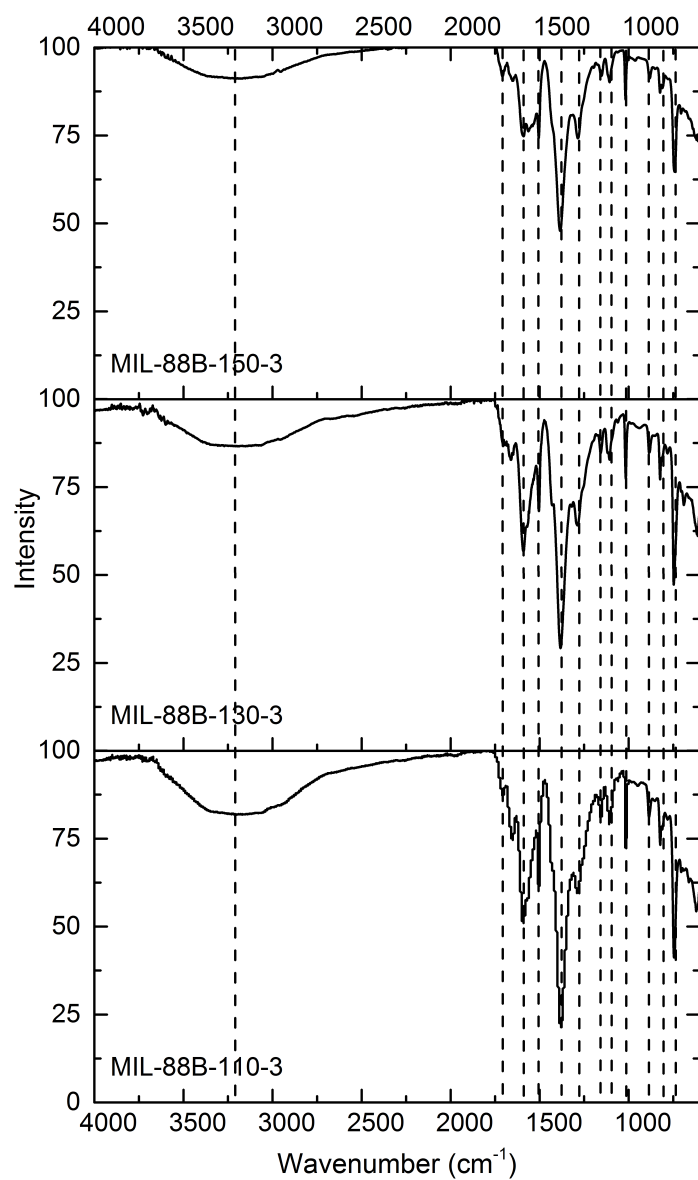


Figure 62. FTIR spectra of hierarchically porous MIL-88Bs synthesized with an Fe:BDC ratio of 3.

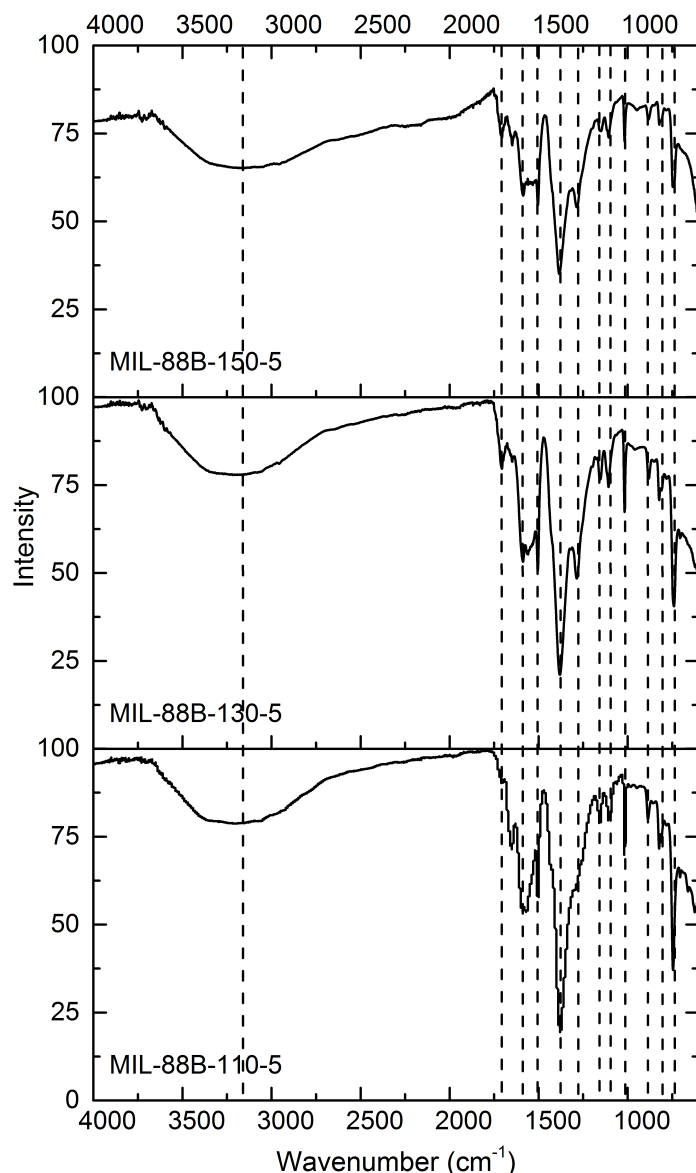


Figure 63. FTIR spectra of hierarchically porous MIL-88Bs synthesized with an Fe:BDC ratio of 5.

Differences in Fe:BDC ratio result band widths and peak intensities to differ. More importantly, the peak at  $1704\text{ cm}^{-1}$  points out the structural changes occurred with Fe:BDC ratio and synthesis temperature. The broad band in between  $3000$  and  $3600\text{ cm}^{-1}$  is assigned to OH groups involved in H-bonds. Hierarchically porous MIL-88Bs synthesized with an Fe:BDC ratio of 5 possess broader OH band in between  $3000$  and  $3600\text{ cm}^{-1}$ . In the meantime, peak intensity of the broadened OH band is lower than the OH band peak intensity of hierarchically porous MIL-88Bs synthesized with lower Fe:BDC ratios. A broadened OH band is a consequence of increased number of unsaturated metal sites and widened pores and



expectedly, hierarchically porous MIL-88Bs synthesized with an Fe:BDC ratio of 3 have the narrowest band width which is in line with our conclusions. Peaks neither at 1063 nor at 2861  $\text{cm}^{-1}$  are present which proved that DMF molecules are successfully removed from the pores. There are no peaks at 1704  $\text{cm}^{-1}$  in the FTIR spectra of hierarchically porous MIL-88Bs synthesized at 110  $^{\circ}\text{C}$  which is attributed to free BDC acid and absence of this peak indicates that almost all  $\text{H}_2\text{BDC}$  is deprotonated. In the meantime, FTIR spectra of hierarchically porous MIL-88Bs synthesized at 130  $^{\circ}\text{C}$  and 150  $^{\circ}\text{C}$  consist the peak at 1704  $\text{cm}^{-1}$  which indicates that there are some free BDC acid left in the structure and complete deprotonation of  $\text{H}_2\text{BDC}$  cannot be achieved. Different from MIL-88B-150-1 and MIL-88B-150-3, MIL-88B-150-5 has peaks at 1647  $\text{cm}^{-1}$  which is associated with C=O asymmetric stretching mode of DMF. Having no peak at 1647  $\text{cm}^{-1}$  confirms the successful removal of DMF molecules from the pores of MIL-88B-150-1 and MIL-88B-150-3. Peaks in between the wavelength range of 1300 and 1650  $\text{cm}^{-1}$  are the characteristic peaks of crystalline state carboxylic acids and proves that the skeletal of hierarchically porous MIL-88Bs are formed successfully. Peaks at 1385 and 1589  $\text{cm}^{-1}$  prove terephthalic acid is attached to metal center. Additionally, the peak at 1107  $\text{cm}^{-1}$  is assigned to C-O-Fe stretching mode and confirms the attachment of terephthalic acid to iron. Lastly, the peaks at 742 and 823  $\text{cm}^{-1}$  prove Fe is successfully coordinated with BDC. Lastly, by comparing the FTIR spectrum of hierarchically porous MIL-88Bs with FTIR spectra of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$  we have shown that there are no metallic iron present. None of the peaks (842  $\text{cm}^{-1}$ , 1594  $\text{cm}^{-1}$ , 2993  $\text{cm}^{-1}$ , 3212  $\text{cm}^{-1}$ , and 3523  $\text{cm}^{-1}$ ) characteristic of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$  were observed in the FTIR spectrum of hierarchically porous MIL-88Bs.

#### 4.3.5. TGA Analysis

Figure 64 shows the TGA curves of hierarchically porous MIL-88Bs. TGA analysis reveals that thermally stable hierarchically porous MIL-88Bs are formed. Percentage of residual mass left at the end of TGA and decomposition temperatures are illustrated at Table 17 and 18, respectively.

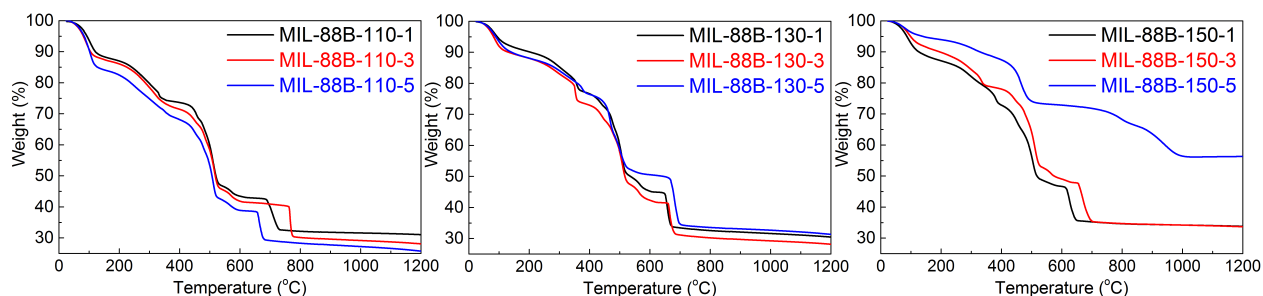


Figure 64. TGA curves of hierarchically porous MIL-88Bs.

Several mass losses occur as temperature increases from 25 °C to 1200 °C. The first mass loss is attributed to adsorbed and coordinated water and DMF molecules. The second mass loss is attributed to trapped solvent molecules inside the pores. Third mass loss is due to decomposition of terephthalic acid which results in structure collapse. And, lastly the fourth step is attributed to CO<sub>2</sub> release as a consequence of carboxylate decomposition. Hierarchically porous MIL-88Bs synthesized with an Fe:BDC ratio of 1 and 5 decompose nearly at the same temperature while MIL-88B-110-3 achieves the highest thermal stability. Fraction of mass left at the end of TGA is almost similar in hierarchically porous MIL-88Bs synthesized with an Fe:BDC ratio of 1 and 3 whereas residual mass increases drastically in MIL-88B-150-5.

Table 17. Percentage of residual mass, %

| Hierarchically porous MIL-88Bs <sup>[a]</sup> | 110 °C | 130 °C | 150 °C |
|-----------------------------------------------|--------|--------|--------|
| M/L 1                                         | 31.0   | 30.5   | 33.8   |
| M/L 3                                         | 28.1   | 28.1   | 33.6   |
| M/L 5                                         | 25.7   | 31.3   | 56.3   |

[a] Synthesis temperature, metal to linker ratio (M/L)

Table 18. Decomposition temperature, °C

| Hierarchically<br>porous MIL-88Bs <sup>[a]</sup> | 110 °C | 130 °C | 150 °C |
|--------------------------------------------------|--------|--------|--------|
| M/L 1                                            | 380    | 392    | 404    |
| M/L 3                                            | 448    | 384    | 442.4  |
| M/L 5                                            | 387    | 405    | -      |

[a] Synthesis temperature, metal to linker ratio (M/L)

Moreover, TGA analysis show that hierarchically porous MIL-88Bs synthesized in this study are thermally stable under adsorption process conditions.

#### 4.3.6. CO<sub>2</sub> Adsorption Studies

Differently synthesized hierarchically porous MIL-88Bs show differences in their CO<sub>2</sub> uptake capacities. Isotherms illustrate the rapidly increased CO<sub>2</sub> uptake capacities in between 0 and 3 bars. For pressures greater than 3 bar, CO<sub>2</sub> adsorption rate decreases, which can be attributed to the relatively low pore volume of the synthesized hierarchically porous MIL-88Bs. Calculated Langmuir and Freundlich isotherm parameters, respective equations of the fitted experimental data, coefficient of determination value (R<sup>2</sup>) and respective comparison of experimental data and nonlinear fitting of the Langmuir and Freundlich models can be found below.

##### Langmuir Model:

$$\frac{C_e}{q_e} = \frac{1}{KQ^0} + \frac{C_e}{Q^0} \quad (4.1)$$

##### Freundlich Model:

$$\log q_e = \log K_F + \frac{1}{n} \log C_e \quad (4.2)$$

Table 19. Respective equations obtained from models

| Hierarchically<br>porous MIL-88Bs | Langmuir Model                           | Freundlich Model                         |
|-----------------------------------|------------------------------------------|------------------------------------------|
| MIL-88B-110-1                     | $y = 0.2396x + 586.96$<br>$R^2 = 0.9986$ | $y = 0.5429x - 1.5641$<br>$R^2 = 0.9588$ |
| MIL-88B-110-3                     | $y = 0.2714x + 627.75$<br>$R^2 = 0.9989$ | $y = 0.5883x - 1.749$<br>$R^2 = 0.9642$  |
| MIL-88B-110-5                     | $y = 0.2758x + 740.17$<br>$R^2 = 0.998$  | $y = 0.559x - 1.6988$<br>$R^2 = 0.9657$  |
| MIL-88B-130-1                     | $y = 0.4109x + 820.32$<br>$R^2 = 0.9972$ | $y = 0.5708x - 1.8328$<br>$R^2 = 0.9638$ |
| MIL-88B-130-3                     | $y = 0.4216x + 733.36$<br>$R^2 = 0.9979$ | $y = 1.3041x - 4.3203$<br>$R^2 = 0.8474$ |
| MIL-88B-130-5                     | $y = 0.5134x + 1110.4$<br>$R^2 = 0.996$  | $y = 0.5372x - 1.8407$<br>$R^2 = 0.9989$ |
| MIL-88B-150-1                     | $y = 0.3062x + 705.14$<br>$R^2 = 0.9986$ | $y = 0.5332x - 1.6231$<br>$R^2 = 0.9578$ |
| MIL-88B-150-3                     | $y = 0.3774x + 935.51$<br>$R^2 = 0.997$  | $y = 0.9251x - 3.0943$<br>$R^2 = 0.9206$ |
| MIL-88B-150-5                     | $y = 0.3776x + 1095.3$<br>$R^2 = 0.9977$ | $y = 0.5639x - 1.871$<br>$R^2 = 0.9663$  |

Table 20. Langmuir and Freundlich isotherm parameters

| MOF           | Langmuir                     | Freundlich              |
|---------------|------------------------------|-------------------------|
| MIL-88B-110-1 | $Q_m = 4.17 \text{ mmol/g}$  | $K_F = 0.0273$          |
|               | $K_a = 4.082\text{E-}04$     | $\eta_F = 1.842$        |
|               | $R^2 = 0.9986$               | $R^2 = 0.9588$          |
| MIL-88B-110-3 | $Q_m = 3.68 \text{ mmol/g}$  | $K_F = 0.0178$          |
|               | $K_a = 4.3\text{E-}04$       | $\eta_F = 1.699$        |
|               | $R^2 = 0.9989$               | $R^2 = 0.9642$          |
| MIL-88B-110-5 | $Q_m = 3.63 \text{ mmol/g}$  | $K_F = 0.020$           |
|               | $K_a = 3.7\text{E-}04$       | $\eta_F = 1.789$        |
|               | $R^2 = 0.998$                | $R^2 = 0.9657$          |
| MIL-88B-130-1 | $Q_m = 2.43 \text{ mmol/g}$  | $K_F = 0.0147$          |
|               | $K_a = 5.01\text{E-}04$      | $\eta_F = 1.752$        |
|               | $R^2 = 0.9972$               | $R^2 = 0.9638$          |
| MIL-88B-130-3 | $Q_m = 2.37 \text{ mmol/g}$  | $K_F = 4.78\text{E-}05$ |
|               | $K_a = 5.7\text{E-}04$       | $\eta_F = 0.766$        |
|               | $R^2 = 0.9979$               | $R^2 = 0.8474$          |
| MIL-88B-130-5 | $Q_m = 1.95 \text{ mmol/g}$  | $K_F = 0.0144$          |
|               | $K_a = 4.6\text{E-}04$       | $\eta_F = 1.862$        |
|               | $R^2 = 0.996$                | $R^2 = 0.9731$          |
| MIL-88B-150-1 | $Q_m = 3.27 \text{ mmol/g}$  | $K_F = 0.0238$          |
|               | $K_a = 4.34\text{E-}04$      | $\eta_F = 1.875$        |
|               | $R^2 = 0.9986$               | $R^2 = 0.9578$          |
| MIL-88B-150-3 | $Q_m = 2.649 \text{ mmol/g}$ | $K_F = 8.05\text{E-}04$ |
|               | $K_a = 4.03\text{E-}04$      | $\eta_F = 1.081$        |
|               | $R^2 = 0.997$                | $R^2 = 0.9206$          |
| MIL-88B-150-5 | $Q_m = 2.648 \text{ mmol/g}$ | $K_F = 0.0135$          |
|               | $K_a = 3.44\text{E-}04$      | $\eta_F = 1.77$         |
|               | $R^2 = 0.9977$               | $R^2 = 0.9663$          |

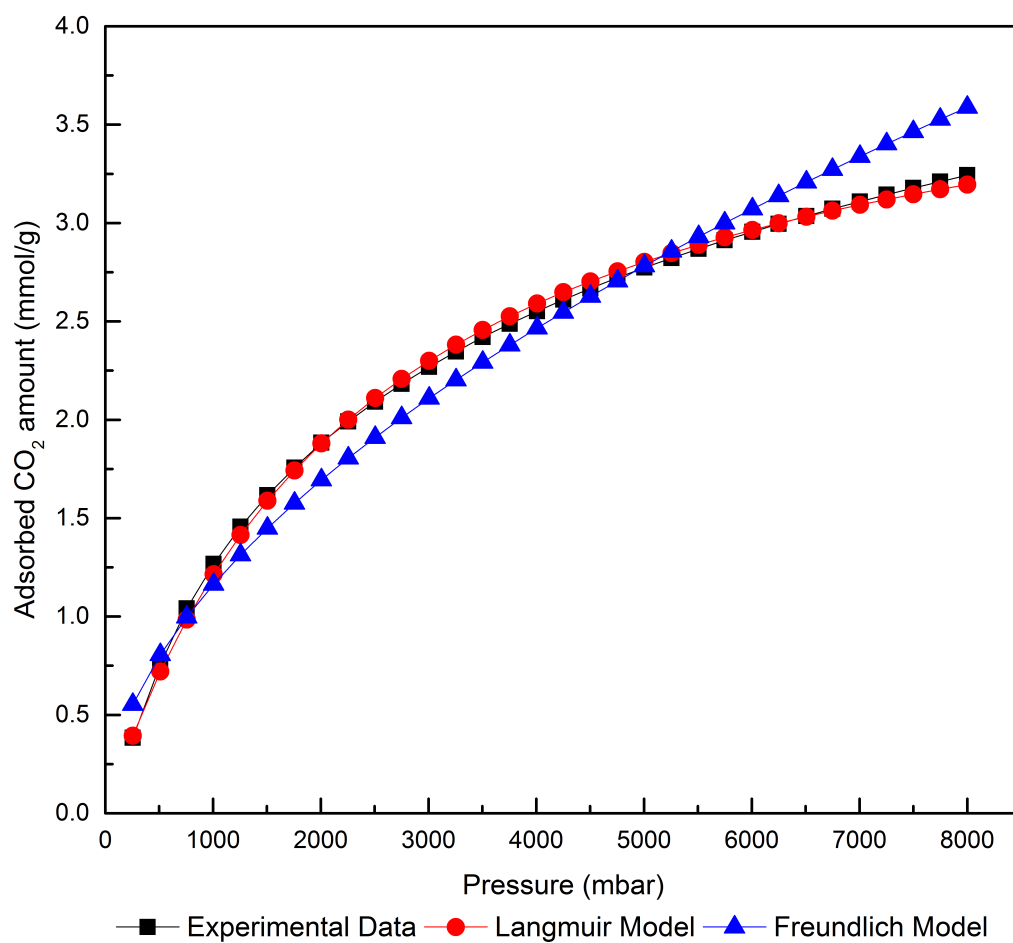


Figure 65. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich model of MIL-88B-110-1.

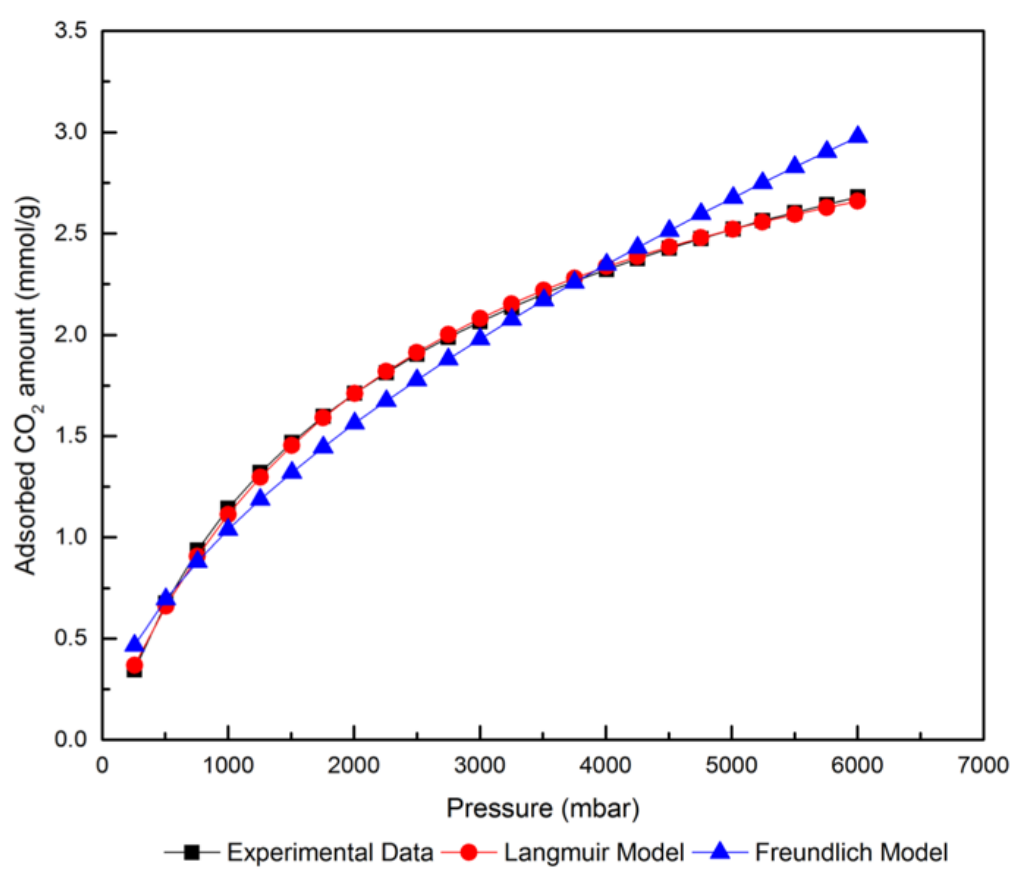


Figure 66. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich model of MIL-88B-110-3.

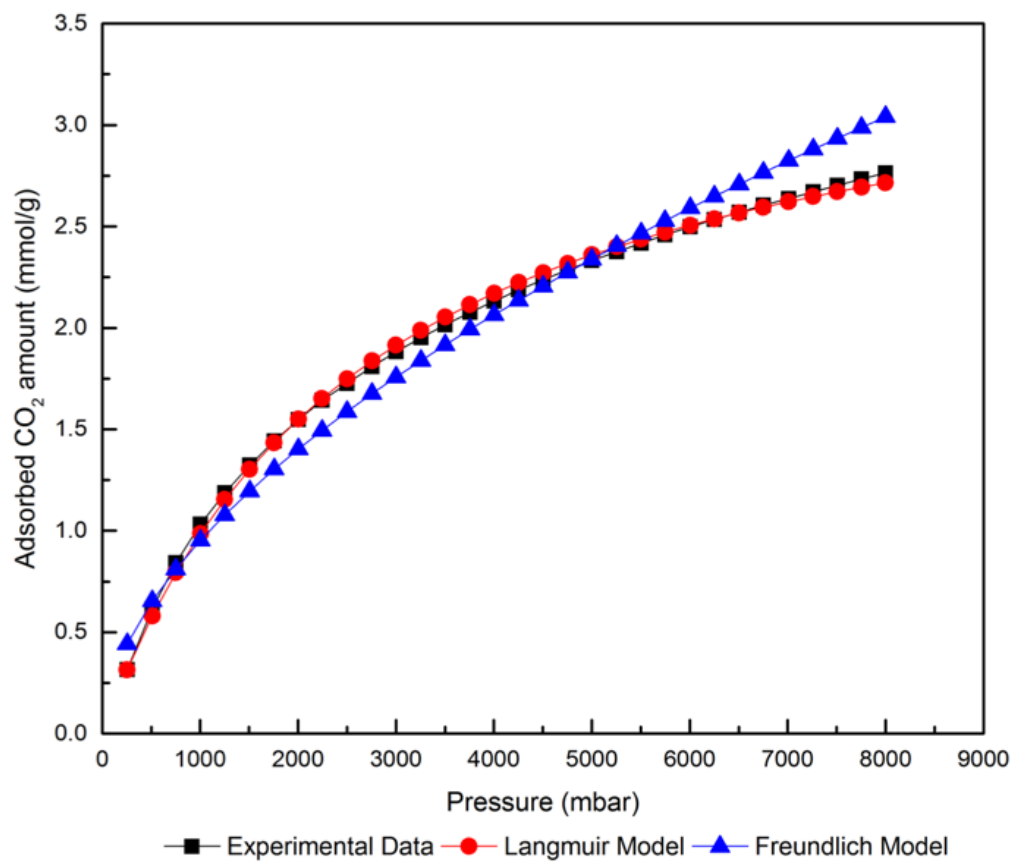


Figure 67. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich model of MIL-88B-110-5.



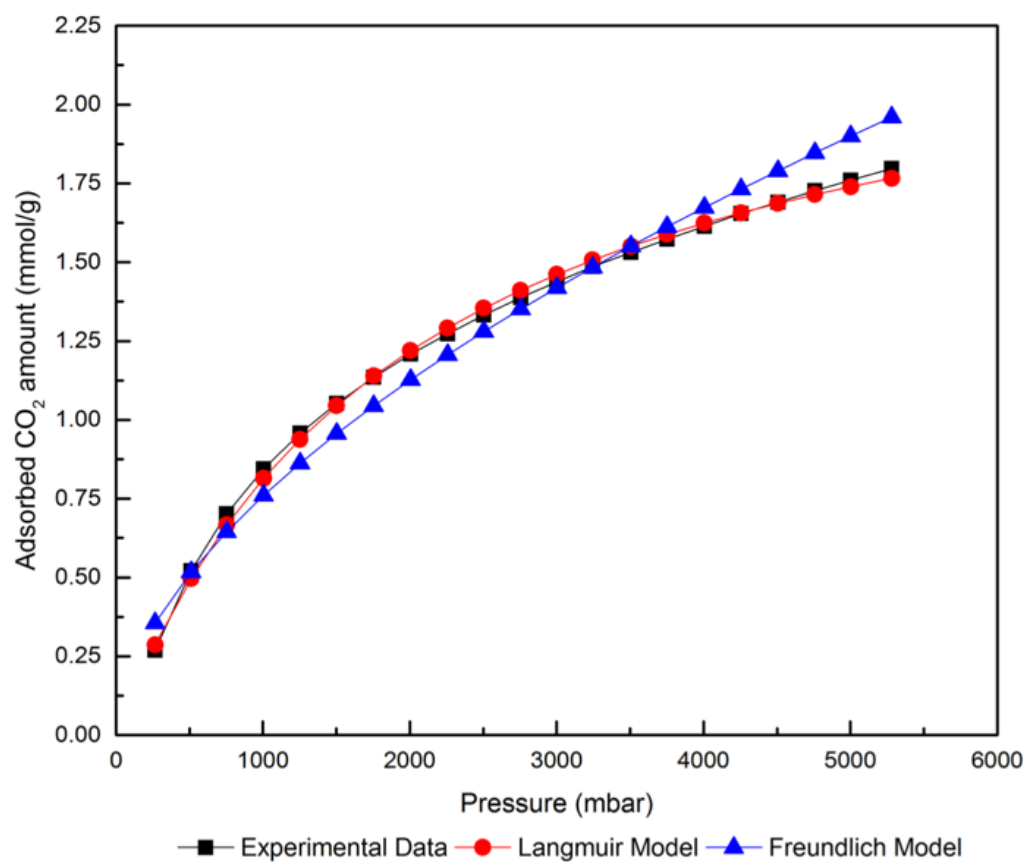


Figure 68. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich model of MIL-88B-130-1.

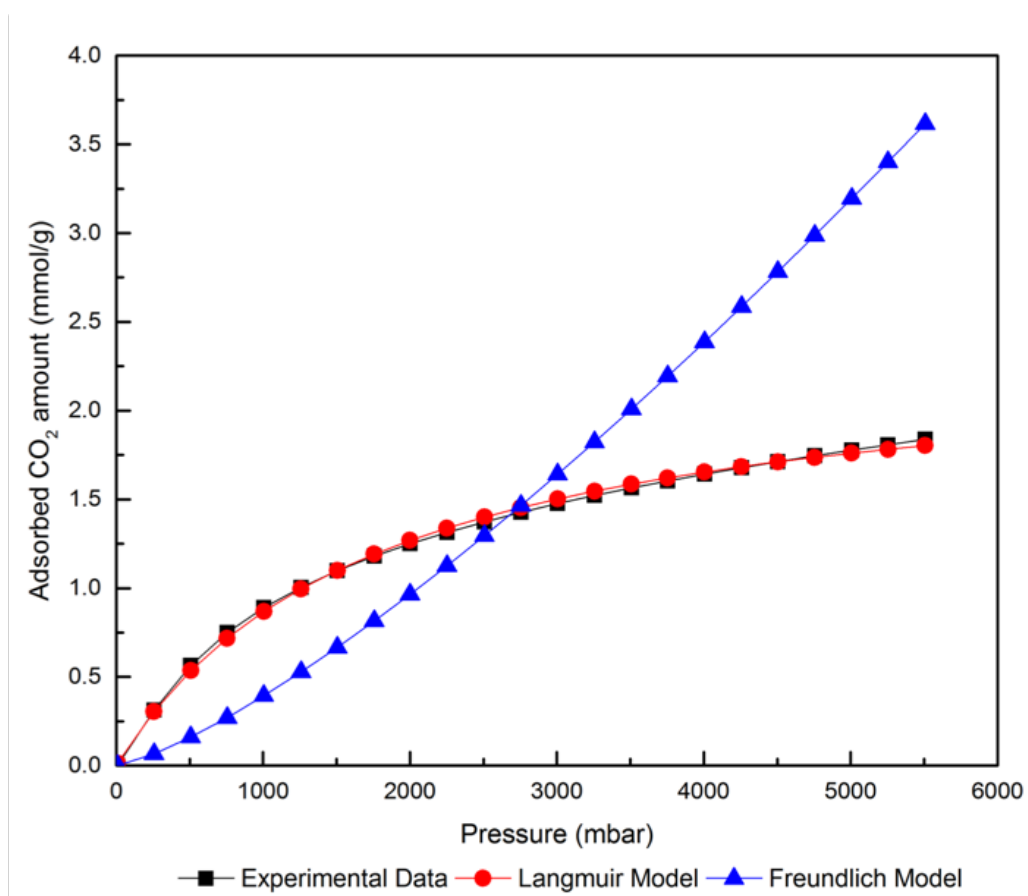


Figure 69. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich model of MIL-88B-130-3.

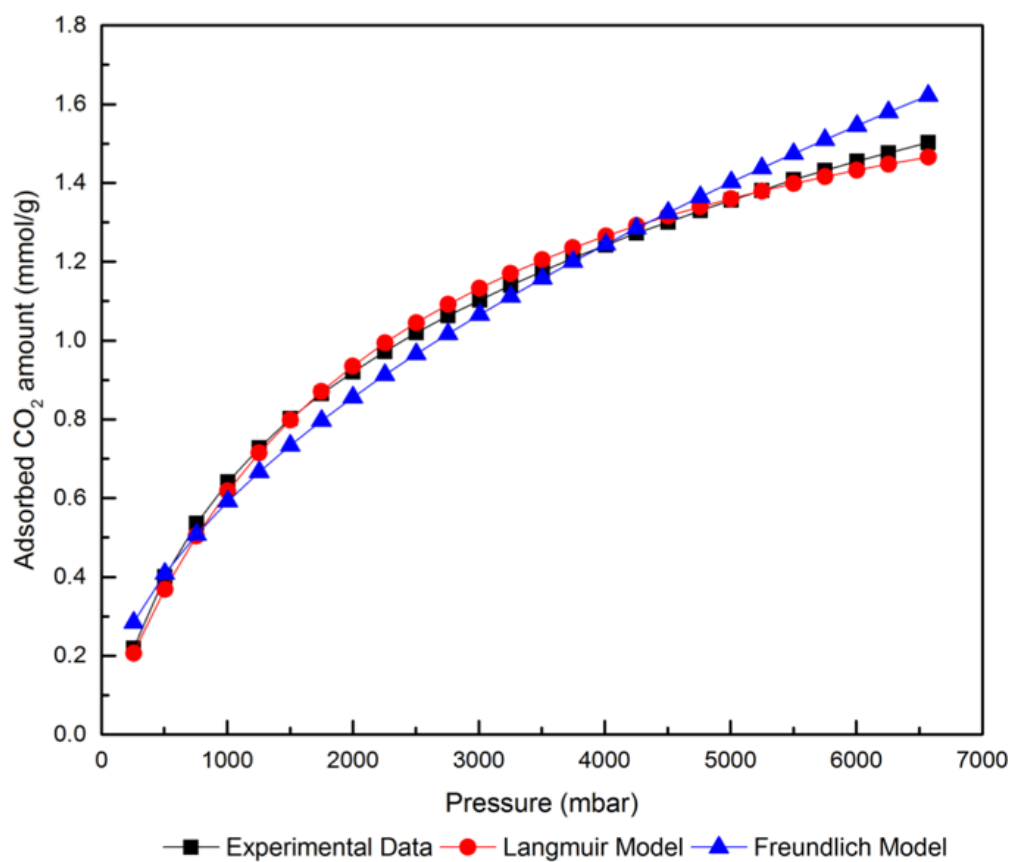


Figure 70. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich model of MIL-88B-130-5.

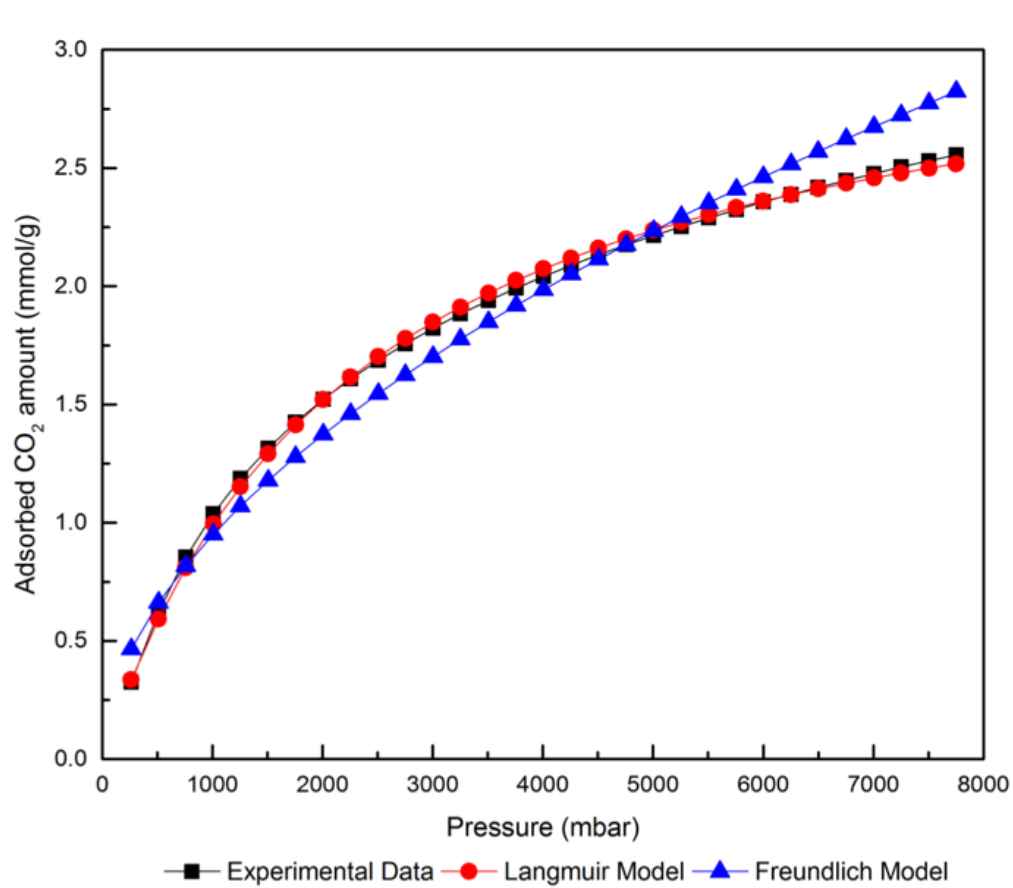


Figure 71. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich model of MIL-88B-150-1.

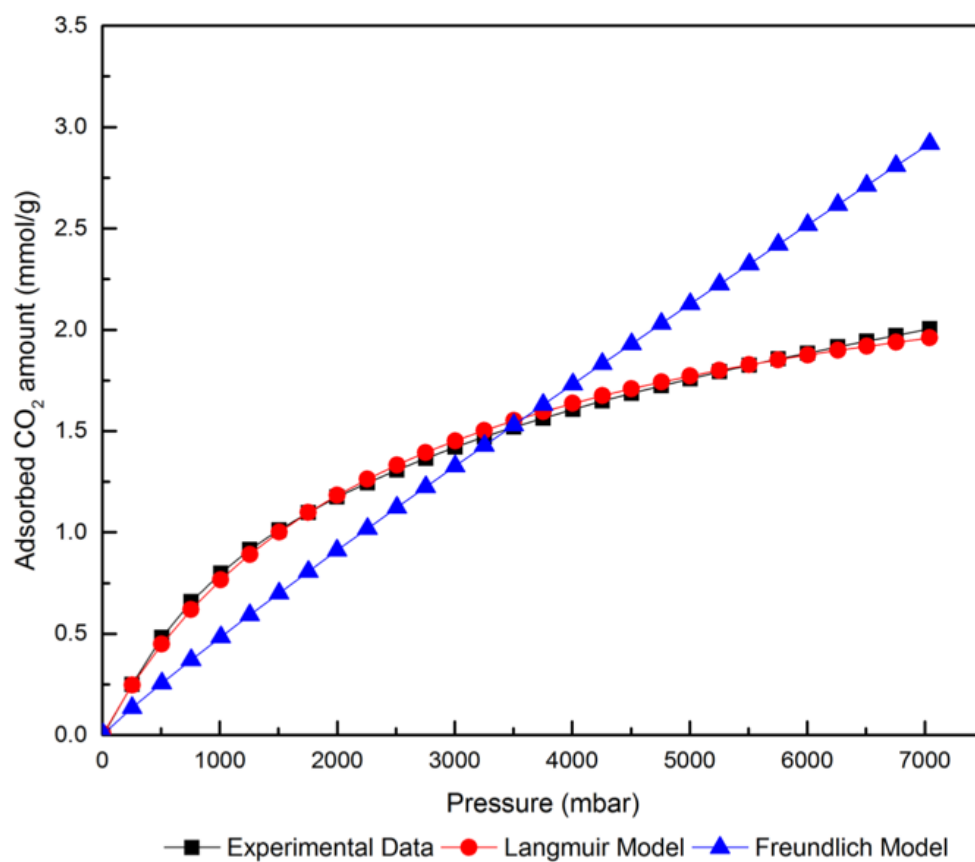


Figure 72. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich model of MIL-88B-150-3.

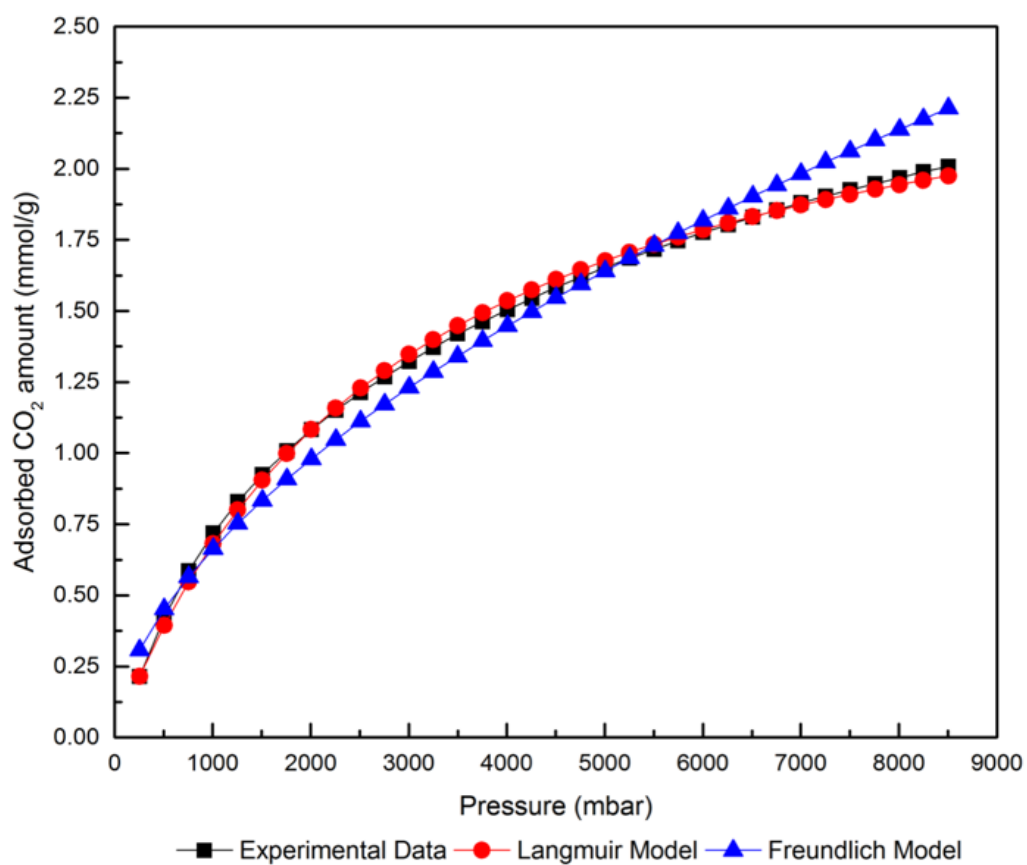


Figure 73. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich model of MIL-88B-150-5.

Table 21. Respective model and monolayer capacity of the hierarchically porous MIL-88Bs

| Hierarchically porous MIL-88Bs | Model    | Monolayer Capacity (mol/kg) |
|--------------------------------|----------|-----------------------------|
| MIL-88B-110-1                  | Langmuir | 4.17                        |
| MIL-88B-110-3                  | Langmuir | 3.68                        |
| MIL-88B-110-5                  | Langmuir | 3.63                        |
| MIL-88B-130-1                  | Langmuir | 2.43                        |
| MIL-88B-130-3                  | Langmuir | 2.37                        |
| MIL-88B-130-5                  | Langmuir | 1.95                        |
| MIL-88B-150-1                  | Langmuir | 3.27                        |
| MIL-88B-150-3                  | Langmuir | 2.65                        |
| MIL-88B-150-5                  | Langmuir | 2.64                        |

The best fit is obtained with the Langmuir model with a relatively high coefficient of determination value. Hierarchically porous MIL-88Bs follow the Langmuir adsorption model, at which adsorption of CO<sub>2</sub> molecules on the surface is homogeneous and monolayer coverage is obtained (Lowell et al., 2004a). Estimated monolayer capacities of hierarchically porous MIL-88Bs and the adsorption model of the synthesized hierarchically porous MIL-88Bs are presented. Hierarchically porous MIL-88Bs show different monolayer capacities. It is certain that Fe:BDC ratio and synthesis temperature have significant effect on the textural porosity of hierarchically porous MIL-88Bs, which in turn affect the CO<sub>2</sub> adsorption capacities. Table 22 presents measured CO<sub>2</sub> uptake capacities at 298 K and 1, 3, and 5 bar, respectively. The CO<sub>2</sub> adsorption isotherms of hierarchically porous MIL-88Bs can be found in Figure 74.

Table 22. CO<sub>2</sub> uptake capacities of hierarchically porous MIL-88Bs at 1, 3 and 5 bar and 25 °C

| MOF           | CO <sub>2</sub> uptake capacity at 1 bar (mol/kg) | CO <sub>2</sub> uptake capacity at 3 bar (mol/kg) | CO <sub>2</sub> uptake capacity at 5 bar (mol/kg) | BET Surface Area (m <sup>2</sup> /g) | Micropore Volume |
|---------------|---------------------------------------------------|---------------------------------------------------|---------------------------------------------------|--------------------------------------|------------------|
| MIL-88B-110-1 | 1.27                                              | 2.27                                              | 2.77                                              | 400.4±1.1E1                          | 0.182±1.4E-2     |
| MIL-88B-110-3 | 1.14                                              | 2.07                                              | 2.52                                              | 452.4±1.9E1                          | 0.239±3.2E-2     |
| MIL-88B-110-5 | 1.03                                              | 1.88                                              | 2.33                                              | 445.9±1.9E1                          | 0.202±3.2E-2     |
| MIL-88B-130-1 | 0.84                                              | 1.44                                              | 1.76                                              | 265.4±2.6E1                          | 0.113±6.5E-3     |
| MIL-88B-130-3 | 0.89                                              | 1.48                                              | 1.78                                              | 249.4±1.6E1                          | 0.115±1.6E-2     |
| MIL-88B-130-5 | 0.64                                              | 1.10                                              | 1.36                                              | 283.1±2.6E1                          | 0.108±2.8E-3     |
| MIL-88B-150-1 | 1.04                                              | 1.82                                              | 2.21                                              | 357.1±7.8E1                          | 0.143±4.6E-2     |
| MIL-88B-150-3 | 0.80                                              | 1.42                                              | 1.76                                              | 346.3±1.7E1                          | 0.140±2.2E-2     |
| MIL-88B-150-5 | 0.72                                              | 1.32                                              | 1.65                                              | 117.7±1.9                            | 0.0350±9.0E-3    |



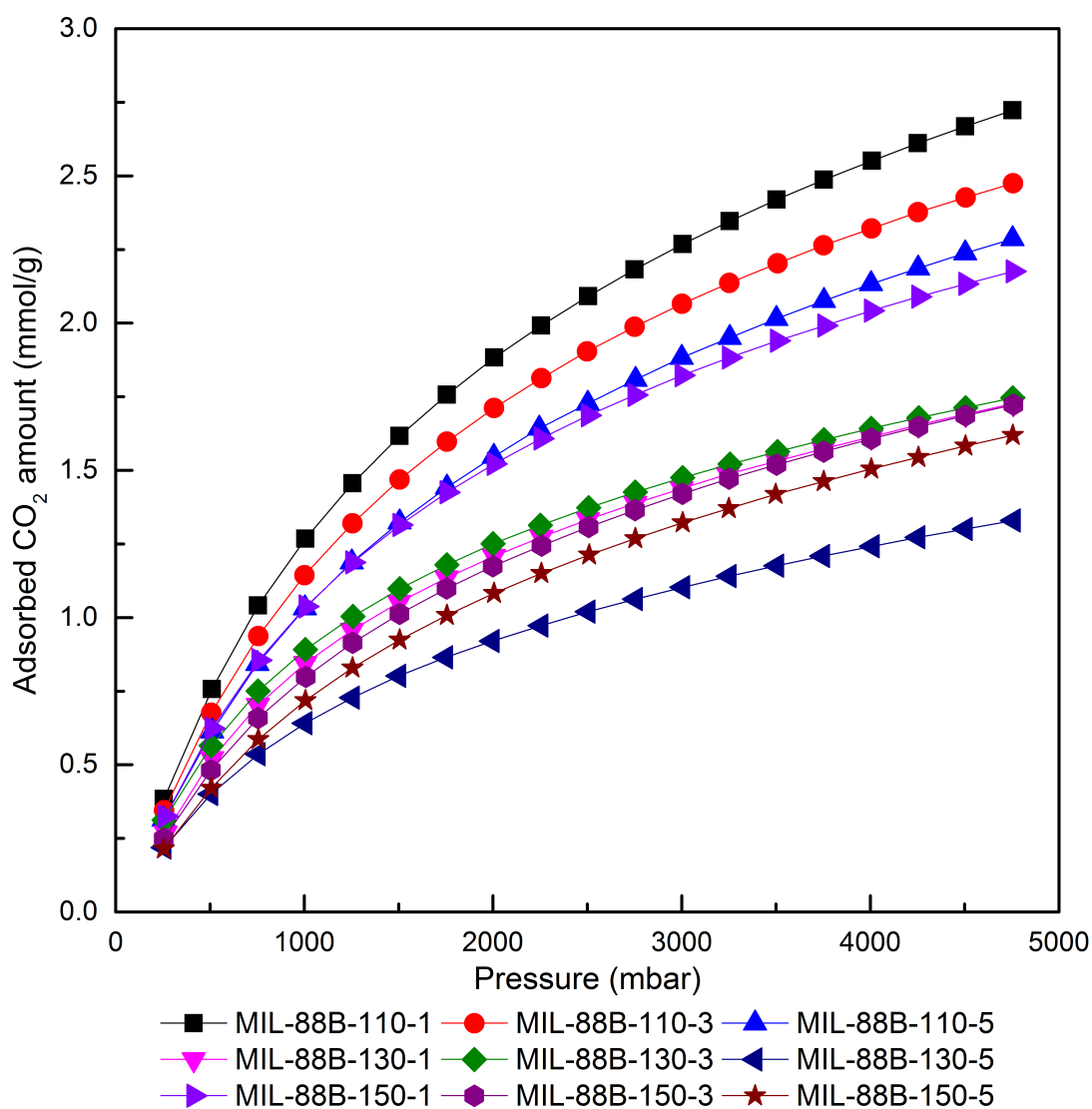


Figure 74. CO<sub>2</sub> adsorption isotherm of hierarchically porous MIL-88Bs measured at 298 K.

At 1, 3, and 5 bar and 298 K, the highest CO<sub>2</sub> uptake capacity is achieved by MIL-88B-110-1 while the lowest CO<sub>2</sub> uptake capacity belongs to MIL-88B-130-5. Even though MIL-88B-110-3 possesses the highest micropore volume (0.239 cm<sup>3</sup>/g) and BET surface area (452.4 m<sup>2</sup>/g), its CO<sub>2</sub> adsorption capacity (2.52 mol/kg) is lower than the CO<sub>2</sub> uptake capacity of MIL-88B-110-1 (2.77 mol/kg) measured at 5 bar and 298 K.

In addition, the lowest micropore volume (0.0355 cm<sup>3</sup>/g) and the lowest BET surface area (117.7 m<sup>2</sup>/g) belongs to MIL-88B-150-5. However, MIL-88B-150-5 possesses a CO<sub>2</sub> adsorption capacity higher (1.65 mol/kg, measured at 5 bar and 298 K) than MIL-88B-130-

5 (1.36 mol/kg, measured at 5 bar and 298 K) which reveals that there is no direct relation between the micropore volume and the CO<sub>2</sub> uptake capacity exists.

To investigate the relation between the CO<sub>2</sub> adsorption capacity with BET surface area, narrow micro-, micro-, meso- and total pore volume, adsorbed CO<sub>2</sub> amount is plotted with respect to BET surface area, narrow micro-, micro-, meso- and total pore volume which can be found below in Figure 75-79. Mesopore volume ( $R^2$ : 0.32), total pore volume ( $R^2$ : 0.1975) and BET surface area ( $R^2$ : 0.5171) are found out to be weakly correlated with the CO<sub>2</sub> adsorption capacity which illustrates that there is no direct relation between these parameters and the CO<sub>2</sub> uptake capacity of hierarchically porous MIL-88Bs.

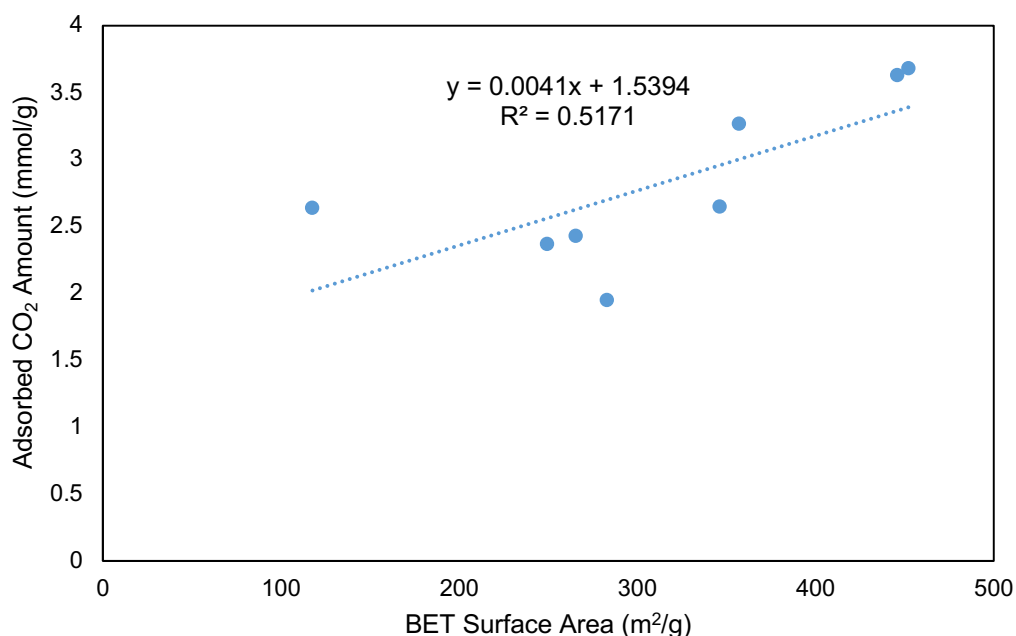


Figure 75. Dependence of CO<sub>2</sub> adsorption capacity on BET surface area.

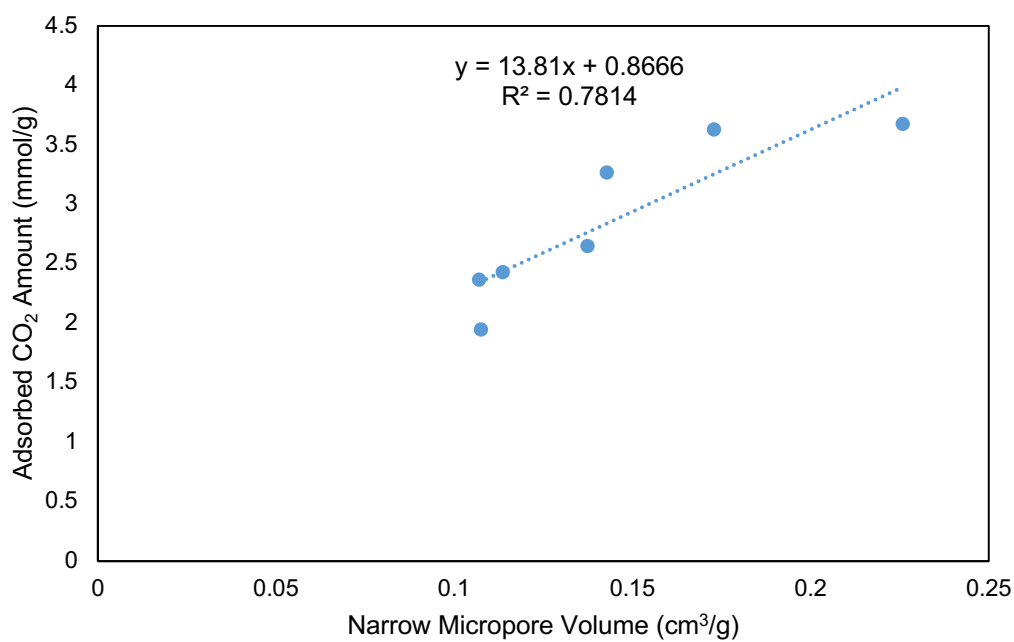


Figure 76. Dependence of CO<sub>2</sub> adsorption capacity on volume of narrow micropores.

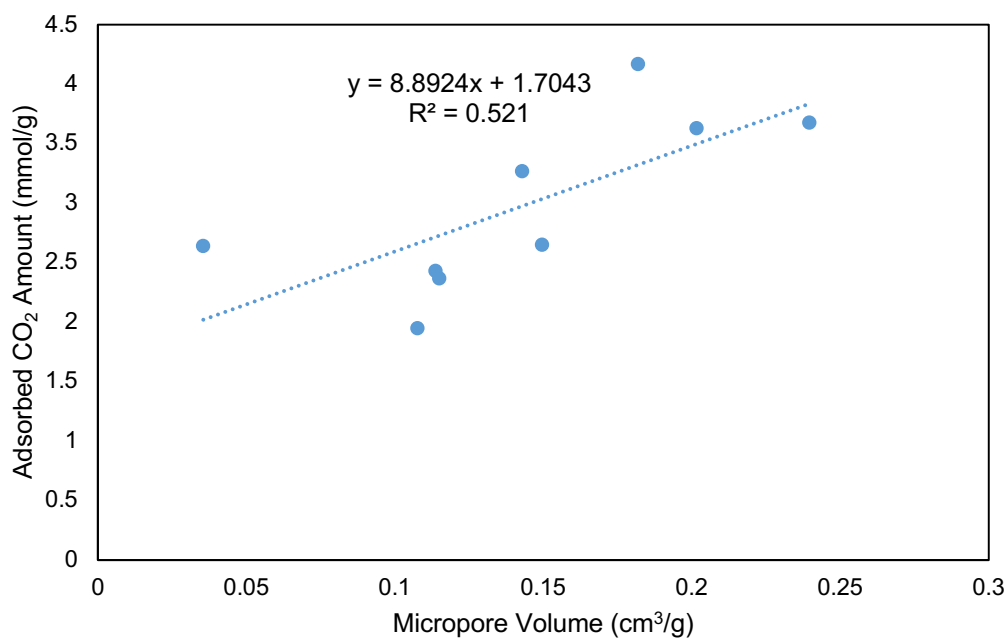


Figure 77. Dependence of CO<sub>2</sub> adsorption capacity on micropore volume.

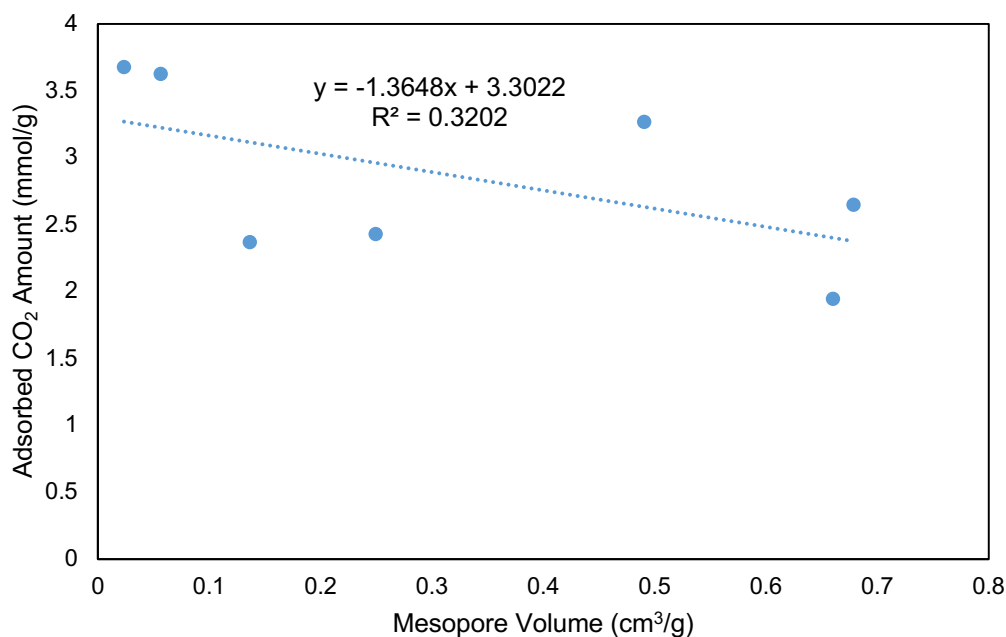


Figure 78. Dependence of CO<sub>2</sub> adsorption capacity on mesopore volume.

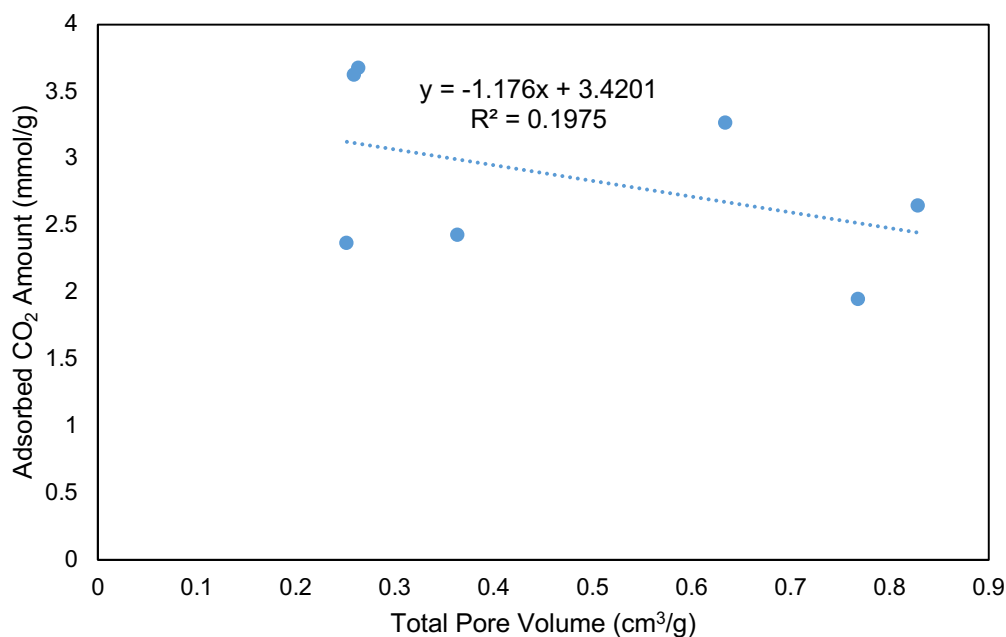


Figure 79. Dependence of CO<sub>2</sub> adsorption capacity on total pore volume.

Among the various parameters examined, the strongest correlation is in between the CO<sub>2</sub> adsorption capacity and the volume of narrow micropores ( $R^2$ : 0.78). However, a  $R^2$  value very close to 1 cannot be achieved which reveals that there may be some other

parameters affecting the CO<sub>2</sub> uptake capacity in addition to the volume of pores narrower than 1 nm.

The highest fraction of microporosity is achieved when hierarchically porous MIL-88Bs were synthesized at 110 °C. However, when synthesis was conducted at temperatures higher than 110 °C, textural mesopores widen and the fraction of textural mesoporosity increases. In accordance with the increased pore diameter, CO<sub>2</sub> uptake capacity is expected to decrease. However, MIL-88B-150-1 shows a greater CO<sub>2</sub> uptake capacity (2.21 mol/kg, measured at 5 bar and 298 K) than MIL-88B-130-1 (1.76 mol/kg, measured at 5 bar and 298 K).

Even though the highest micropore volume is achieved by MIL-88B-110-3 (0.239 cm<sup>3</sup>/g), its sorption capacity (2.52 mol/kg, measured at 5 bar and 298 K) is lower than the sorption capacity of MIL-88B-110-1 (2.77 mol/kg, measured at 5 bar and 298 K) which makes us focus on the micropore size distribution of MIL-88B type MOF crystallites. Table 23 illustrates volume of pores narrower than 1 and 2 nm, ratio of pore volumes of pores narrower than 1 nm to 2 nm, and CO<sub>2</sub> uptake capacity of MIL-88B type MOF crystallites at 5 bar.

Table 23. Pore volumes, pore volume ratios, and CO<sub>2</sub> uptake capacity of hierarchically porous MIL-88Bs

| Hierarchically porous MIL-88Bs | Vpores < 1 nm (cm <sup>3</sup> /g) | Vpores < 2 nm (cm <sup>3</sup> /g) | Ratio of Vpores < 1 nm to Vpores < 2 nm <sup>[a]</sup> | CO <sub>2</sub> uptake capacity at 5 bar (mol/kg) |
|--------------------------------|------------------------------------|------------------------------------|--------------------------------------------------------|---------------------------------------------------|
| MIL-88B-110-1                  | 0.177±1.7E-2                       | 0.182±1.4E-2                       | 0.97                                                   | 2.77                                              |
| MIL-88B-110-3                  | 0.226±1.2E-2                       | 0.239±3.2E-2                       | 0.94                                                   | 2.52                                              |
| MIL-88B-110-5                  | 0.172±1.7E-2                       | 0.202±3.2E-2                       | 0.85                                                   | 2.33                                              |
| MIL-88B-130-1                  | 0.113±1.6E-2                       | 0.1137±6.5E-3                      |                                                        | 1.76                                              |
| MIL-88B-130-3                  | 0.107±2.6E-2                       | 0.115±1.6E-2                       | 0.93                                                   | 1.78                                              |
| MIL-88B-130-5                  | 0.108±1.1E-2                       | 0.108±2.8E-3                       |                                                        | 1.36                                              |
| MIL-88B-150-1                  | 0.142±3.7E-2                       | 0.143±4.6E-2                       |                                                        | 2.21                                              |
| MIL-88B-150-3                  | 0.137±3.2E-2                       | 0.149±2.2E-2                       | 0.916                                                  | 1.76                                              |
| MIL-88B-150-5                  | 0.023±1.8E-2                       | 0.0355±9.0E-3                      | 0.65                                                   | 1.65                                              |

*[a] Volume ratio of pores smaller than 1 nm to 2 nm*

The highest pore volume of 0.82 cm<sup>3</sup>/g belongs to MIL-88B-150-3 while its CO<sub>2</sub> uptake capacity (1.76 mol/kg) is lower than MIL-88B-110-1 (2.77 mol/kg, measured at 5 bar and 298 K) which has considerably lower pore volume (0.20 cm<sup>3</sup>/g). A similar trend is observed for MIL-88B-110-3 (2.52 mol/kg, measured at 5 bar and 298 K). Despite its high micropore volume (0.239 cm<sup>3</sup>/g) and total pore volume (0.249 cm<sup>3</sup>/g), the CO<sub>2</sub> uptake capacity of MIL-88B-110-3 (2.52 mol/kg, measured at 5 bar and 298 K) is lower than the CO<sub>2</sub> adsorption capacity of MIL-88B-110-1 (2.77 mol/kg, measured at 5 bar and 298 K). Apparently, hierarchically porous MIL-88Bs that possess higher pore volumes for pores narrower than 1 nm achieve higher CO<sub>2</sub> uptake capacities. This enhanced adsorption capacity is attributed to high CO<sub>2</sub> adsorption potential of narrow micropores (pore diameters < 1 nm) (Fonseca, Gutierrez, & Lueking, 2008; Romanos et al., 2012).

Among the hierarchically porous MIL-88Bs synthesized at different temperatures with different Fe:BDC ratios, hierarchically porous MIL-88Bs synthesized at 110 °C show higher CO<sub>2</sub> adsorption capacities than hierarchically porous MIL-88Bs synthesized at 130

and 150 °C. As mentioned above, synthesizing hierarchically porous MIL-88Bs at 110 °C leads to highly microporous hierarchically porous MIL-88Bs to form. Pores narrower than 1 nm dominate the micropore size distribution whose volumes correspond to 97, 94 and 85% of the micropore volume of MIL-88B-110-1, MIL-88B-110-3, and MIL-88B-110-5, respectively. Surprisingly, MIL-88B-110-1 achieves a CO<sub>2</sub> adsorption capacity (2.77 mol/kg, measured at 5 bar and 298 K) higher than MIL-88B-110-3 (2.52 mol/kg, measured at 5 bar and 298 K) whose volume of narrow micropores (0.177 cm<sup>3</sup>/g) is lower than the volume of narrow micropores of MIL-88B-110-3 (0.226 cm<sup>3</sup>/g). This high CO<sub>2</sub> adsorption capacity of MIL-88B-110-1 is attributed to its high fraction of narrow micropores (97%) present in its micropore size distribution. Pore volumes narrower than 1 nm and 2 nm are illustrated at Figure 80.

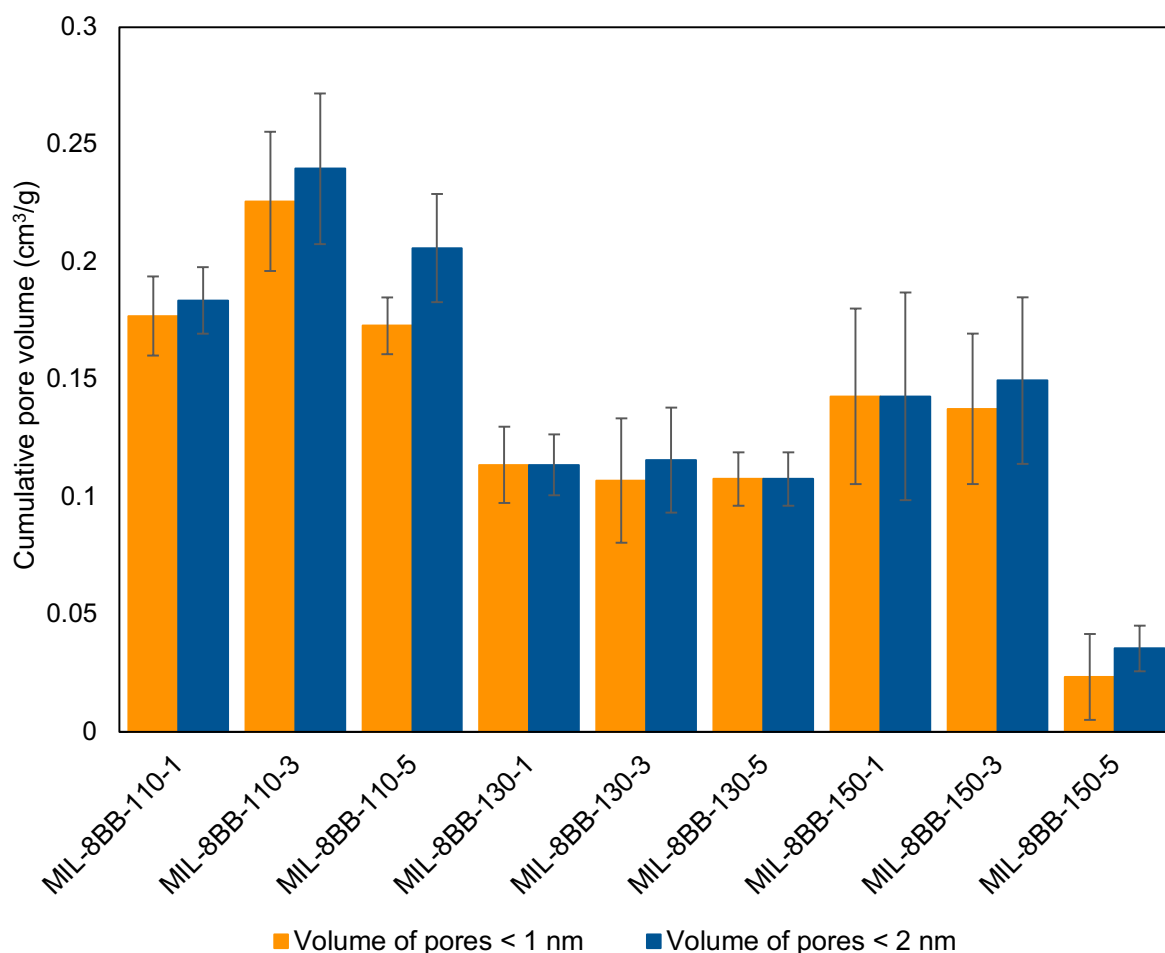


Figure 80. Volume of pores narrower than 1 and 2 nm reported with standard deviations.

Order of CO<sub>2</sub> uptake capacity from the highest to the lowest is in the order of the highest to the lowest volume of pores narrower than 1 nm. CO<sub>2</sub> adsorption capacity increases as the volume of narrow micropores increase. The volume of narrow micropores present in hierarchically porous MIL-88Bs synthesized at 110 °C is higher than the volumes of narrow micropores present in hierarchically porous MIL-88Bs synthesized at 130 and 150 °C. Meanwhile, the CO<sub>2</sub> uptake capacities of hierarchically porous MIL-88Bs synthesized at 150 °C are lower than the CO<sub>2</sub> uptake capacities of hierarchically porous MIL-88Bs synthesized at 110 °C. It is important to note that, even though, MIL-88B-150-3 possesses a greater micropore volume (0.149 cm<sup>3</sup>/g) than MIL-88B-150-1 (0.142 cm<sup>3</sup>/g), narrow micropores present in MIL-88B-150-1 provide these crystallites achieve a higher CO<sub>2</sub> uptake capacity (2.21 mol/kg) than MIL-88B-150-3 (1.76 mol/kg) at 5 bar and 298 K. Volume of the pores narrower than 1 nm is almost equal in MIL-88B-130-3 and MIL-88B-130-5. However, MIL-88B-130-3 possesses a CO<sub>2</sub> adsorption capacity higher (1.78 mol/kg) than MIL-88B-130-5 (1.36 mol/kg) at 5 bar and 298 K. When examined in more detail, it is observed that MIL-88B-130-3 has a cumulative pore volume of 0.104 cm<sup>3</sup>/g for pores narrower than 0.7 nm. Meanwhile, the cumulative pore volume of pores narrower than 1 nm in MIL-88B-130-5 is 0.108 cm<sup>3</sup>/g. Although, MIL-88B-130-3 and MIL-88B-130-5 possess similar pore volumes for pores narrower than 1 nm, the CO<sub>2</sub> uptake capacity of MIL-88B-130-3 is 1.31 times higher than the CO<sub>2</sub> uptake capacity of MIL-88B-130-5. Thereby, we concluded that it is not only the volume of micropores narrower than 1 nm affecting the CO<sub>2</sub> adsorption capacity, but also the volume of pores with pore diameters ranging in between 0.5 and 0.7 nm that heavily influences the CO<sub>2</sub> adsorption capacity.

These results simply indicate that as opposed to BET surface area, mesopore volume and total pore volume, volume of pores narrower than 1 nm and their distribution within the micropore size range affect the CO<sub>2</sub> uptake capacity.

The significance of pores being narrower than 1 nm lies behind their increased binding energies. As pore sizes decrease, their binding energies increase (Fonseca et al., 2008; Romanos et al., 2012). The overlapped adsorption potentials cause ultramicropores to attract CO<sub>2</sub> molecules stronger. In fact, deep well potential is created when the interaction potentials of opposite ultramicropore walls overlap, which attracts CO<sub>2</sub> molecules more strongly (Ello et al., 2013). Thus, a narrower micropore size distribution and higher fraction of narrow micropores enables higher CO<sub>2</sub> uptake capacities to be attained.



#### 4.4. Comparison with Literature

Several MOFs with high BET surface areas have been investigated for their CO<sub>2</sub> uptake capacities. In line with our results, in this study BET surface area was not the main factor enhancing CO<sub>2</sub> adsorption capacities. For instance, at 1 bar and 298 K MOF-177 with 5400 m<sup>2</sup>/g of BET surface area possessed 3.6 wt.% CO<sub>2</sub> uptake capacity (Mason et al., 2011a); MOF-5 with 2833 m<sup>2</sup>/g BET surface area possessed 4.5 wt.% CO<sub>2</sub> uptake capacity (Millward & Yaghi, 2005b); IRMOF-3 with 2160 m<sup>2</sup>/g BET surface area had 5.1 wt.% CO<sub>2</sub> uptake capacity (Millward & Yaghi, 2005b); IRMOF-6 with 2516 m<sup>2</sup>/g BET surface area had 5.1 wt.% CO<sub>2</sub> uptake capacity (Millward & Yaghi, 2005b); ZIF-8 with 1135 m<sup>2</sup>/g BET surface area possessed 4.3 wt.% CO<sub>2</sub> uptake capacity (A. O. Yazaydin et al., 2009); MIL-101(Cr) with 2674 m<sup>2</sup>/g BET surface area had 4.2 wt.% CO<sub>2</sub> adsorption capacity (Chowdhury, Bikkina, & Gumma, 2009); and lastly UMCM-1 with 4034 m<sup>2</sup>/g BET surface area had 3.8 wt.% CO<sub>2</sub> adsorption capacity (A. O. Yazaydin et al., 2009). Additionally, to the best of our knowledge the obtained CO<sub>2</sub> adsorption capacity of MIL-88B type MOF crystallites in the present study is greater than those of IRMOF-6 (Millward & Yaghi, 2005b), MIL-101(Cr) (B. Wang et al., 2008), MIL-102 (Phan et al., 2010), MOF-2 (Millward & Yaghi, 2005b), ZIF-8 (Mason et al., 2011a), ZIF-71 (A. O. Yazaydin et al., 2009), ZIF-95 (Frost et al., 2006a), ZIF-97 (Frost et al., 2006a) and ZIF-100 (Trickett et al., 2017). Figure 81 illustrates the CO<sub>2</sub> adsorption capacity (wt. %) of several reported MOFs.

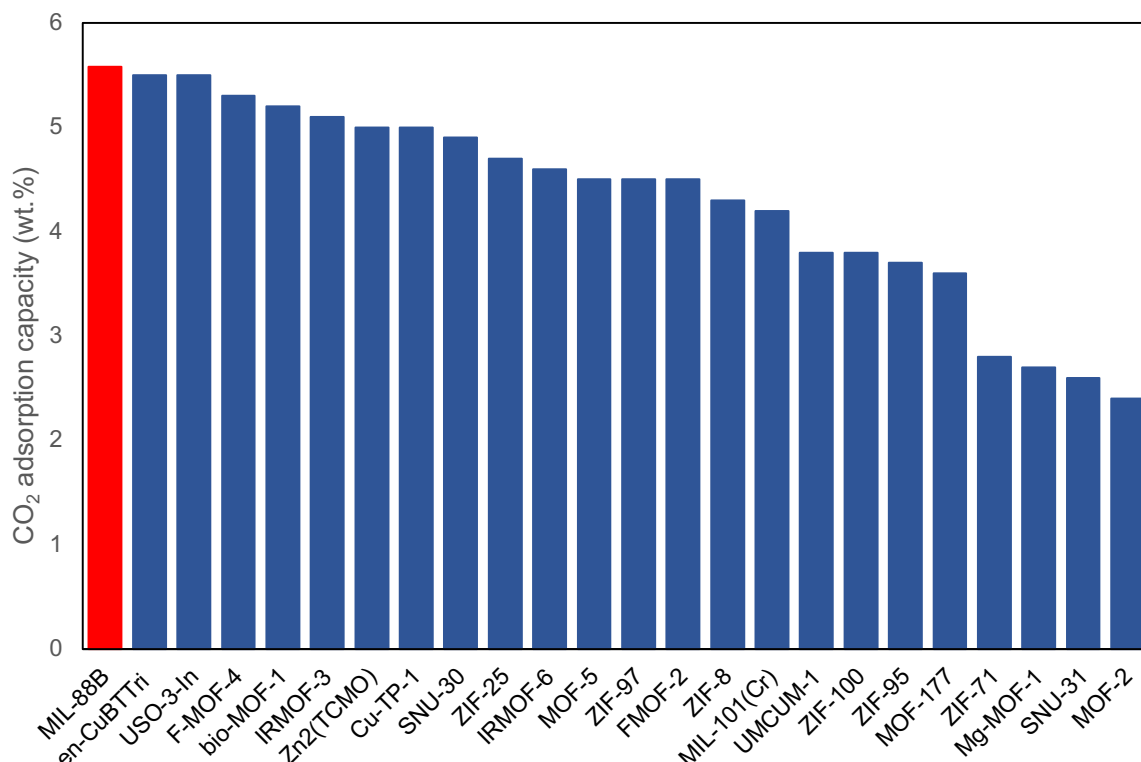


Figure 81. CO<sub>2</sub> uptake capacity of some of the MOFs reported in literature and MIL-88B (shown in red) reported in this report (at 1 bar and 298 K).

In comparison to the mentioned MOFs, hierarchically porous MIL-88Bs synthesized with a relatively short linker (BET surface area: 400.4 m<sup>2</sup>/g) possess a relatively higher CO<sub>2</sub> uptake capacity than the reported ones (the CO<sub>2</sub> uptake capacity of hierarchically porous MIL-88Bs synthesized in the present study is represented by red in Figure 81). By forming hierarchical pores via stirring metal salt, linker and DMF vigorously and tuning the pore size and pore size distribution of textural mesoporosity via synthesis temperature and Fe:BDC ratio, the CO<sub>2</sub> uptake capacity of hierarchically porous MIL-88Bs is increased by a factor of 2.1 (5.58 wt.% at 298 K and 1 bar) which is relatively higher than those of listed MOF structures.

#### 4.5. Concluding Remarks

The CO<sub>2</sub> uptake capacities of hierarchically porous MIL-88Bs were found to be dependent on the fraction and volume of narrow micropores (pore diameter < 1 nm). Textural

pores were strategically controlled by Fe:BDC ratio and synthesis temperature. Volume of narrow micropores (pore diameter  $< 1$  nm) increased by a factor of 1.65, and the highest volume of narrow micropores were achieved (MIL-88B-110-3,  $0.226 \text{ cm}^3/\text{g}$ ). Among the hierarchically porous MIL-88Bs synthesized at different temperatures with different Fe:BDC ratios, the highest  $\text{CO}_2$  adsorption capacity (5.58 wt.% at 298 K and 1 bar) was attained by those with the highest fraction (97%) and volume of narrow micropores ( $0.177 \text{ cm}^3/\text{g}$ ).

As pore sizes become narrower than 1 nm, adsorption potentials overlapped, which in turn results in higher binding energies (Fonseca et al., 2008; Romanos et al., 2012) and thereby, the amount of  $\text{CO}_2$  adsorbed increases to 5.58 wt.% at 298 K and 1 bar. Our results demonstrate that  $\text{CO}_2$  adsorption capacity is heavily dependent on: (i) the volume of micropores narrower than 1 nm; (ii) the cumulative volume of pores narrower than 0.7 nm; and lastly (iii) the distribution of narrow micropores (pore diameters  $< 1$  nm) within the micropore size distribution ( $V_{\text{pores} < 1 \text{ nm}} / V_{\text{pores} < 2 \text{ nm}}$ ).

This study reports a controlled synthesis strategy at which hierarchical pores are controlled by Fe:BDC ratio and synthesis temperature. The  $\text{CO}_2$  adsorption capacity of hierarchically porous MIL-88Bs were enhanced by a factor of 2.1, and a  $\text{CO}_2$  adsorption capacity (5.58 wt.% at 298 K and 1 bar) higher than those of commercially available MOFs is achieved. To move beyond the  $\text{CO}_2$  uptake capacities achieved today, strategies to synthesize porous sorbents that are majorly formed of ultramicropores should be considered. The present study suggests that hierarchically porous MIL-88Bs synthesized in this work can be a promising and novel candidate in gas adsorption studies while our controlled synthesis strategy paves the way for the design of hierarchically porous MOFs with increased fraction and volume of micropores narrower than 1 nm.

## Chapter V

### Hydrogen adsorption capacity of hierarchically porous MIL-88Bs and the role of ultramicropores

#### 5.1. Background

Energy plays a crucial role in society's economic development (Mao & Chen, 2007). Rising energy demand results in excessive fossil fuel consumption, and more importantly, adversely influences the ecosystem and human health (Fakioğlu et al., 2004). Hydrogen comes to the fore as a clean alternative to fossil fuels (Fakioğlu et al., 2004). Therefore, the use of hydrogen in energy and transportation applications is a key to decrease pollutant emissions (U.S. Department of Energy, 2015). In 2011, the U.S. Department of Energy (DOE) set a target to develop safe and cost-effective onboard vehicle hydrogen storage systems that can provide 300 miles of driving (U.S. Department of Energy, 2015). More than 180 fuel cell light-duty vehicles and 20 fuel cell buses using compressed hydrogen have been reported (U.S. Department of Energy, 2015). However, the high energy density demands and DOE target for 2020 (5.5 wt.% H<sub>2</sub>) limited the use of hydrogen in energy and transportation applications (U.S. Department of Energy, 2015).

Physisorption of hydrogen on porous materials is a cost-effective, efficient and safe way of storing hydrogen (K. C. Kim, 2018; Jianwei Ren, Langmi, North, & Mathe, 2014a; Jianwei Ren, Musyoka, Langmi, Mathe, & Liao, 2017; Louis Schlapbach, Schlapbach, & Züttel, 2001; U.S. Department of Energy, 2015). Porous materials show very promising results at 77 K and high pressures (Beckner & Dailly, 2016). However, their H<sub>2</sub> adsorption capacities decrease drastically at 298 K and low pressures (0-100 bar) which limit the practical use of porous materials, economically (Broom et al., 2016; Kaskun & Kayfeci, 2018). The hydrogen adsorption capacity of a porous material changes with the surface area, pore volume, pressure, and temperature at which hydrogen storage studies are carried on (Jianwei Ren et al., 2017). Materials with high surface area and low density (i.e. carbon materials, activated carbons, zeolites, and metal-organic frameworks) tend to adsorb more

H<sub>2</sub> molecules (A. Züttel, 2003). Particularly, carbon materials have been used widely in H<sub>2</sub> sorption studies (Andersson & Grönkvist, 2019; Blankenship, Balahmar, & Mokaya, 2017; Broom et al., 2016; Yürüm et al., 2009a). However, theoretical studies illustrated their limited H<sub>2</sub> sorption capacities (only a few wt.%) (Becher et al., 2003; Barbara Panella et al., 2005a; Rzepka, Lamp, & de la Casa-Lillo, 2002; Yürüm et al., 2009a).

In 1995 a new family of porous materials, metal-organic frameworks (MOFs), formed of an organic and inorganic part was introduced (O M Yaghi et al., 1995). Controllable synthesis conditions, designable organic ligands, tuneable pore sizes, high specific surface area, and the highly porous nature make MOFs attractive in H<sub>2</sub> storage applications (Andersson & Grönkvist, 2019; Balderas-Xicohténcatl, Schlichtenmayer, & Hirscher, 2018; García-Holley et al., 2018; Jianwei Ren et al., 2014a; G. Xu et al., 2019).

MOFs possess incredibly high H<sub>2</sub> adsorption capacities at high pressures and cryogenic temperatures (Abdalla et al., 2018; Kaye et al., 2007a; Jianwei Ren, Langmi, North, & Mathe, 2014b; Rowsell & Yaghi, 2004a). However, very low H<sub>2</sub> sorption capacities can be achieved at 298 K and low pressures (Klyamkin et al., 2014; Murray, Dincă, & Long, 2009). These low H<sub>2</sub> sorption capacities have been due to weak van der Waals interactions between H<sub>2</sub> molecules and the surface (Latroche, Surblé, Serre, Mellot-Draznieks, Llewellyn, Lee, Chang, Sung, et al., 2006a; Barbara Panella, Hirscher, Pütter, & Müller, 2006; Surblé, Millange, et al., 2006). In order to enhance the H<sub>2</sub> sorption capacities measured at 298 K, researchers have focused on increasing the surface area of MOFs. However, the effect of pore size has remained understudied. To the best of our knowledge, there are scarcely any reports that investigates the relation between the pore size and the adsorbed H<sub>2</sub> amount.

In this work, the effect of pore size on the adsorbed H<sub>2</sub> amount has been reported. Hierarchically porous MIL-88Bs were synthesized via a perturbation assisted nanofusion synthesis strategy and the fraction and the volume of textural pores were controlled by the iron to terephthalic acid (TPA) ratio (1, 3, and 5). By the control over textural porosity via Fe:TPA ratio, an ultramicroporous MOF structure (pores with pore diameters of 0.6 nm dominated the pore structure) with a BET surface area 2.11 and 2.74 times higher than those of reported MIL-88B's have been achieved (C. Gao et al., 2017; Hou et al., 2018). More importantly, the measured H<sub>2</sub> adsorption capacity at 298 K has been enhanced by a factor of 1.96. Our results reveal that H<sub>2</sub> adsorption capacity of porous structures (at 298 K and

pressures lower than 10 bar) are highly dependent on: i) the presence of ultramicropores; ii) high fraction of ultramicropores through the whole pore size distribution; and iii) the volume of ultramicropores (Aysu Yurduşen et al., 2019).

## **5.2. Experimental**

Synthesis and characterization analyses were conducted for five times. BET specific surface area, ultramicro-, micro-, upper meso-, and mesopore and total pore volumes were reported with calculated standard deviations.

### **5.2.1. Materials**

98% pure, ACS Reagent grade, iron(III) chloride hexahydrate ( $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ ) (Merck Millipore); and HPLC grade 98% pure terephthalic acid, 99.9% pure N, N-Dimethylformamide (DMF), and 99.8% pure methanol (MeOH) was used (Sigma Aldrich). Chemicals were used as they were received. An isothermal oven (Protherm Furnace), Teflon capped glass vials (ISOLAB) and a vacuum oven (Nüve, EV 018) was used during the synthesis of MIL-88B type MOF crystallites.

### **5.2.2. Synthesis**

3.1 mmol of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ , TPA (3.1 mmol or 1 mmol or 0.62 mmol) and 80 mL of DMF were vigorously stirred via a magnetic stirrer with a stirring rate of 800 rpm for an hour at 25 °C. Prepared clear solution was then distributed into glass vials capped with Teflon caps (20 mL). An isothermal oven was used to heat the samples for two days at 110 °C. Then the precipitates and the solution were distributed into 50 mL falcon tubes. A solvent exchange process was used for the washing procedure. Precipitates and the solution were washed with DMF (three times) and methanol (three times). Lastly, the precipitates were dried under vacuum at 100 °C for 30 hours. The abbreviations of hierarchically porous MIL-88Bs can be found below in Table 24. For the samples prepared with 3.1 mmol of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ , 3.1 mmol of TPA and 80 mL of DMF the sample abbreviation of MIL-88B-

1; for the samples synthesized with 3.1 mmol of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ , 1.03 mmol of TPA and 80 mL of DMF the sample abbreviation of MIL-88B-3; and for the samples prepared with 3.1 mmol of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ , 0.62 mmol of TPA and 80 mL of DMF the sample abbreviation of MIL-88B-5 have been used through the manuscript.

Table 24. Sample Abbreviations

| Sample Abbreviation | Fe:TPA ratio |
|---------------------|--------------|
| MIL-88B-1           | 1            |
| MIL-88B-3           | 3            |
| MIL-88B-5           | 5            |

### 5.2.3. Characterization Analysis

Powder x-ray diffraction (XRD), scanning electron microscopy (SEM) analysis,  $\text{N}_2$  sorption isotherms, pore size distribution analysis, nitrogen gas adsorption measurements, Fourier Transform Infrared Spectroscopy (FTIR), and thermogravimetric analysis (TGA) were used for structural characterization of the synthesized hierarchically porous MIL-88Bs. Each characterization analysis was repeated for five times and the results are reported with their respective standard deviations.

#### 5.2.3.1. X-Ray diffraction

X-ray diffraction analysis was carried out with a Bruker D2 Phaser XRD. The analysis was carried with a step size of  $0.02^\circ$  in between a  $2\theta$  range of 2 to  $90^\circ$ .

#### 5.2.3.2. Scanning electron microscopy (SEM)

Imaging was conducted with a Leo Supra 35VP field emission scanning electron microscope. Voltage and working distance were set in accordance with the MOF imaged.

#### **5.2.3.3. Brunauer-Emmett-Teller (BET) surface area and pore size distribution analysis**

BET surface area and pore size distribution analysis was conducted with a Micromeritics 3Flex Instrument.  $0.35 \pm 0.05$  grams (g) of MOF was used. Before each analysis, hierarchically porous MIL-88Bs were degassed at 120 °C for 6 hours. BET was used for surface area analysis and NLDFT model was used for pore size distribution analysis.

#### **5.2.3.4. Fourier Transform Infrared Spectroscopy (FT-IR) Analysis**

Thermo Scientific Nicolet Is10 was used for the FTIR analysis. A wavelength range of 600 to 4000  $\text{cm}^{-1}$  with a spectral resolution of 4  $\text{cm}^{-1}$  was used. Scans were repeated for 32 times and each spectrum was corrected for background noise.

#### **5.2.3.5. Thermogravimetric analysis**

Shimadzu DTG-60H simultaneous thermal analysis TG-DTA was used.  $49 \pm 5$  mg MOF was analyzed under an  $\text{N}_2$  flow of 20 mL/min. A heating rate of 10 K was used.

#### **5.2.3.6. $\text{H}_2$ sorption isotherm measurement**

$\text{H}_2$  uptake capacities were measured gravimetrically via Intelligent Gravimetric Analyzer (IGA) from very low (vacuum) to high pressures. Hydrogen adsorption studies were conducted in between 0 and 8 bar and at 298 K. A microbalance head placed in a stainless-steel vacuum-pressure reactor with  $\pm 1.0$   $\mu\text{g}$  sensitivity was used for accuracy. Hierarchically porous MIL-88Bs samples were outgassed at 120 °C for 6 hours.

### **5.3. Results and Discussion**

#### **5.3.1. XRD Analysis**

A perturbation assisted nanofusion synthesis strategy that forms hierarchical pores were used in the synthesis of hierarchically porous MIL-88Bs. Vigorously stirring iron salt, linker and DMF caused secondary building units (SBUs) to aggregate into nanosized MOF



crystallites which were later embedded in an amorphous matrix. Single crystal X-ray crystallography analyses proved that micro-sized single crystals were not formed and there were no metallic-iron present. Figure 82 illustrates the XRD patterns of hierarchically porous MIL-88Bs.

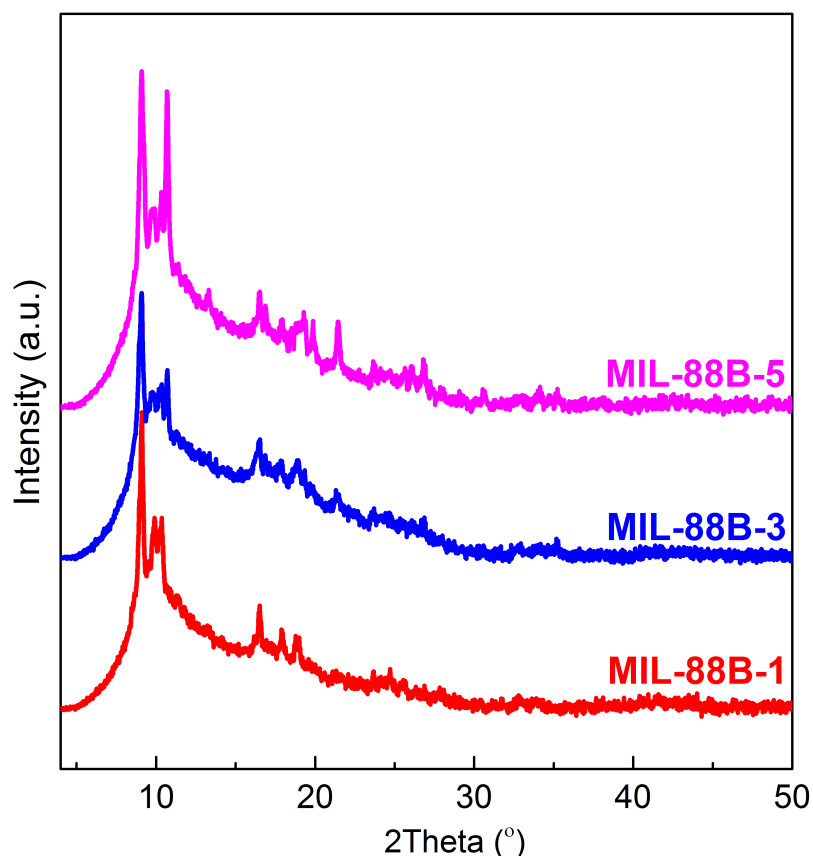


Figure 82. XRD patterns of MIL-88B-1, MIL-88B-3, and MIL-88B-5.

XRD patterns of the hierarchically porous MIL-88Bs agree well with the XRD pattern of the simulated MIL-88B (Surblé, Serre, Mellot-Draznieks, Millange, & Férey, 2006). Single crystal X-ray crystallography analyses demonstrated that micro-sized single crystals were not formed and there were no metallic-iron present. A comparison of the XRD pattern of the reference MIL-88B with the XRD patterns of the synthesized hierarchically porous MIL-88Bs can be found below in Figure 83.

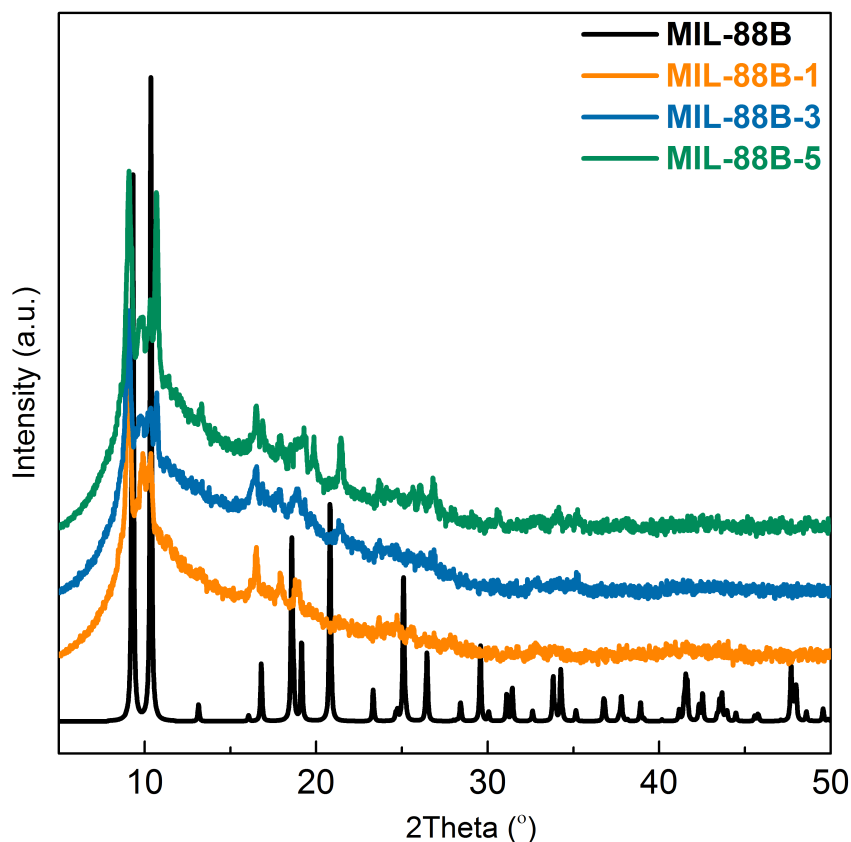


Figure 83. Comparison of XRD patterns of simulated MIL-88B and synthesized hierarchically porous MIL-88Bs.

Both the MIL-88B nanorods and the amorphous matrix at which MIL-88B nanorods were embedded in, cause the observed broadening in the XRD patterns as well as the amorphous nature of the XRD patterns.

In the case of MIL-88B-5, Bragg peaks were even more broadened. The broadened Bragg peaks are attributed to the excess amount of iron salt used during the synthesis. Excess amount of iron salt causes more iron oxide clusters to form which competes for TPA. Aggregates of excess iron oxide clusters form the MIL-88B nanorods.

### 5.3.2. SEM Images

Figure 84 illustrates the SEM images of MIL-88B-1, MIL-88B-3, and MIL-88-5.

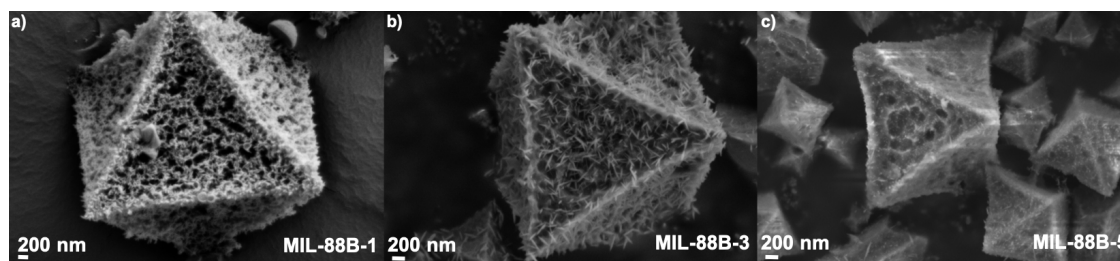


Figure 84. SEM images of hierarchically porous MIL-88Bs.

SEM images show the MIL-88B nanorods and the amorphous matrix at which the nanosized MIL-88B rods were embedded in. Hierarchically porous MIL-88Bs were formed by the precipitation of aggregated MIL-88B nanorods. Aggregated MIL-88B nanorods were precipitated on the amorphous matrix at which the interparticle voids formed the textural porosity. Textural pores with pore diameters ranging in between 2 to 50 nm can be seen as dark spots in Figure 84 a), b), and c).

### 5.3.3. N<sub>2</sub> Sorption Isotherms

BET surface areas of MIL-88B crystallites (MIL-88B-1: 400.4 m<sup>2</sup>/g; MIL-88B-3: 452.4 m<sup>2</sup>/g; MIL-88B-5: 445.9 m<sup>2</sup>/g) are higher than those of reported MIL-88B structures (C. Gao et al., 2017; Vuong et al., 2013a). The enhancement in the BET surface area is a consequence of the hierarchical pores introduced to the pore structure. Textural pores were formed by the coordination, nucleation and nanoparticle aggregation mechanism. MIL-88B nanocrystallites were embedded in an amorphous matrix at which the textural pores were formed. Introducing textural pores to the pore structure enhances BET surface areas and the pore volumes of the crystallites which are found to be higher than those of reported BET surface areas and pore volumes of MIL-88B (C. Gao et al., 2017; Vuong et al., 2013b). Figure 85-88 illustrates the respective N<sub>2</sub> sorption isotherms.

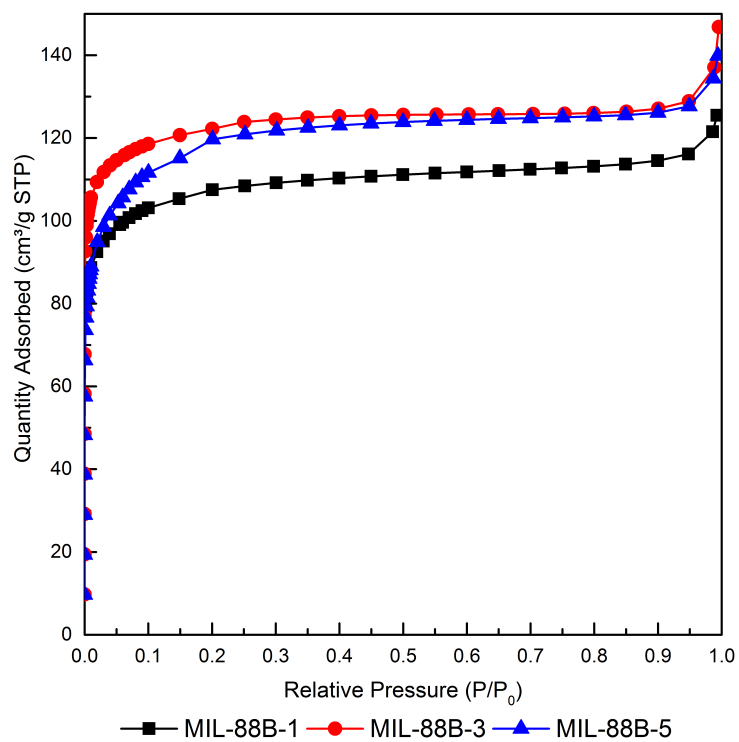


Figure 85. N<sub>2</sub> sorption isotherms of MIL-88B-1, MIL-88B-3, and MIL-88B-5.

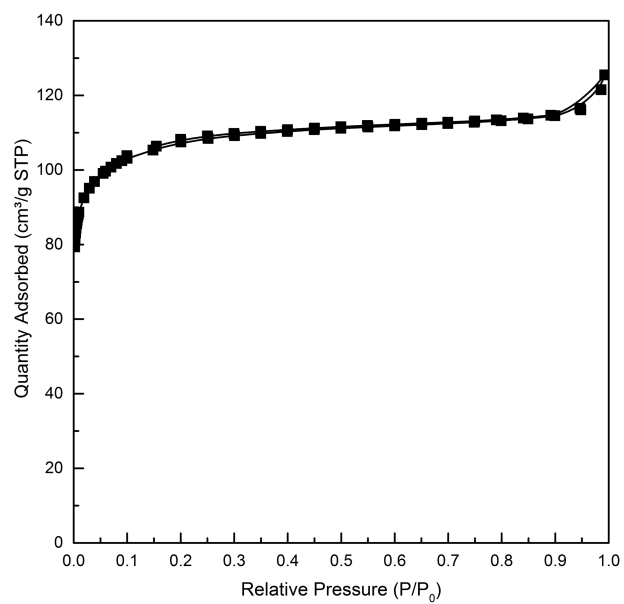


Figure 86. N<sub>2</sub> sorption isotherm of MIL-88B-1.

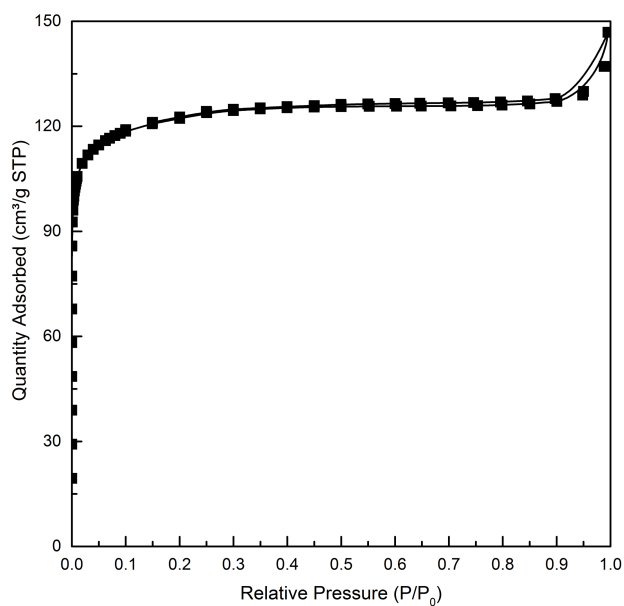


Figure 87. N<sub>2</sub> sorption isotherm of MIL-88B-3.

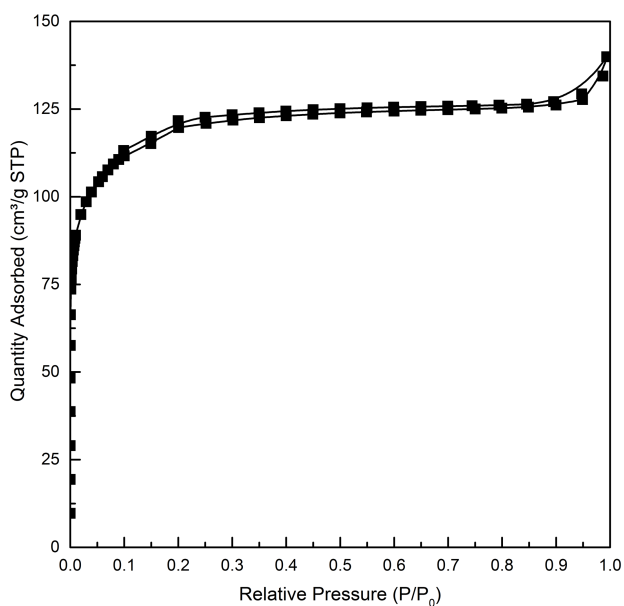


Figure 88. N<sub>2</sub> sorption isotherm of MIL-88B-5.

N<sub>2</sub> sorption isotherms of MIL-88B-1, MIL-88BB-3, and MIL-88B-5 have the features of IUPAC type I isotherms with some mesoporosity. At low relative pressures ( $P/P_0 < 0.1$ ) hierarchical porous MIL-88Bs show sharp increases in the adsorbed N<sub>2</sub> amount. In between the relative pressure ranges of 0.2 and 0.9 N<sub>2</sub> sorption isotherm of MIL-88B-3 possesses a horizontal plateau while a relatively small slope is observed in the N<sub>2</sub> sorption

isotherms of MIL-88B-1, and MIL-88B-5. This relatively small slope is associated with mesopore filling which is due to the presence of mesopores. At pressures close to saturation pressure ( $P/P_0 > 0.9$ ), the amount of  $N_2$  adsorbed increases which reveals that there are some mesopores present. Lastly, neither of the isotherms possess hysteresis. In order to compare the micropore volume, t-plot method is used.

#### 5.3.4. t-plot Method

t-plot method is used to estimate the micropore volumes of MIL-88B-1, MIL-88B-3, and MIL-88B-5. Respective t-plots of MIL-88B-1, MIL-88B-3, and MIL-88B-5 can be found in Figure 89-92.

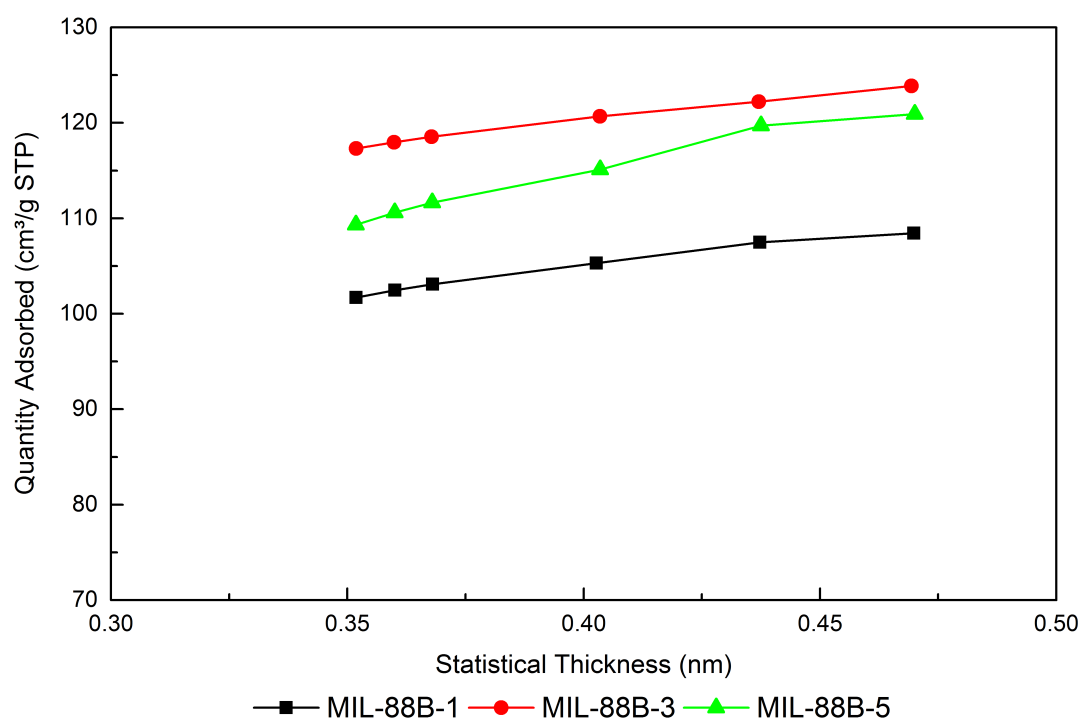


Figure 89. t-plots of MIL-88B-1, MIL-88B-3, and MIL-88B-5.

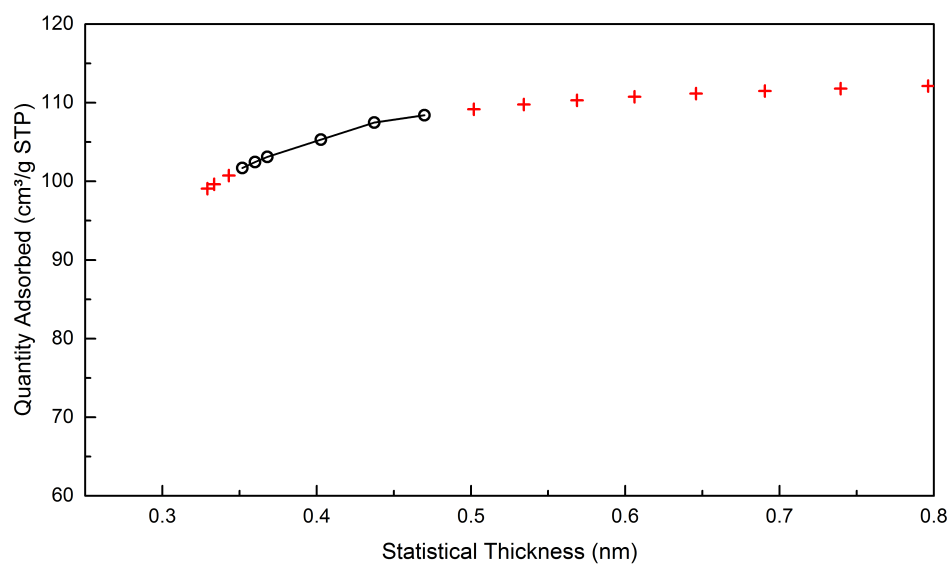


Figure 90. t-plot of MIL-88B-1.

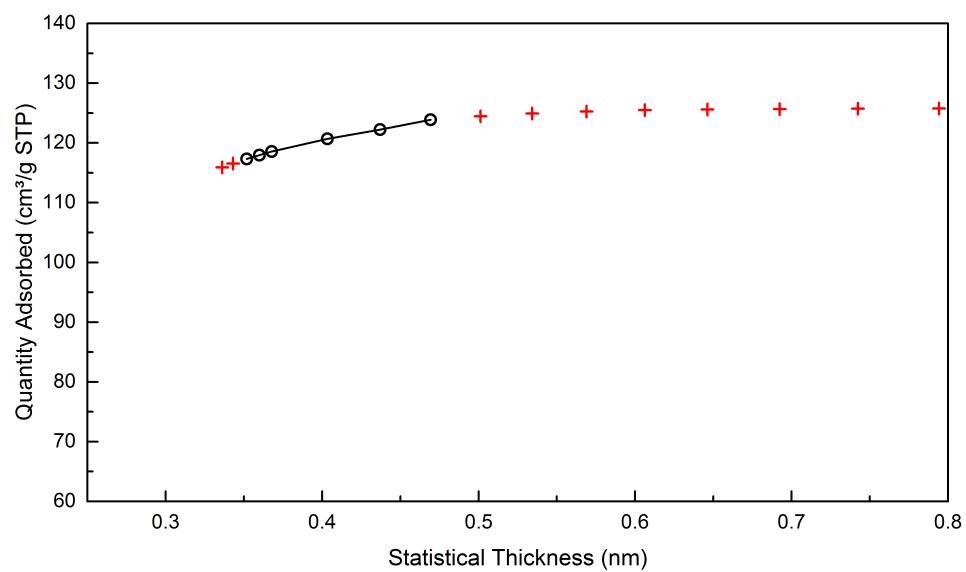


Figure 91. t-plot of MIL-88B-3.

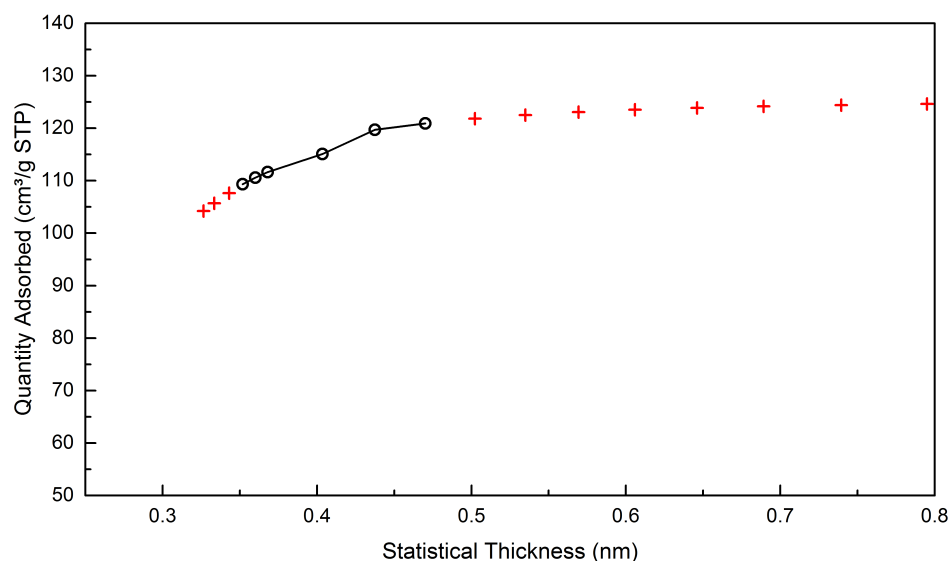


Figure 92. t-plot of MIL-88B-5.

MIL-88B-3 intersects y-axis at a considerably higher value than MIL-88B-1, and MIL-88B-5 evidencing that MIL-88B-3 possesses a relatively higher micropore volume than MIL-88B-1, and MIL-88B-5. For a better pore volume estimation NLDFT method has been used. Figure 93 illustrates the NLDFT plots of MIL-88B-1, MIL-88B-3, and MIL-88B-5.

### 5.3.5. NLDFT Method

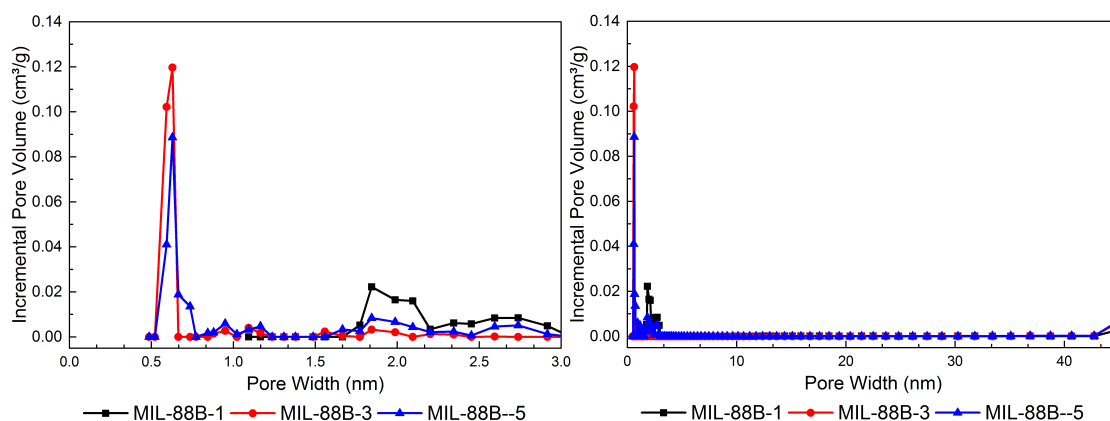


Figure 93. NLDFT plots of MIL-88B type MOF crystallites.

NLDFT plots of incremental pore volume-pore width show several increases within micro- and mesopore size range. In addition to the wide mesopores at 44.8 nm, some narrow



mesopores are also tracked. MIL-88B-1 is mainly formed of micropores (92%) while volume of mesopores contribute by 7.5%. NLDFT analysis shows that MIL-88B-1 has no pores with pore diameters ranging in between 3 to 11.2 nm. Pores within the mesopore size range occupy a volume of 0.01481 cm<sup>3</sup>/g which corresponds to 7.5% of the total pore volume. Pores with the pore diameters of 44.8 nm form 40% of the mesopores.

MIL-88B-3 does not have any pores narrower than 0.59 nm. The volume increase associated with micropores narrower than 0.62 nm corresponds to 89% of the total pore volume while micropores form 96.1% of the total pore volume. NLDFT analysis shows that there are no pores with pore diameters ranging in between 2.7 and 33.4 nm. In between 35 and 44.8 nm a relatively small increase in pore volume is observed. Within the mesoporous range, a volume increase of 0.0096 cm<sup>3</sup>/g which corresponds to 3.9% of the total pore volume is issued.

NLDFT plot of MIL-88B-5 shows a steep increase in the microporous region which is then followed by large and small volume increases till a pore diameter of 3 nm. The highest volume increase of 0.13 cm<sup>3</sup>/g is observed for pore diameters ranging between 0.59 nm and 0.62 nm which corresponds to 56.4% of the total pores. In brief, the volume increase in the microporous region corresponds to 87.8% of the total pore volume. There are no pores with pore diameters ranging between 3.1 to 30.3 nm. In the meanwhile, in between the pores with pore diameters of 31.8 and 44.8 nm a volume increase of 0.00768 cm<sup>3</sup>/g is observed. Table 25 illustrates the volume of ultramicropores, narrow micropores, micropores, and mesopores.

Table 25. Volume of ultramicropores, narrow micropores, micropores, and mesopores

| Hierarchical porous MIL-88Bs | Volume of ultramicropores (cm <sup>3</sup> /g) | Volume of narrow micropores (cm <sup>3</sup> /g) | Volume of micropores (cm <sup>3</sup> /g) | Volume of mesopores (cm <sup>3</sup> /g) |
|------------------------------|------------------------------------------------|--------------------------------------------------|-------------------------------------------|------------------------------------------|
| MIL-88B-1                    | -                                              | 0.177±1.7E-2                                     | 0.182±1.4E-2                              | 0.0165±1.4E-2                            |
| MIL-88B-3                    | 0.22                                           | 0.226±1.2E-2                                     | 0.239±3.2E-2                              | 0.0096±7.0E-3                            |
| MIL-88B-5                    | 0.16                                           | 0.172±1.7E-2                                     | 0.202±3.2E-2                              | 0.0281±1.7E-2                            |

## A possible mechanism for the widened mesopores in MIL-88B-5

The following mechanism is suggested for the widened mesopores in MIL-88B-5. To introduce textural pores, MIL-88B-1, MIL-88B-3, and MIL-88B-5 were synthesized by a perturbation assisted nanofusion synthesis strategy. By this way, single crystal growth would be prevented, and amount and fraction of textural pores can be controlled. Strongly stirring iron salt, TPA and DMF, prevented the single crystal growth. The vigorous stirring of iron salt, TPA and DMF, formed SBUs which aggregate into nanosized MIL-88B rods. The high Fe:TPA ratio used in the synthesis of MIL-88B-5 caused iron oxide clusters to form that compete for the limited amount of TPA present in the solution. Aggregated nanosized MIL-88Bs were embedded in the amorphous matrix at which interparticle voids formed the textural mesoporosity. We suggest that using a high Fe:TPA ratio caused more nanosized MIL-88B type MOF crystallites to aggregate which widens the interparticle voids (textural mesopores). Figure 94 shows the sequence of textural pore formation and Figure 95 illustrates the textural pore formation mechanism.



Figure 94. Schematic diagram of textural pore formation sequence.

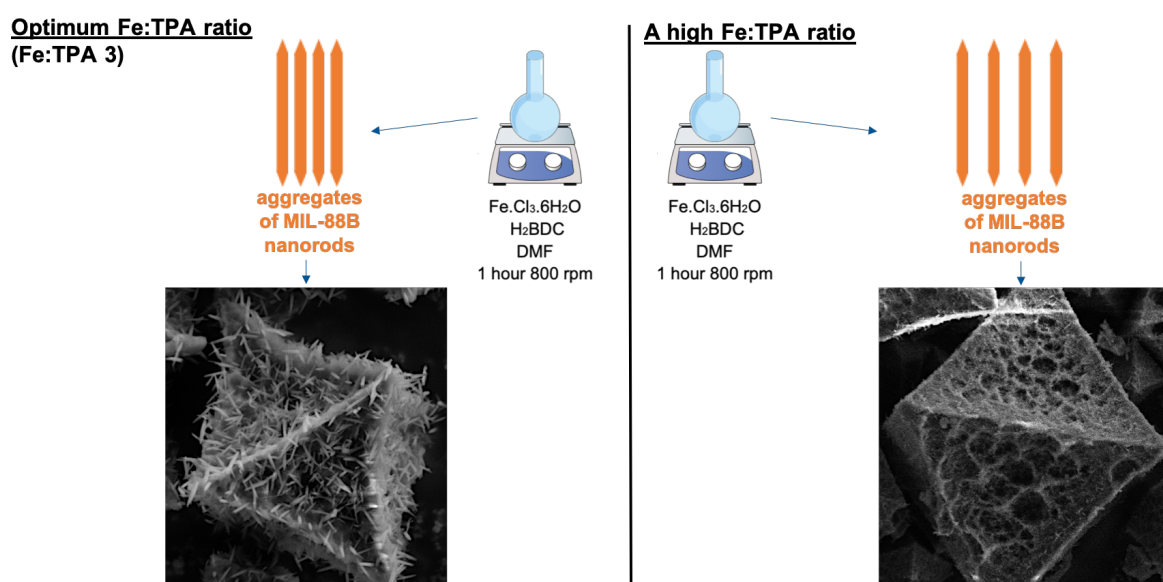


Figure 95. Schematic diagram of textural pore formation mechanism.

Our results show that in the presence of insufficient amount of terephthalic acid (a high Fe:TPA ratio), pore diameters widen, and the volume occupied by the pores at the upper mesoporous range increases. We have attributed the observed increase in the mesopore fraction to the formation of iron oxide clusters and aggregation of the nanosized MIL-88B-5 crystallites. Thereby, interparticle voids (textural mesopores) widen and the fraction of textural mesopores increases.

#### **5.3.6. FTIR Analysis**

Figure 96 illustrates FTIR spectra of hierarchical porous MIL-88Bs. FTIR spectra agree well with each other with some small changes in band shapes and peak intensities.

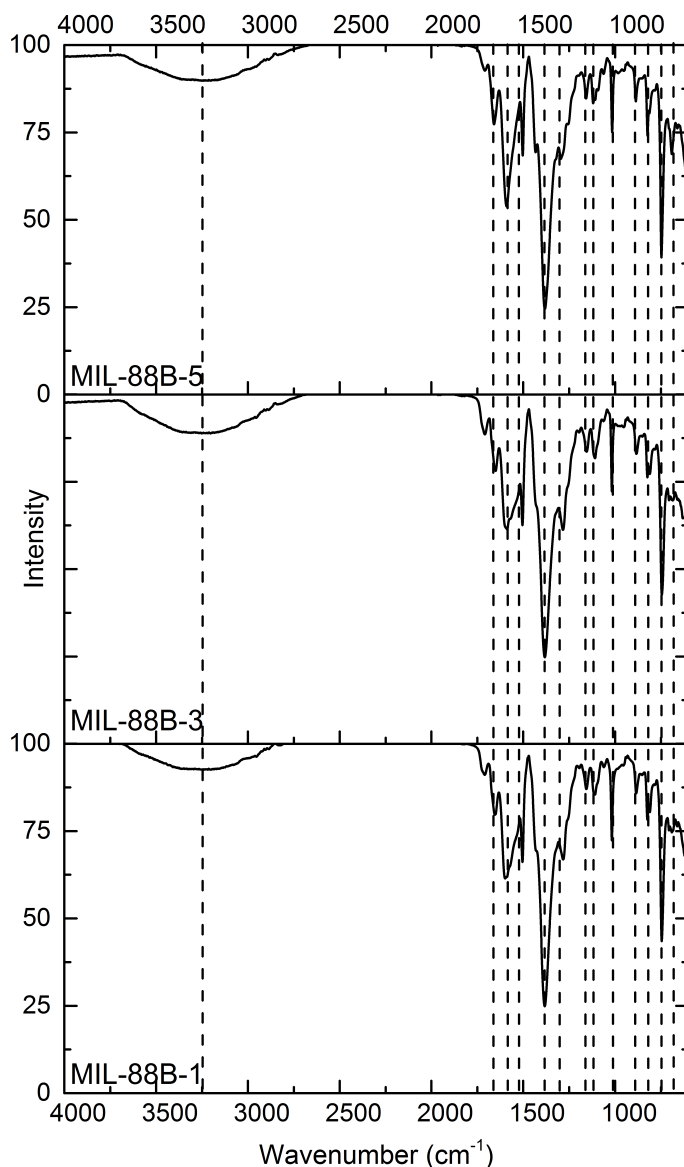


Figure 96. FTIR spectra of MIL-88B-1, MIL-88B-3, and MIL-88B-5.

In between the wavelengths of 3000 to 3600  $\text{cm}^{-1}$  broad bands typical of OH groups are observed. MIL-88B-5 possesses a wider band width with lower peak intensity than MIL-88B-1 and MIL-88B-3. In a study of Jacobs et. al., broadened OH bands were attributed to widened pore widths (Jacobs & Mortier, 1982). Having the broadest OH band with the lowest intensity, it is concluded that MIL-88B-5 possess larger pores in comparison to MIL-88B-1, and MIL-88B-3.

There is no peak at  $1704\text{ cm}^{-1}$  suggesting that most of the  $\text{H}_2\text{BDC}$  used during the synthesis are deprotonated. More importantly, using a  $\text{Cl}^-$  based metal salt eliminates the necessity to remove free terephthalic acid present in the sample.

Presence of peaks at  $1647\text{ cm}^{-1}$  illustrates that there is still some residual DMF left in the pores ( $1659\text{ cm}^{-1}$ ;  $\text{C}=\text{O}$  asymmetric stretching mode) (Sharma, Kaur, Mahajan, Tripathi, & Saini, 2007).

We have confirmed that we have formed the skeletal of our hierarchical porous MIL-88Bs by the peaks obtained in between the wavelengths  $1300$  and  $1650\text{ cm}^{-1}$ . Peaks at  $1385$  and  $1589\text{ cm}^{-1}$  illustrate that TPA was attached successfully to the metal center (Benbellat et al., 2006; Rowsell & Yaghi, 2006b; Tafipolsky et al., 2010).

The peaks obtained at  $1017\text{ cm}^{-1}$ ,  $1155\text{ cm}^{-1}$ ,  $1504\text{ cm}^{-1}$ , and  $1589\text{ cm}^{-1}$  are associated with a form of TPA (Arenas & Marcos, 1979; Téllez S. et al., 2001; Tripathi & Sheng, 1979). The peak at  $1017\text{ cm}^{-1}$  ( $\text{C}-\text{O}-\text{Fe}$  stretching mode) illustrates TPA was successfully attached to the metal center. In addition, the peaks obtained at  $742$  and  $823\text{ cm}^{-1}$  are assigned to  $\text{Fe}-\text{O}$  stretching mode proving that Fe is coordinated with TPA (Ye Li et al., 2015). Finally, the peak in between  $600$  and  $626\text{ cm}^{-1}$  is assigned to central oxygen in single  $\text{Fe}_3\text{O}$  and observed in the FTIR spectra of all the crystallites (Vuong et al., 2013a). Moreover, FTIR spectrum of hierarchically porous MIL-88Bs were compared with the FTIR spectra of  $\text{FeCl}_3.6\text{H}_2\text{O}$ . Having no peaks at  $842\text{ cm}^{-1}$ ,  $1594\text{ cm}^{-1}$ ,  $2993\text{ cm}^{-1}$ ,  $3212\text{ cm}^{-1}$ , and  $3523\text{ cm}^{-1}$  which are the characteristic peaks of  $\text{FeCl}_3.6\text{H}_2\text{O}$  showed that there are no metallic iron present.

### 5.3.7. Thermal Gravimetric Analysis (TGA)

Figure 97 illustrates the respective TGA curves. Similar TGA curves were obtained for the synthesized hierarchically porous MIL-88Bs. Detailed TGA results with percentage of mass losses is provided in Table 26.

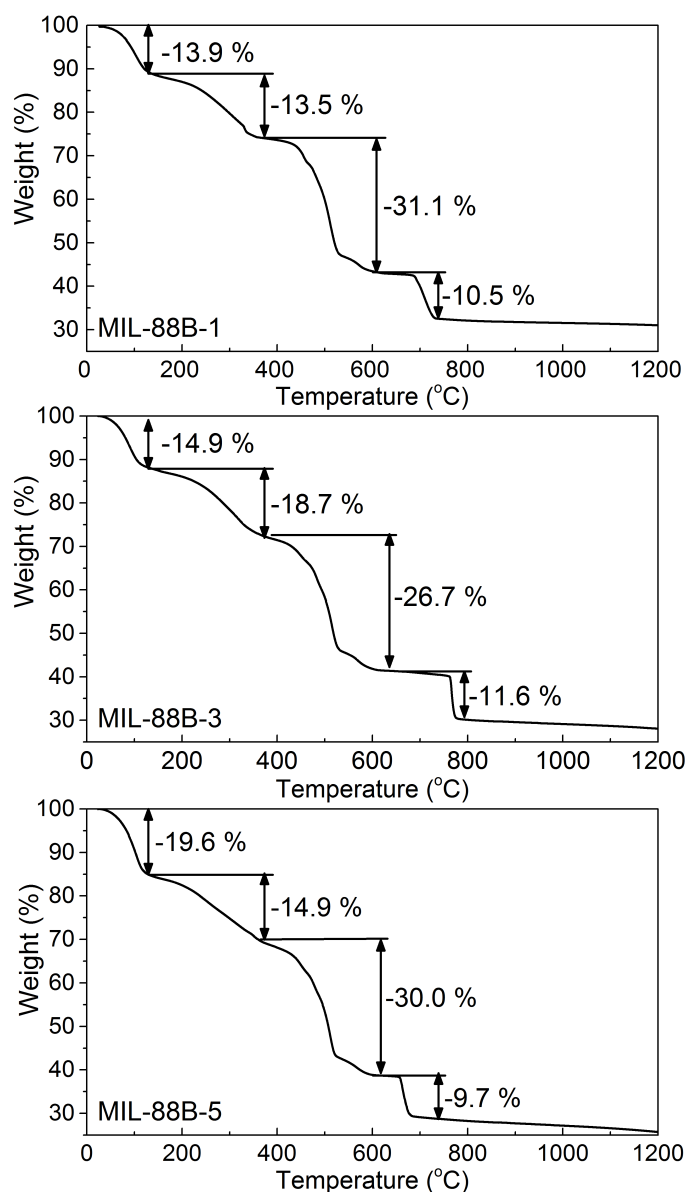


Figure 97. TGA curve of hierarchically porous MIL-88B.

Table 26. % mass loss during TGA

| Temperature Range (°C) | MIL-88B-1 (%) | Temperature Range (°C) | MIL-88B-3 (%) | Temperature Range (°C) | MIL-88B-5 (%) |
|------------------------|---------------|------------------------|---------------|------------------------|---------------|
| 25-185                 | -13.9         | 25-175                 | -14.9         | 25-169                 | -19.6         |
| 185-380                | -13.5         | 175-448                | -18.7         | 169-387                | -14.9         |
| 380-642                | -31.1         | 448-638                | -26.7         | 387-625                | -30           |
| 642-757                | -10.5         | 638-850                | -11.6         | 625-716                | -9.7          |

At the first step adsorbed and coordinated water and DMF molecules are lost. MIL-88B-5 has the highest amount of mass loss in the first step. The second step is associated with solvent molecules trapped in the pores. The third step occurs due to linker decomposition and MIL-88B-3 is found to decompose at a temperature higher than MIL-88B-1, and MIL-88B-5. Finally, the last step corresponds to CO<sub>2</sub> release during the decomposition of carboxylates. Additionally, TGA analysis shows that hierarchically porous MIL-88Bs are thermally stable under adsorption process conditions.

### 5.3.8. H<sub>2</sub> Sorption Analysis

Hierarchically porous MIL-88Bs synthesized with different Fe:TPA ratio (1, 3, and 5) possess different H<sub>2</sub> sorption capacities. Figure 98 illustrates H<sub>2</sub> adsorption isotherms.

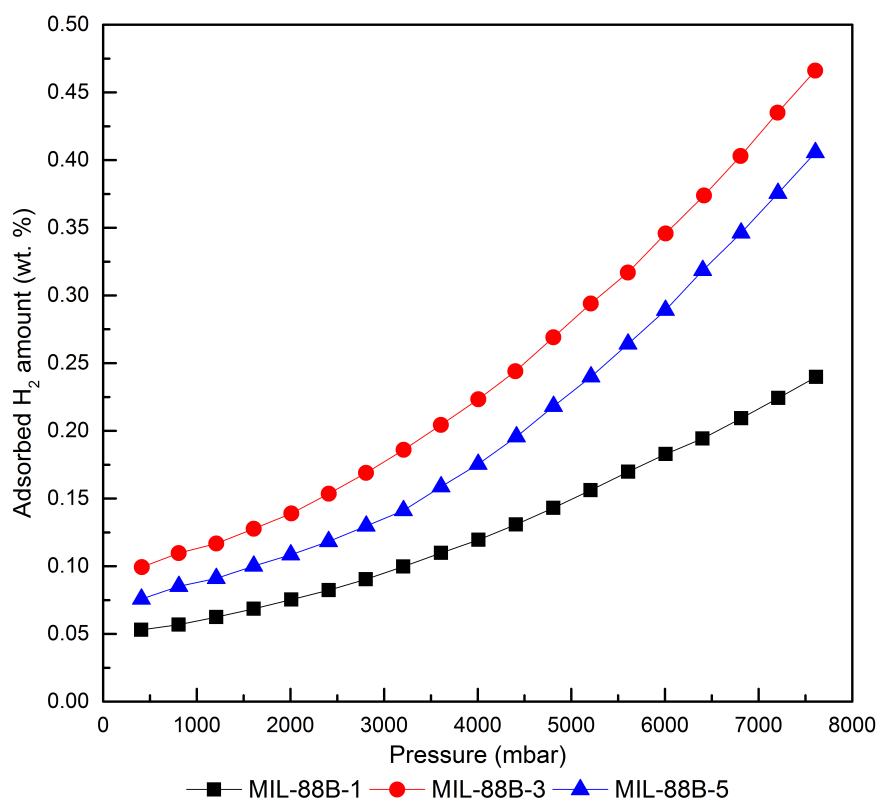


Figure 98. H<sub>2</sub> sorption isotherms of MIL-88B-1, MIL-88B-3, and MIL-88B-5 measured at 298 K.

Calculated Langmuir and Freundlich isotherm parameters and the representative plots comparing experimental data with the nonlinear fitting of Langmuir and Freundlich model can be found below. The Freundlich model describes H<sub>2</sub> adsorption behavior of MIL-88B type MOF crystallites measured at 298 K, better. However, as the adsorption studies were conducted till 8 bars, the shape of the isotherm may be misleading. Table 27-28 illustrate the respective coefficient of determination, R<sup>2</sup>, values for MIL-88B-1, MIL-88B-3, and MIL-88B-5. Table 29 presents the textural properties, H<sub>2</sub> sorption capacities (at 7.6 bar) and adsorbed H<sub>2</sub> amount per specific surface area of MIL-88B-1, MIL-88B-3, and MIL-88B-5.

#### Langmuir Model:

$$\frac{C_e}{q_e} = \frac{1}{KQ^0} + \frac{C_e}{Q^0} \quad (5.1)$$



**Freundlich Model:**

$$\log q_e = \log K_F + \frac{1}{n} \log C_e \quad (5.2)$$

Table 27. Respective equations obtained from models

| Hierarchically porous MIL-88Bs | Langmuir Model                            | Freundlich Model                         |
|--------------------------------|-------------------------------------------|------------------------------------------|
| MIL-88B-1                      | $y = 0.5001 x + 3790.4$<br>$R^2 = 0.5676$ | $y = 0.8398x - 3.2216$<br>$R^2 = 0.9759$ |
| MIL-88B-3                      | $y = 0.2509x + 2068.1$<br>$R^2 = 0.5104$  | $y = 0.8673x - 3.0457$<br>$R^2 = 0.9716$ |
| MIL-88B-5                      | $y = 0.2926x + 2697.3$<br>$R^2 = 0.4014$  | $y = 0.9502x - 3.4377$<br>$R^2 = 0.9588$ |

Table 28. Langmuir and Freundlich isotherm parameters

| Hierarchically porous MIL-88Bs | Langmuir Model                                       | Freundlich Model                  |
|--------------------------------|------------------------------------------------------|-----------------------------------|
|                                | $Q_m = 1.99 \text{ mg/g}$                            | $K_F = 6.0E-04$                   |
| MIL-88B-1                      | $K_a = 1.32E-04 \text{ mg}^{-1}$<br>$R^2 = 0.5676$   | $\eta_F = 1.19$<br>$R^2 = 0.9759$ |
|                                | $Q_m = 3.99 \text{ mg/g}$                            | $K_F = 9.0E-04$                   |
| MIL-88B-3                      | $K_a = 1.21E-04 \text{ mg}^{-1}$<br>$R^2 = 0.51$     | $\eta_F = 1.15$<br>$R^2 = 0.9716$ |
|                                | $Q_m = 3.42 \text{ mg/g}$                            | $K_F = 3.65E-04$                  |
| MIL-88B-5                      | $K_a = 1.0851E-04 \text{ mg}^{-1}$<br>$R^2 = 0.4014$ | $\eta_F = 1.05$<br>$R^2 = 0.9588$ |

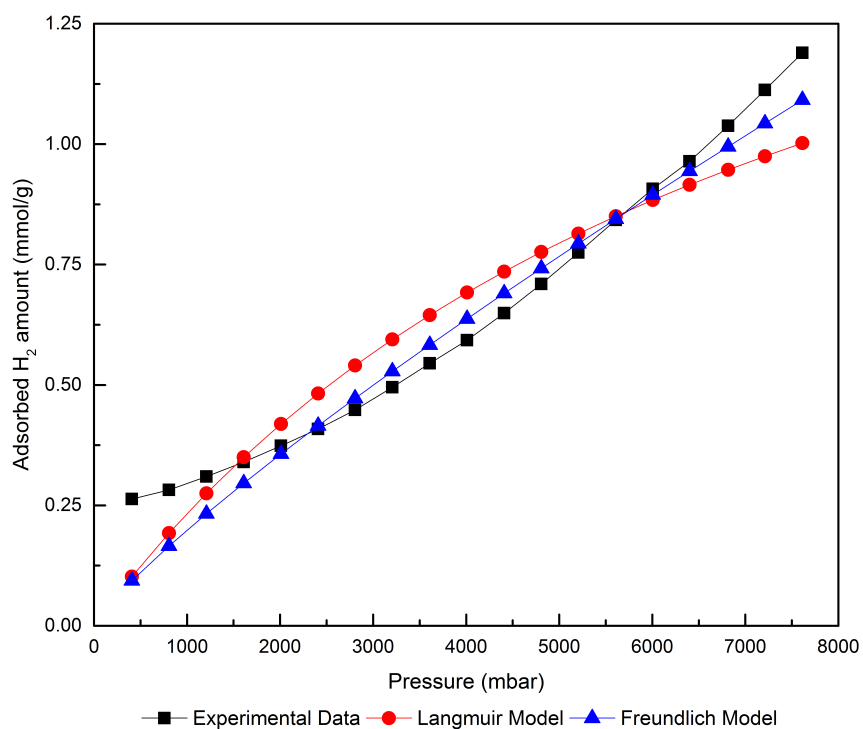


Figure 99. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich model of H<sub>2</sub> adsorption behavior on MIL-88B-1.

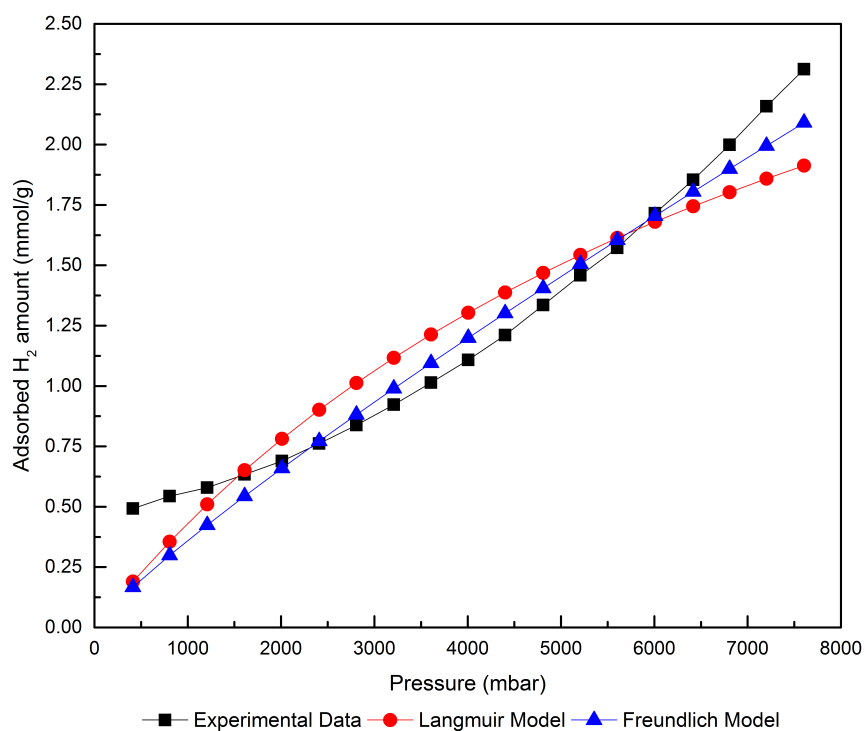


Figure 100. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich model of H<sub>2</sub> adsorption behavior on MIL-88B-3.

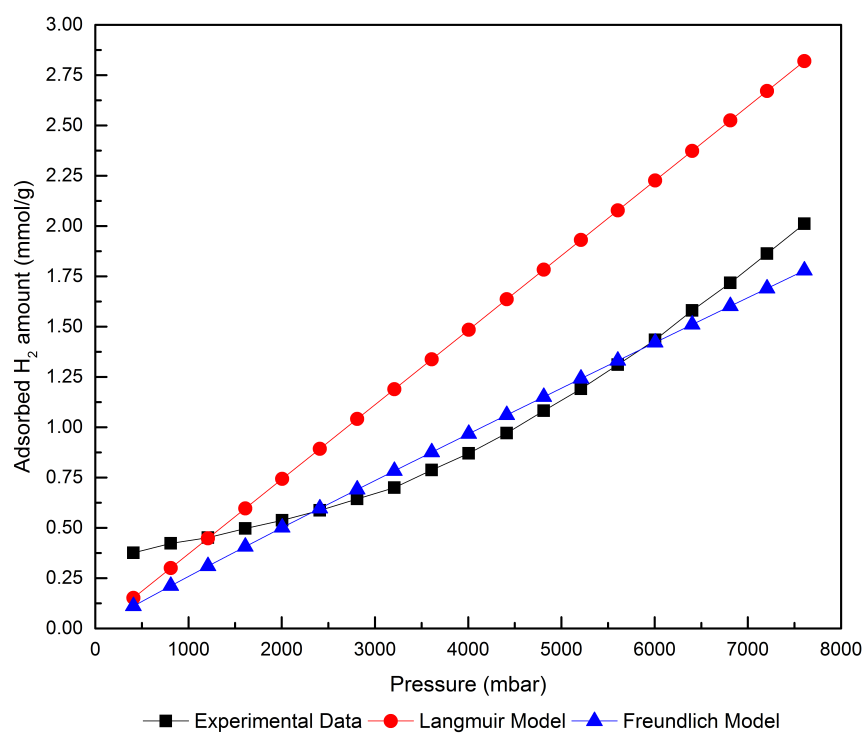


Figure 101. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich model of H<sub>2</sub> adsorption behavior on MIL-88B-5.

Table 29. Textural properties, H<sub>2</sub> sorption capacity (wt. % at 7.6 bar and 298 K), H<sub>2</sub> uptake per specific surface area (10<sup>3</sup> wt. % g/m<sup>2</sup>) of MIL-88B-1, MIL-88B-3, and MIL-88B-5

| Hierarchical porous MIL-88Bs | V <sub>micro</sub> (cm <sup>3</sup> /g) [a] | V <sub>meso</sub> (cm <sup>3</sup> /g) [b] | V <sub>narrow micro</sub> (cm <sup>3</sup> /g) [c] | V <sub>ultra micro</sub> (cm <sup>3</sup> /g) [d] | V <sub>ultramicro</sub> / V <sub>narrow micro</sub> [e] | H <sub>2</sub> sorption capacity (wt. %) [f] | H <sub>2</sub> uptake per SSA (10 <sup>3</sup> wt.% g/m <sup>2</sup> ) [g] |
|------------------------------|---------------------------------------------|--------------------------------------------|----------------------------------------------------|---------------------------------------------------|---------------------------------------------------------|----------------------------------------------|----------------------------------------------------------------------------|
| MIL-88B-1                    | 0.182±1.4E-2                                | 0.0165±1.4E-2                              | 0.177±1.7E-2                                       | -                                                 | -                                                       | 0.24                                         | 0.599                                                                      |
| MIL-88B-3                    | 0.239±3.2E-2                                | 0.0096±7E-3                                | 0.226±1.2E-2                                       | 0.221                                             | 0.98                                                    | 0.47                                         | 1.03                                                                       |
| MIL-88B-5                    | 0.202±3.2E-2                                | 0.0281±1.7E-2                              | 0.172±1.7E-2                                       | 0.162                                             | 0.94                                                    | 0.41                                         | 0.909                                                                      |

[a] Micropore volume (cm<sup>3</sup>/g)

[b] Mesopore volume (cm<sup>3</sup>/g)

[c] Narrow micropore volume (cm<sup>3</sup>/g)

[d] Ultramicropore volume (cm<sup>3</sup>/g)

[e] Fraction of ultramicropore volume to narrow micropore volume

[f] at 7.6 bar and 298 K

[g] H<sub>2</sub> uptake per specific surface area

MIL-88B-3 whose BET surface area and the ultramicropore volume (0.22 cm<sup>3</sup>/g) are the highest among the synthesized hierarchical porous MIL-88Bs, possesses the highest H<sub>2</sub> adsorption capacity (0.47 wt.% at 7.6 bar and 298 K). at which ultramicropores possess a volume of 0.22 cm<sup>3</sup>/g (98% of the narrow micropore volume) and narrow micropores possess a volume of 0.226 cm<sup>3</sup>/g.

MIL-88B-5 that is formed of ultramicropores (0.162 cm<sup>3</sup>/g) possesses a H<sub>2</sub> adsorption capacity 1.69 times greater than MIL-88B-1. Despite the low narrow micropore volume of MIL-88B-5, MIL-88B-5 possesses ultramicropores in its pore structure, whereas there are no ultramicropores in the pore structure of MIL-88B-1. Therefore, the higher (1.69 times) H<sub>2</sub> adsorption capacity of MIL-88B-5 is attributed to: i) the presence of ultramicropores; and ii) the relatively narrower micropore size distribution. Figure 102 illustrates the different micropores size distribution of MIL-88B-1, MIL-88B-3, and MIL-88B-5 and Figure 103 and 104 illustrate the different pore size distributions of MIL-88B-1, MIL-88B-3, and MIL-88B-5.

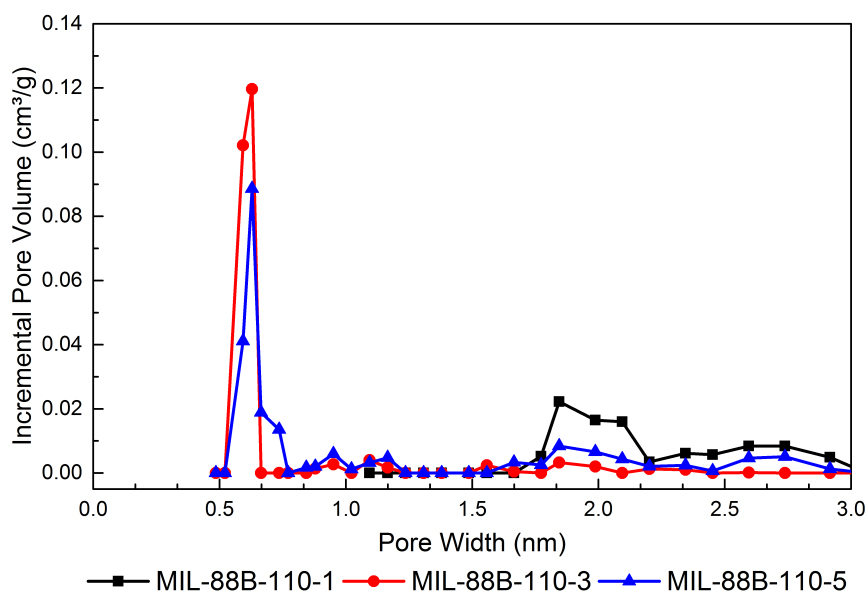


Figure 102. NLDFT plots of incremental pore volume versus pore width of hierarchical porous MIL-88Bs.

Vigorously stirring  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ , TPA and DMF formed textural pores and differences in Fe:TPA ratio resulted in differences in textural porosity. NLDFT plot of MIL-88B-3 shows a sharp peak in 0.6 nm while MIL-88B-5 has a broadened peak centered at 0.65 nm with a lower volume increase with some small peaks located within the microporous range. In the case of MIL-88B-1, two peaks: i) one centred at the upper microporous range; and ii) the other centred at lower mesoporous range are observed. Different from MIL-88B-1 and MIL-88B-5, MIL-88B-3 is mainly formed of pores with identical pore sizes (0.6 nm). In the meantime, MIL-88B-1 and MIL-88B-5 possess a broader pore size range. Apparently, MIL-88B-5 is formed of micropores at the upper micropore size range and lower mesopore size range (pore diameter < 5 nm).

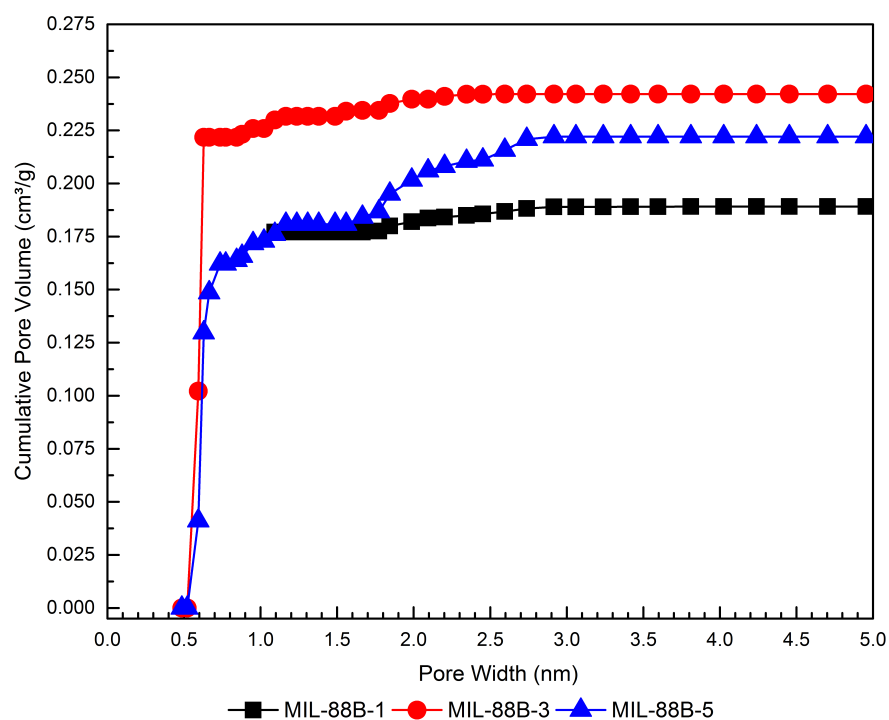


Figure 103. NLDFT plots of cumulative pore volume versus pore width of hierarchical porous MIL-88Bs.

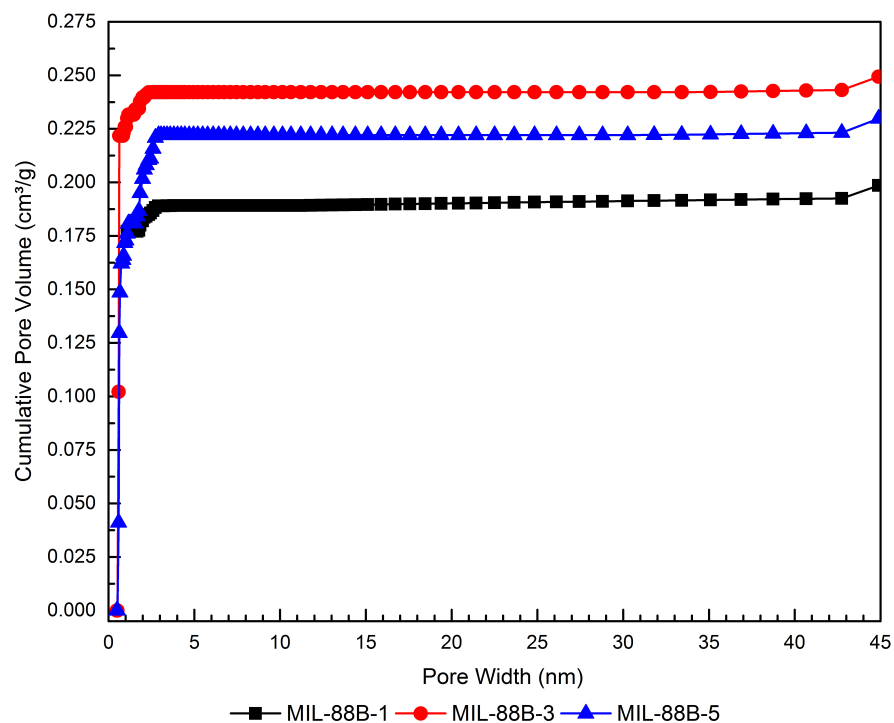


Figure 104. NLDFT plots of cumulative pore volume versus pore width of MIL-88B crystallites.

Unlike MIL-88B-1, and MIL-88B-5, MIL-88B-3 is mainly formed of pores with identical pore sizes (0.6 nm) and volume of these pores correspond to 89% of the overall pore volume. It is known that physisorption mechanism dominates adsorption in MOFs, and pore size influences the storage density heavily (Murray, Dincă, et al., 2009). More importantly, it is reported that at room temperature, pores that possess pore diameters of 6 to 8 Å achieves the highest van der Waals potential which can be explained by Lenard-Jones potential (Schlichtenmayer & Hirscher, 2012). Attractive forces dominate when the adsorbent and the hydrogen molecule is separated by a long distance whereas repulsion forces dominate when the adsorbent and the hydrogen molecule is separated by a short distance (Schlichtenmayer & Hirscher, 2012). Interestingly, theoretical studies show that when H<sub>2</sub> molecules are adsorbed on the wide pores, a hydrogen layer would be formed on the wells located close to the pore walls and a less dense layer of hydrogen would be adsorbed on the center of the pore which minimizes the attraction force felt by the pore walls and thereby, H<sub>2</sub> adsorption capacity decreases (Becher et al., 2003; Broom et al., 2019; Murray, Dincă, et al., 2009; Barbara Panella et al., 2005a; Schlichtenmayer & Hirscher, 2012, 2016; Schlichtenmayer, Streppel, & Hirscher, 2011).

In line with literature, we have found that the order of H<sub>2</sub> sorption capacity is from the highest to the lowest in accordance with the highest to the lowest volume of ultramicropores. Volume of ultramicropores present in MIL-88B-5 (0.162 cm<sup>3</sup>/g) is 1.4 times less than the volume of ultramicropores present in MIL-88B-3 (0.221 cm<sup>3</sup>/g). The significant increase in the adsorbed H<sub>2</sub> amount is attributed to: i) the presence of pores with pore sizes smaller than 0.7 nm which have stronger van der Waals interactions between the pore walls and H<sub>2</sub> molecules, ii) the higher volume of ultramicropores, and iii) the narrower pore size distribution (Rehman & Park, 2019a, 2019b; Schlichtenmayer & Hirscher, 2012; Schlichtenmayer et al., 2011; Qinyu Wang & Johnson, 1999).

Our results reveal that the volume of ultramicropores and their distribution within the microporous range influence the adsorbed H<sub>2</sub> amount heavily. MIL-88B-3 that is formed mainly of pores with pore diameters of 0.6 nm (89%) possesses an H<sub>2</sub> adsorption capacity 1.96 and 1.15 times greater than the measured H<sub>2</sub> sorption capacity of MIL-88B-1, and MIL-88B-5, respectively.



#### 5.4. Comparison with Literature

Highly porous MOFs come to fore with their high surface area and low density in H<sub>2</sub> sorption studies (Murray, Dincă, et al., 2009). MIL-88B-3 possesses the highest H<sub>2</sub> sorption capacity among the synthesized hierarchical porous MIL-88Bs. Table 30 shows the reported H<sub>2</sub> sorption capacities of some of the MOFs.

Table 30. H<sub>2</sub> sorption capacities of MOFs

| MOF                                        | Pressure (bar) | Temperature (K) | H <sub>2</sub> sorption capacity (wt. %) | Reference                                                                               |
|--------------------------------------------|----------------|-----------------|------------------------------------------|-----------------------------------------------------------------------------------------|
| MIL-88B type MOF crystallites (this study) | 7.6            | 298             | 0.47                                     |                                                                                         |
| MIL-100                                    | 73.3           | 298             | 0.15                                     | (Latroche, Surblé, Serre, Mellot-Draznieks, Llewellyn, Lee, Chang, Sung, et al., 2006b) |
| MIL-101 (Cr)                               | 80             | 298             | 0.43                                     | (Latroche, Surblé, Serre, Mellot-Draznieks, Llewellyn, Lee, Chang, Sung, et al., 2006b) |
| Co <sub>2</sub> (BDC) <sub>2</sub> dabco   | 10             | 298             | 0.03                                     | (L. G. Zhu & Xiao, 2008)                                                                |
| HKUST-1                                    | 65             | 298             | 0.35                                     | (Barbara Panella et al., 2006)                                                          |
| ZIF-8                                      | 60             | 298             | 0.13                                     | (W. Zhou, Wu, Hartman, & Yildirim, 2007)                                                |
| MOF-5                                      | 65             | 298             | 0.28                                     | (Barbara Panella et al., 2006)                                                          |
| IRMOF-8                                    | 30             | 298             | 0.4                                      | (Dailly, Vajo, & Ahn, 2006)                                                             |
| ZIF-8                                      | 60             | 298             | 0.13                                     | (W. Zhou et al., 2007)                                                                  |

By introducing textural pores to the pore structure of MIL-88Bs and the control of textural porosity via Fe:TPA ratio, a H<sub>2</sub> adsorption capacity higher than some of those reported MOFs has been achieved. For instance, MIL-100 with a Langmuir surface area of

2700 m<sup>2</sup>/g possesses an H<sub>2</sub> sorption capacity of 0.15 wt.% at 73.3 bar and 298 K (Latroche, Surblé, Serre, Mellot-Draznieks, Llewellyn, Lee, Chang, Sung, et al., 2006a); MIL-101(Cr) with a Langmuir surface area of 5500 m<sup>2</sup>/g possesses an H<sub>2</sub> sorption capacity of 0.43 wt.% at 80 bar and 298 K (Latroche, Surblé, Serre, Mellot-Draznieks, Llewellyn, Lee, Chang, Sung, et al., 2006a); Co<sub>2</sub>(BDC)<sub>2</sub>dabco with a BET surface area of 1595 m<sup>2</sup>/g possesses an H<sub>2</sub> sorption capacity of 0.03 wt.% at 10 bar and 298 K (L. G. Zhu & Xiao, 2008); HKUST-1 (Cu<sub>3</sub>BTC)<sub>2</sub> with a BET surface area of 1154 m<sup>2</sup>/g possesses an H<sub>2</sub> sorption capacity of 0.35 wt.% at 65 bar and 298 K (Barbara Panella et al., 2006); ZIF-8 with a BET surface area of 1630 m<sup>2</sup>/g possesses an H<sub>2</sub> sorption capacity of 0.13 wt.% at 60 bar and 298 K (W. Zhou et al., 2007); MOF-5 with a BET surface area of 2296 m<sup>2</sup>/g possesses an H<sub>2</sub> sorption capacity of 0.28 wt.% at 65 bar and 298 K (Barbara Panella et al., 2006); IRMOF-1 with a BET surface area of 572 m<sup>2</sup>/g possesses an H<sub>2</sub> sorption capacity of 0.2 wt.% at 67 bar and 298 K; and IRMOF-8 with a Langmuir surface area of 1818 m<sup>2</sup>/g possesses an H<sub>2</sub> sorption capacity of 0.4 wt.% at 30 bar and 298 K (Dailly et al., 2006); and ZIF-8 with a BET surface area of 1630 m<sup>2</sup>/g possesses an H<sub>2</sub> sorption capacity of 0.13 wt.% at 60 bar and 298 K (W. Zhou et al., 2007).

Despite the relatively low BET surface area (452.4 m<sup>2</sup>/g) of the hierarchically porous MIL-88Bs, their measured H<sub>2</sub> sorption capacity of 0.47 wt.% (298 K, 7.6 bar) is higher than the above-mentioned MOFs (Table 30). By the formation and control of textural porosity, a highly ultramicroporous MIL-88B is synthesized at which ultramicropores with pore diameters of 0.6 nm (89% of the total pore volume) dominate the pore structure and an H<sub>2</sub> adsorption capacity (0.47 wt.% at 7.6 bar and 298 K) that is greater than those of reported MOFs is attained.

## 5.5. Concluding Remarks

This study reveals the significant effect of ultramicropores on the adsorbed H<sub>2</sub> amount. Hierarchical porous MIL-88Bs were synthesized by a perturbation assisted nanofusion synthesis strategy that forms textural pores. The fraction and volume of textural mesoporosity were controlled by Fe:TPA ratio. MIL-88B-1, MIL-88B-3, and MIL-88B-5 with different pore size distributions show different H<sub>2</sub> sorption capacities (0.24, 0.47, and 0.405 wt.%, respectively at 7.6 bar and 298 K). The highest H<sub>2</sub> adsorption capacity (0.47

wt.% H<sub>2</sub> sorption capacity at 7.6 bar and 298 K) belongs to MIL-88B-3 (MIL-88B-3) which possesses the highest fraction (89%) and volume (0.22 cm<sup>3</sup>/g) of ultramicropores. Additionally, a BET surface area 2.11 and 2.74 times higher than those of reported MIL-88B's has been achieved (C. Gao et al., 2017; Hou et al., 2018). Moreover, by the formation and control of hierarchical pores, the fraction of ultramicropores was increased to 89% which results measured H<sub>2</sub> adsorption capacities to increase by a factor of 1.96 (0.47 wt.% at 7.6 bar and 298 K). This measured H<sub>2</sub> adsorption capacity (at 7.6 bar and 298 K) of MIL-88B-3 is higher than some of those reported and commercially available MOFs which is thought to be a consequence of its high fraction of pores with pore diameters of 0.6 nm (89% of the total pore volume was formed of pores with 0.6 nm diameter) (Murray, Dincă, et al., 2009; Qinyu Wang & Johnson, 1999).

Our results show that H<sub>2</sub> adsorption capacity measured at 298 K is dependent on: i) the pore size of the porous sorbents (H<sub>2</sub> favors ultramicropores); and ii) the narrow distribution of ultramicropores through the micropore size distribution (high fraction of ultramicropores). This study is an experimental proof of the critical role of fraction and volume of ultramicropores on the adsorbed H<sub>2</sub> amount. The control of textural porosity via Fe:TPA ratio leads the way to increase the fraction of ultramicropores and thereby, enhances H<sub>2</sub> adsorption capacities at 298 K. Further studies should be focused on synthesizing MOFs formed of high fraction and volume of ultramicropores with pore diameters of 0.6 nm which would be the key to enhance H<sub>2</sub> sorption capacities measured at 298 K.

## Chapter VI

### Carbon dioxide adsorption capacity of Basolite F300 like hierarchical porous Fe-BTCs and the role of ultramicropores

#### 6.1. Background

From pre-industrial period (1850 to 1900) till today, global mean surface temperature has increased by 1 °C (IPCC, 2018). In the evidence of increased global mean surface temperature, climate and weather extremes become more apparent (IPCC, 2018). The greenhouse gas emissions measured in 2010 were the highest of those measured greenhouse gas emissions through the human history.

Within the framework of Paris Agreement, a target has been set to decrease the greenhouse gas emissions. Among the greenhouse gasses CO<sub>2</sub> is the one that plays the key role in climate change (Ciais et al., 2013). Particularly, water vapor, methane, and nitrous oxides leave the atmosphere in 10 days, 10 years, and 100 years, respectively, while 10% of the CO<sub>2</sub> produced today remains in the atmosphere for 10 thousand years (Ciais et al., 2013). Within the last forty years, cumulative CO<sub>2</sub> concentrations reached the 50% of the cumulative CO<sub>2</sub> concentrations measured in between 1750 and 2010 (Intergovernmental Panel on Climate Change, 2014) and Intergovernmental Panel on Climate Change pointed out the necessity to develop and improve technologies to decrease CO<sub>2</sub> emissions (Metz et al., 2005). CO<sub>2</sub> capture and storage (CCS) technologies come to the fore with its ability to decrease CO<sub>2</sub> emissions by 80 to 90% (Metz et al., 2005) at which CO<sub>2</sub> is first separated from its source, then transported and stored at a site.

In order to increase the efficiency and the practical use of CCS technologies, researchers pointed out the need of cost-effective functional materials that will decrease the energy requirements and eliminate the by-product formation (S. Choi et al., 2009a; Cuéllar-Franca & Azapagic, 2015).

MOFs are highly crystalline materials that are introduced in 1995 (O M Yaghi et al., 1995). MOFs are formed of an organic and an inorganic part (O M Yaghi et al., 1995) and

come to the fore among the porous materials with their designable organic ligands, tunable pore structure, and high chemical stability (Rowsell & Yaghi, 2004a). MOFs have the listed advantages over other porous sorbents: i) reticular chemistry allow MOFs to be designed with the desired properties (Furukawa, Cordova, O’Keeffe, & Yaghi, 2013); ii) MOFs can be controlled at molecular level (Juncong Jiang, Zhao, & Yaghi, 2016); and iii) high and tuneable porosity allow MOFs to store large amounts of gases. Particularly, activated carbons with high BET surface areas and pore volumes have limited use in CO<sub>2</sub> capture studies due to their low CO<sub>2</sub>/N<sub>2</sub> selectivity. Similarly, despite their high BET surface areas, the low CO<sub>2</sub> uptake capacities of zeolites decrease their use in CCS studies. To illustrate, CO<sub>2</sub> adsorption capacity of MOF-177 is 9 times higher than zeolite 13X at 35 bar (S. Choi et al., 2009a). Thereby, synthesizing MOFs with high BET surface for high CO<sub>2</sub> adsorption capacity has drawn particular attention.

The conventional MOF synthesis lasts for days to weeks and only a few milligrams of MOF can be produced. However, a large quantity of MOF is needed for industrial and commercial uses. Researchers have been searching for synthesis methods that produce high yields of MOF. MIL-53(Al) (Basolite A100), HKUST-1 (Basolite C100), Fe-BTC (Basolite F300), ZIF-8 (Basolite Z1200), MOF-177 (Basolite Z377), and magnesium formate (Basosiv M050) have been commercialized under the name of Basolite. Among the commercialized MOFs, Fe-BTC (Basolite F300) stands out among the others with its high thermal stability and low toxicity (Horcajada et al., 2012). Additionally, the high BET surface area and the high porosity of Fe-BTC (Basolite F300), increases its possibility to be used in CO<sub>2</sub> capture studies.

Fe-BTC (Basolite F300) is formed of Fe(III) and BTC (benzene-1,3,5-tricarboxylic acid). Interestingly, there is another MOF structure formed of the same starting chemicals, MIL-100(Fe). But these two MOFs differ from each other by their relative crystallinities, and BET surface areas. MIL-100(Fe) is a highly crystalline MOF while Fe-BTC (Basolite F300) has a disordered nature. Even though the crystal structure of Fe-BTC (Basolite F300) has been a mystery, its structure is thought to be similar of MIL-100(Fe), at which trimers of iron octahedra share a common vertex and linked by benzene-1,3,5-tricarboxylic acid.

To the best of our knowledge, despite its high BET surface area and porosity, there has been a study that has reported the CO<sub>2</sub> adsorption capacity of Fe-BTC (Basolite F300) (M. Du, Li, Li, & Si, 2016).

Herein, we report the CO<sub>2</sub> adsorption capacity of a series of Fe-BTC synthesized by a perturbation assisted nanofusion synthesis strategy that forms hierarchical pores. By the perturbation assisted nanofusion synthesis strategy, BET surface area, and total pore volume are increased by a factor of 1.6 and 3.1 times, respectively (Dhakshinamoorthy, Alvaro, Chevreau, et al., 2012; Dhakshinamoorthy, Alvaro, & Garcia, 2011; Dhakshinamoorthy, Alvaro, Horcajada, et al., 2012) and a Fe-BTC that possesses ultramicropores were formed. The reported BET surface area, and total pore volume are the highest of the BET surface area, and total pore volume reported for Fe-BTC, so far (Dhakshinamoorthy et al., 2011; Dhakshinamoorthy, Alvaro, & Garcia, 2012; M. Du et al., 2016; X. Hu et al., 2016; Opanasenko et al., 2013; Zuka, Opanasenko, Rubeš, Nachtigall, & Jagiello, 2015).

Among the synthesized Fe-BTCs, the highest CO<sub>2</sub> uptake capacity (5.20 wt.% at 1 bar and 298 K, 27.5 wt.% at 8.5 bar and 298 K) belongs to Fe-BTC-150-3 which is also higher than those of MOFs reported in literature (Gumma, Chowdhury, & Bikkina, 2009; Loiseau et al., 2006; Mallick, Saha, Pachfule, Roy, & Banerjee, 2010; Mason, Sumida, Herm, Krishna, & Long, 2011b; Millward & Yaghi, 2005a; W. Morris et al., 2010; H. J. Park, Cheon, & Suh, 2010; Phan et al., 2010; Surblé, Millange, et al., 2006; Wiersum et al., 2011; A. Ö. Yazaydin et al., 2009).

Our results demonstrate the critical role of ultramicropores on the adsorbed CO<sub>2</sub> amount and show that adsorbed CO<sub>2</sub> amount depends on: i) the presence of ultramicropores; ii) narrow micropore volume; and iii) the narrow distribution of narrow micropores through the micropores (Aysu Yurduşen, Yürüm, & Yürüm, 2020b).

## **6.2. Experimental**

Fe-BTCs were repetitively synthesized for five times and characterization analyses were conducted for five times.

### **6.2.1. Materials**

All the chemicals were used as received. 98% pure (ACS Reagent grade) iron(III) chloride hexahydrate (FeCl<sub>3</sub>·6H<sub>2</sub>O) was supplied from Merck Millipore. 95% pure benzene-

1,3,5-tricarboxylic acid, 99.9% pure (HPLC grade) *N,N*-Dimethylformamide (DMF), and 99.8% pure methanol were supplied from Sigma Aldrich.

### **6.2.2. Synthesis of Hierarchically Porous Fe-BTCs**

A perturbation assisted nanofusion mechanism was used to form hierarchical pores. 3.1 mmol of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ , (0.62 mmol, 1 mmol, or 3.1 mmol) benzene-1,3,5-tricarboxylic acid, and 80 mL of DMF was mixed vigorously via a magnetic stirrer with a stirring rate of 800 rpm for an hour at room temperature (298 K). By vigorously stirring metal salt, benzene-1,3,5-tricarboxylic acid, and DMF, the growth of large single crystals was prevented. At the end of stirring, a clear solution was obtained which was then poured into glass vials (20 mL) capped with Teflon caps. Glass vials filled with clear solutions were heated in an isothermal oven at 110, 130, and 150 °C for 2 days. Obtained precipitates and the solutions were transferred into 50 mL falcon tubes. Solvent exchange process was carried out for 6 days (three times with DMF and three times with methanol) and each solvent was changed at the end of 24 hours. At the end of the washing process, samples were dried under vacuum at 100 °C for 30 hours. Table 31 illustrates the sample abbreviations for hierarchically porous Fe-BTCs.

Table 31. Sample abbreviations for hierarchical porous Fe-BTCs

| Sample Abbreviation | Synthesis Temperature (°C) | Fe:BTC ratio |
|---------------------|----------------------------|--------------|
| Fe-BTC-110-1        | 110                        | 1            |
| Fe-BTC-110-3        | 110                        | 3            |
| Fe-BTC-110-5        | 110                        | 5            |
| Fe-BTC-130-1        | 130                        | 1            |
| Fe-BTC-130-3        | 130                        | 3            |
| Fe-BTC-130-5        | 130                        | 5            |
| Fe-BTC-150-1        | 150                        | 1            |
| Fe-BTC-150-3        | 150                        | 3            |
| Fe-BTC-150-5        | 150                        | 5            |

### 6.2.3. Characterization of Hierarchically Porous Fe-BTCs

Characterization analyses were repeated for five times. Characterization analyses were performed by powder x-ray diffraction (PXRD) analysis, scanning electron microscopy (SEM), Brunauer-Emmett-Teller (BET) surface area and pore size distribution analysis, Fourier Transform Infrared Spectroscopy (FT-IR) analysis, and thermogravimetric analysis (TGA). CO<sub>2</sub> uptake capacities were measured at 298 K by an Intelligent Gravimetric Analyzer (IGA).

#### 6.2.3.1. X-ray diffraction

0.15406 nm Cu K $\alpha$  radiation, 40 kV was used as X-ray generator voltage and 5 mA current was used in X-ray diffraction analysis. X-ray diffraction analysis were performed with a step size of 0.02° in between 2 and 90°.



#### **6.2.3.2. Scanning electron microscopy (SEM)**

A Leo Supra 35 VP field emission scanning electron microscope was used in SEM imaging. A working distance of 8 to 9 mm was used, and the voltage was set depending on the Fe-BTC imaged.

#### **6.2.3.3. Brunauer-Emmett-Teller (BET) surface area and pore size distribution analyses**

A Micromeritics 3Flex Instrument were used for BET surface area measurements and pore size distribution analysis. 100 to 150 milligrams (mg) of Fe-BTC weighed for each BET analysis. Fe-BTC were degassed for 6 hours at 120 °C and NLDFT method was used for pore volume estimations. BET surface areas were calculated in between the relative pressure( $P/P_0$ ) range of 0.05 and 0.099.

#### **6.2.3.4. Fourier transform infrared spectroscopy (FTIR) analyses**

Thermo Scientific Nicolet Is10 was used for FTIR analysis. Analyses were conducted with a spectral resolution of 4  $\text{cm}^{-1}$  for the wavelengths ranging between 600 to 4000  $\text{cm}^{-1}$ . Scans were repeated for 32 times and background noise was corrected.

#### **6.2.3.5. Thermogravimetric analysis (TGA)**

Shimadzu DTG-60H simultaneous thermal analysis (TG-DTA) was used in thermogravimetric analysis. Under a continuous flow of  $\text{N}_2$  (20 mL/min) samples were heated from 25 to 1200 °C with a heating rate of 10 K. For each TGA test  $32 \pm 5$  mg of Fe-BTC was used.

## 6.3. Results and Discussion

### 6.3.1. XRD Analysis

XRD patterns of hierarchically porous Fe-BTCs are illustrated at Figure 105. Poor crystallinity observed in the XRD patterns is a consequence of the semiamorphous nature of Fe-BTC.

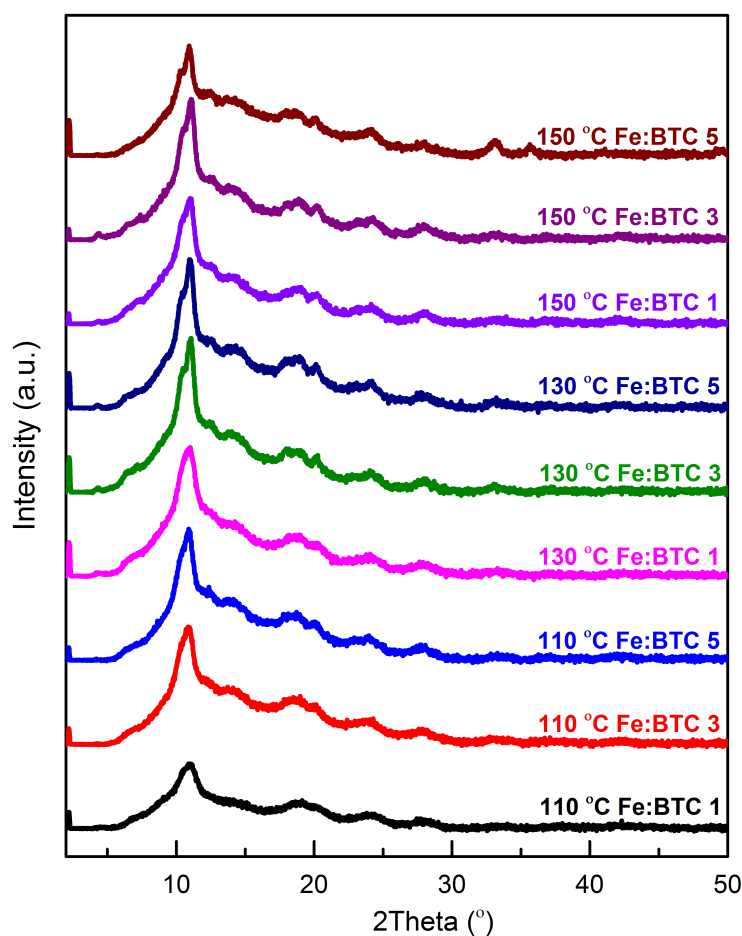


Figure 105. XRD patterns of hierarchically porous Fe-BTCs.

Similarities in Bragg peak positions and similar Bragg peak intensities reveal that Fe-BTC was synthesized successfully by the perturbation assisted nanofusion synthesis strategy.

XRD patterns consist broad bands with relatively weak intensities which illustrates the disordered nature of Fe-BTC. Additionally, synthesizing Fe-BTC via a perturbation

assisted nanofusion synthesis strategy caused nanosized MOF crystallites to be embedded in an amorphous matrix which caused broadening in bands (Cao et al., 2016).

XRD patterns of Fe-BTC type crystallites agree well with each other having Bragg reflections located at the same peak positions. XRD patterns comparing the peak positions of Fe-BTC synthesized at 110, 130, and 150 °C can be found in Supplementary Information. Moreover, it was proved by single crystal X-ray crystallography analyses that micro-sized single crystals were not formed and there were no metallic-iron present.

### 6.3.2. SEM Images

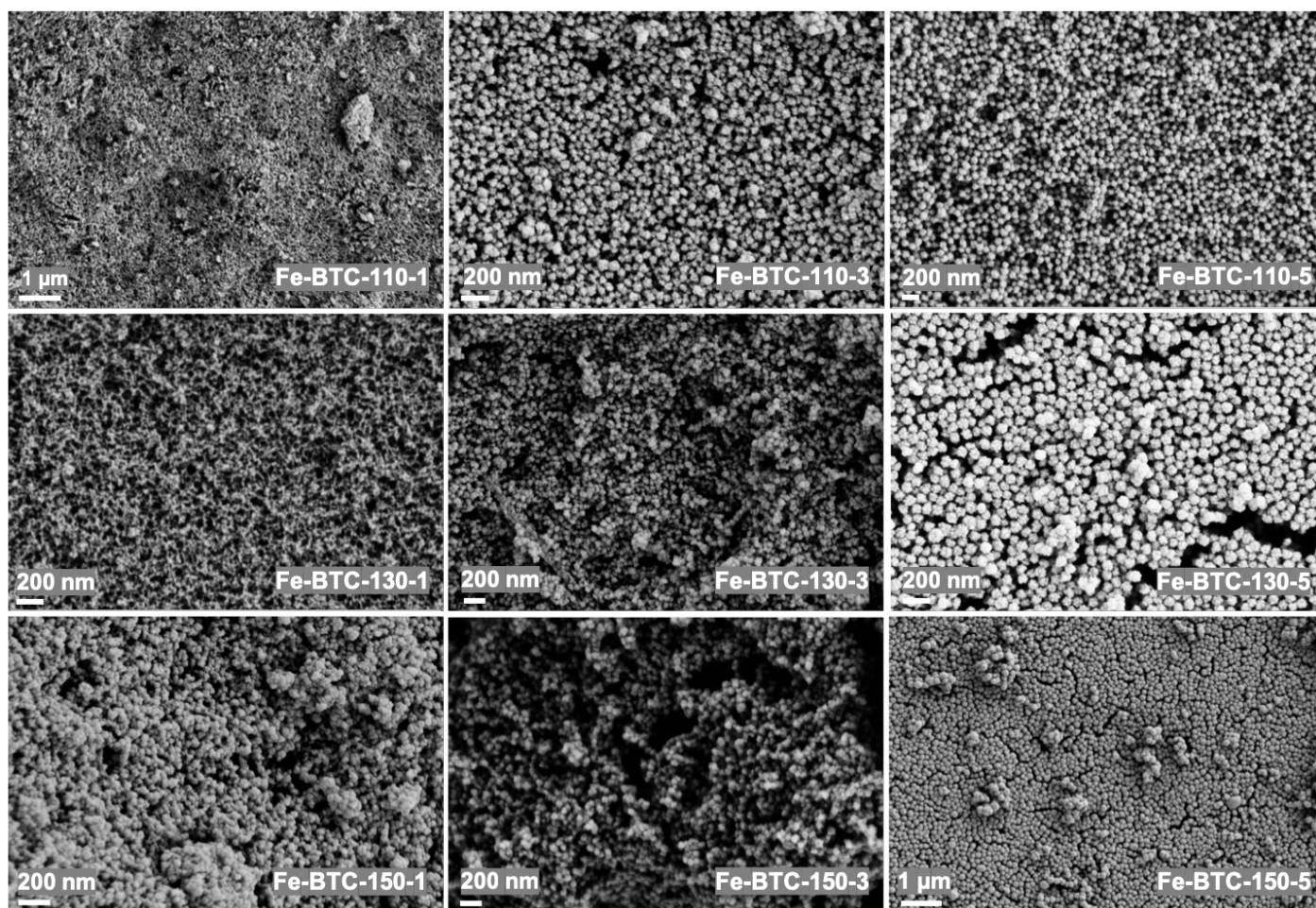


Figure 106. SEM images of hierarchically porous Fe-BTCs.

Figure 106 shows the SEM images hierarchically porous Fe-BTCs. SEM images illustrates the highly porous nature of Fe-BTC. Synthesizing Fe-BTC with a perturbation assisted nanofusion synthesis strategy resulted SBUs (secondary building units) to aggregate into nanosized Fe-BTC crystals which were embedded in an amorphous matrix. The aggregated SBUs, nanosized Fe-BTC crystals and the interconnected porous network can be visibly seen in the SEM images (Figure 106).

### 6.3.3. N<sub>2</sub> Sorption Isotherms

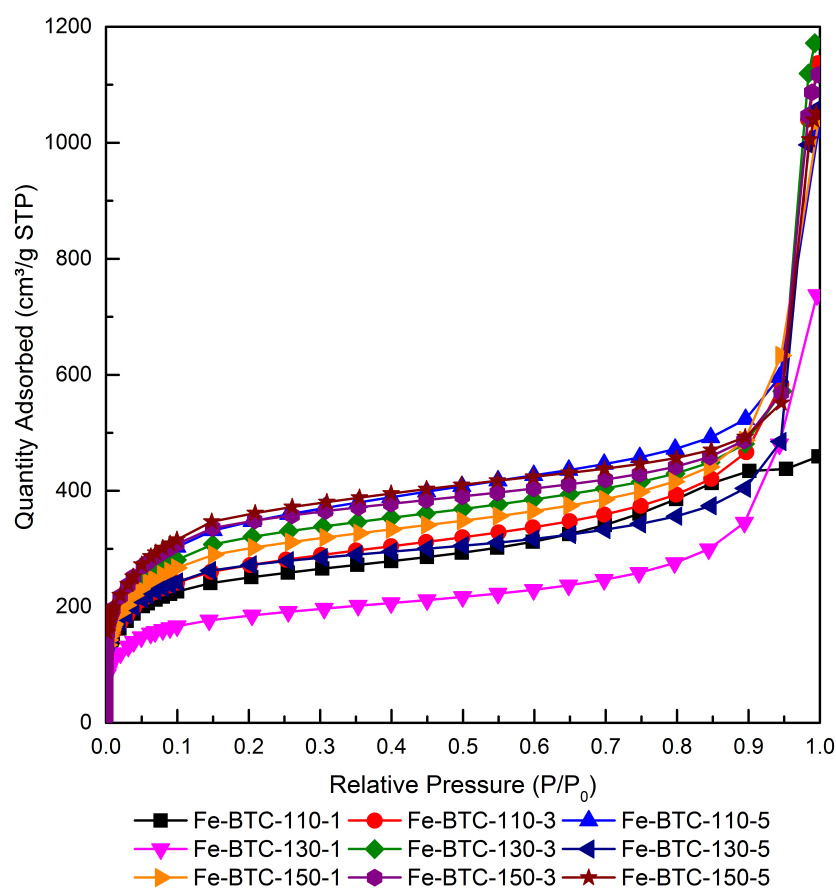


Figure 107. N<sub>2</sub> sorption isotherms of hierarchically porous Fe-BTCs.

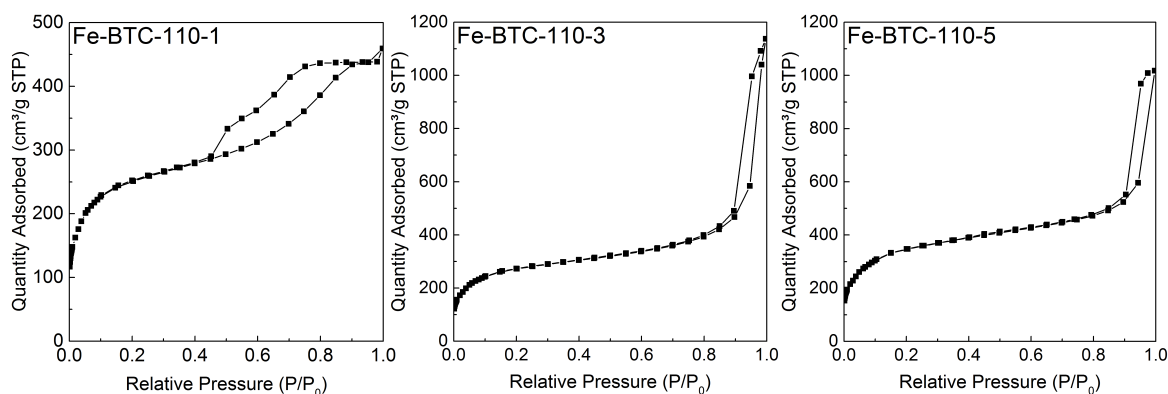


Figure 108. N<sub>2</sub> sorption isotherms of Fe-BTC-110-1, Fe-BTC-110-3, and Fe-BTC-110-5.

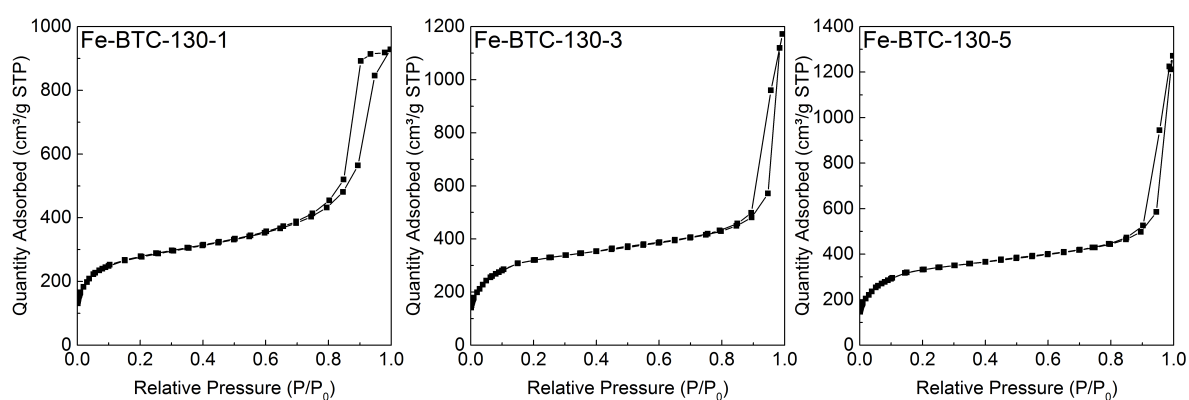


Figure 109. N<sub>2</sub> sorption isotherms of Fe-BTC-130-1, Fe-BTC-130-3, and Fe-BTC-130-5.

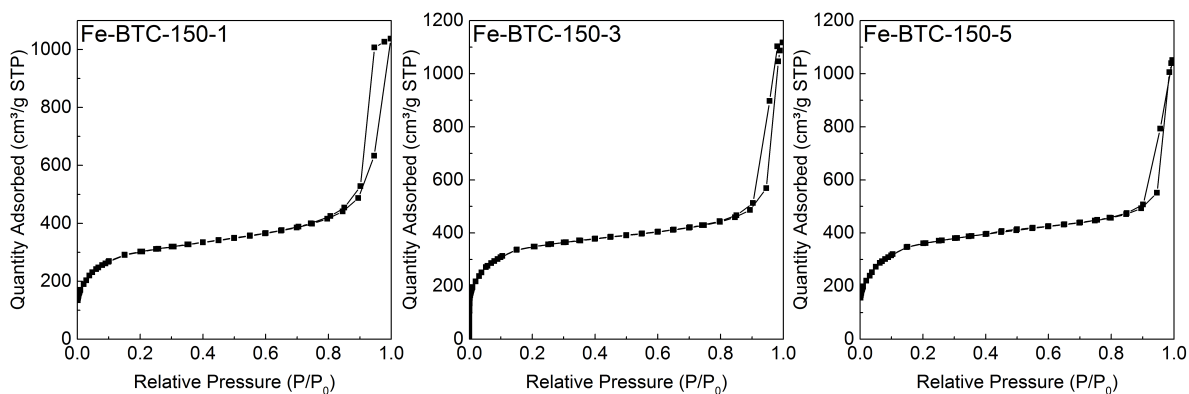


Figure 110. N<sub>2</sub> sorption isotherms of Fe-BTC-150-1, Fe-BTC-150-3, and Fe-BTC-150-5.

Figure 107-110 illustrate N<sub>2</sub> sorption isotherms hierarchically porous Fe-BTCs. N<sub>2</sub> sorption isotherms followed typical IUPAC type IV isotherms with some microporosity present. At low pressures ( $P/P_0 < 0.1$ ), high N<sub>2</sub> uptakes are observed. These high N<sub>2</sub> uptakes are attributed to micropores present in the pore structure. In between relative pressures of 0.2 and 0.9, a true horizontal plateau cannot be achieved, and the observed slope is associated

with mesopore filling. At pressures close to saturation pressure ( $0.9 < P/P_0 < 1$ ), the amount of  $N_2$  adsorbed increased drastically which illustrates that pores with pore diameters at the upper mesopore size range is present.

### 6.3.4. Pore Size Distribution Analysis

#### 6.3.4.1. t-plot method

t-plots of Fe-BTCs can be found below at Figure 111. t-plots show the amount of  $N_2$  adsorbed at standard temperature and pressure with respect to statistical thickness (Lowell et al., 2004a).

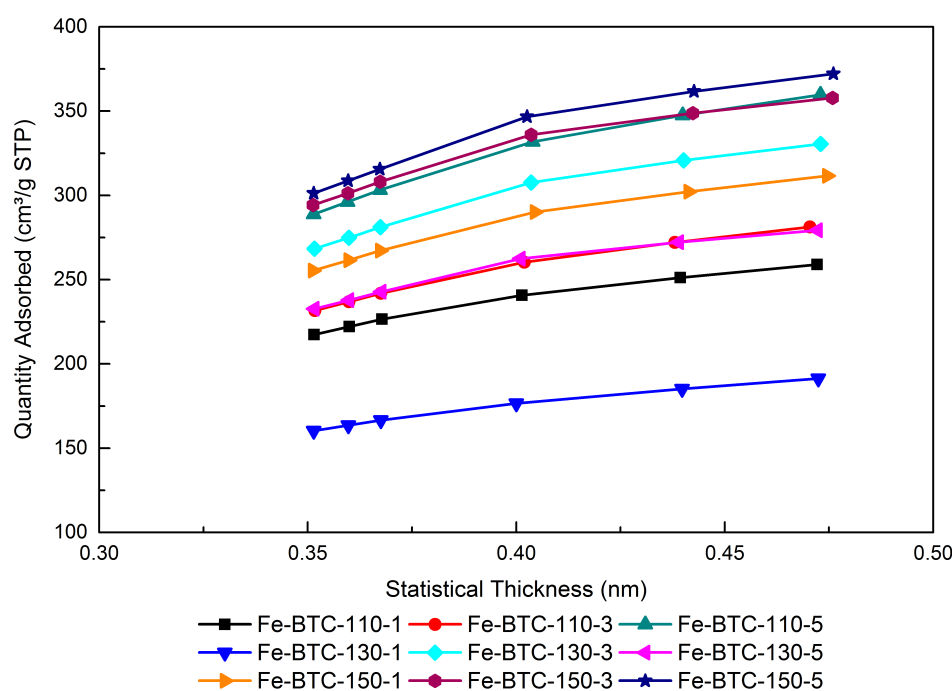


Figure 111. t-plots of hierarchically porous Fe-BTCs.

t-plots show deviations from the straight line. Deviations are towards downwards and t-plots held positive intercepts which suggest the presence of micropores (Lowell et al., 2004a). The highest micropore volume ( $0.181 \text{ cm}^3/\text{g}$ ) belongs to Fe-BTC-150-3 while the lowest micropore volume belongs to Fe-BTC-130-1 ( $0.112 \text{ cm}^3/\text{g}$ ). Respective micropore

volumes, micro- and mesopore areas estimated by t-plot method can be found below at Table 32.

Table 32. Micro- and mesopore area ( $\text{m}^2/\text{g}$ ), micropore volume of Fe-BTC type crystallites estimated by t-plot method.

| Hierarchically porous Fe-BTCs | S <sub>micro</sub> ( $\text{m}^2/\text{g}$ ) | S <sub>meso</sub> ( $\text{m}^2/\text{g}$ ) | S <sub>micro</sub> (%) | V <sub>micro</sub> ( $\text{cm}^3/\text{g}$ ) |
|-------------------------------|----------------------------------------------|---------------------------------------------|------------------------|-----------------------------------------------|
| Fe-BTC-110-1                  | 419.4 $\pm$ 3.2E1                            | 531 $\pm$ 1.2E2                             | 44.9                   | 0.154 $\pm$ 1.6E-2                            |
| Fe-BTC-110-3                  | 374.1 $\pm$ 3.7E1                            | 650 $\pm$ 1.8E2                             | 36.5                   | 0.135 $\pm$ 1.0E-2                            |
| Fe-BTC-110-5                  | 388.8 $\pm$ 8.9E1                            | 913.8 $\pm$ 1.6E2                           | 29.8                   | 0.133 $\pm$ 4.0E-2                            |
| Fe-BTC-130-1                  | 298.2 $\pm$ 7.1E1                            | 394.7 $\pm$ 1.9E2                           | 43.1                   | 0.112 $\pm$ 2.5E-2                            |
| Fe-BTC-130-3                  | 400.7 $\pm$ 6.0E1                            | 806.4                                       | 33.2                   | 0.139 $\pm$ 2.3E-2                            |
| Fe-BTC-130-5                  | 418.9 $\pm$ 4.4E1                            | 605.7 $\pm$ 1.2E2                           | 40.8                   | 0.146 $\pm$ 1.6E-2                            |
| Fe-BTC-150-1                  | 425.5 $\pm$ 5.3E1                            | 713.6 $\pm$ 7.4E1                           | 37.4                   | 0.151 $\pm$ 2.6-2                             |
| Fe-BTC-150-3                  | 509.6 $\pm$ 6.0E-1                           | 803.2 $\pm$ 1.2E1                           | 38.8                   | 0.181                                         |
| Fe-BTC-150-5                  | 458.7 $\pm$ 1.5E2                            | 897.2 $\pm$ 7.7                             | 33.8                   | 0.159 $\pm$ 7.8E-2                            |

#### 6.3.4.2.NLDFT method

Figure 112 represents the NLDFT plots of Fe-BTC type crystallites.

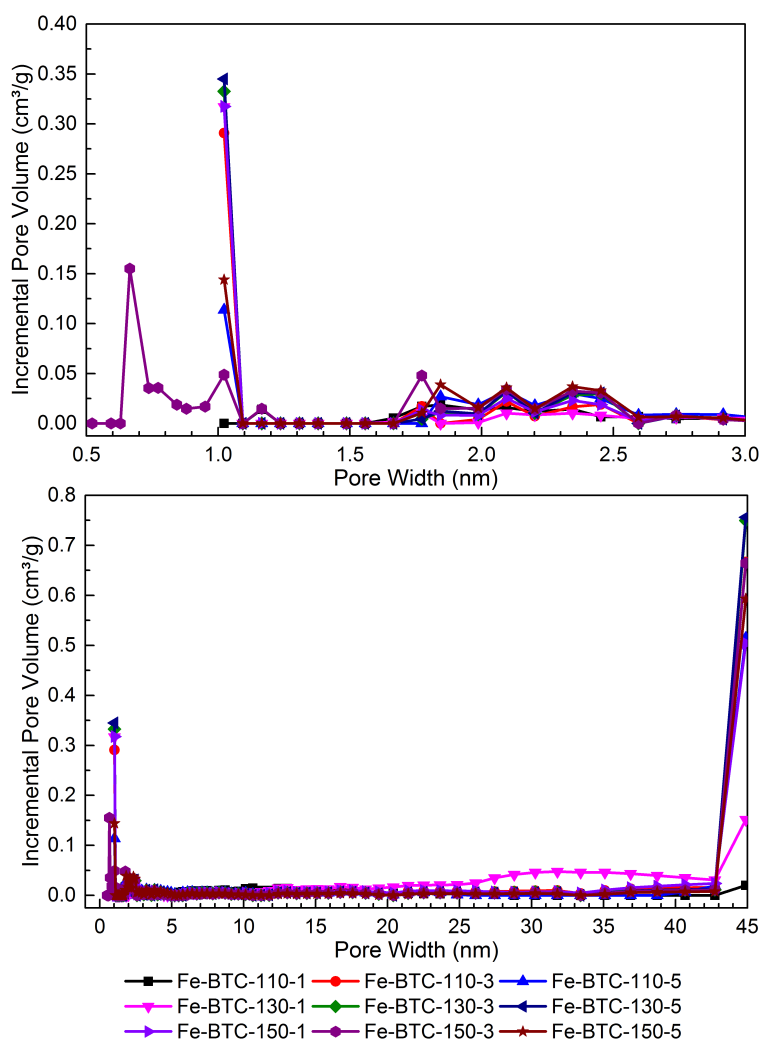


Figure 112. NLDFT plots of Fe-BTC type crystallites.

NLDFT plots (Figure 112) illustrate the different pore size distributions of Fe:BTCs. Remarkably, it is Fe-BTC-150-3 that has ultramicropores in its pore structure while the others have contributions from pores with pore diameters greater than 1 nm. Table 33 summarizes the pore volumes of narrow micropores, micropores, upper mesopores and mesopores, total pore volumes estimated by NLDFT method.



Table 33. Volume of pores smaller than 1 nm, micro-, uppermeso-, mesopore and total pore volume, and fraction of micropores of Fe-BTCs estimated by NLDFT method.

|              | Vpores <1 nm<br>(cm <sup>3</sup> /g) | Vmicro<br>(cm <sup>3</sup> /g) | Vuppermeso<br>(cm <sup>3</sup> /g) | Vmeso<br>(cm <sup>3</sup> /g) | Vtotal<br>(cm <sup>3</sup> /g) | Vmicro<br>(%) |
|--------------|--------------------------------------|--------------------------------|------------------------------------|-------------------------------|--------------------------------|---------------|
| Fe-BTC-110-1 | 0.265±0.019                          | 0.350±0.019                    | 0.020±0.005                        | 0.367±0.043                   | 0.717±0.053                    | 48.8          |
| Fe-BTC-110-3 | 0.291±0.063                          | 0.334±0.075                    | 0.667±0.135                        | 1.056±0.102                   | 1.390±0.051                    | 24.0          |
| Fe-BTC-110-5 | 0.365±0.033                          | 0.444±0.052                    | 0.510±0.062                        | 0.856±0.071                   | 1.300±0.110                    | 34.2          |
| Fe-BTC-130-1 | 0.198±0.074                          | 0.234±0.077                    | 0.332±0.093                        | 0.725±0.204                   | 0.959±0.281                    | 23.9          |
| Fe-BTC-130-3 | 0.333±0.007                          | 0.389±0.038                    | 0.750±0.125                        | 1.065±0.159                   | 1.454±0.121                    | 26.8          |
| Fe-BTC-130-5 | 0.292±0.027                          | 0.348±0.050                    | 0.698±0.074                        | 0.942±0.099                   | 1.289±0.100                    | 26.9          |
| Fe-BTC-150-1 | 0.318±0.008                          | 0.373±0.008                    | 0.504±0.087                        | 0.917±0.065                   | 1.290±0.064                    | 28.9          |
| Fe-BTC-150-3 | 0.326±0.004                          | 0.453±0.006                    | 0.664±0.044                        | 0.957±0.063                   | 1.410±0.057                    | 32.1          |
| Fe-BTC-150-5 | 0.367±0.015                          | 0.468±0.030                    | 0.590±0.280                        | 0.872±0.287                   | 1.340±0.257                    | 34.9          |

It is observed that volume of narrow micropores, micropores, upper mesopores, and mesopores differ with synthesis temperature and Fe:BTC ratio. It is notable that, Fe-BTC-110-1 possesses a relatively lower mesopore volume (0.0201±0.005 cm<sup>3</sup>/g) than Fe-BTC-110-3, and Fe-BTC-110-5. Mesopore volume of Fe-BTC-110-1 is 2.88 and 2.33 times lower than the mesopore volumes of Fe-BTC-110-3, and Fe-BTC-110-5, respectively and the total pore volume of Fe-BTC-110-1 is 1.94 and 1.8 times lower than the total pore volume of Fe-BTC-110-3, and Fe-BTC-110-5, respectively. These differences observed in pore size distribution reveal that textural porosity differ with synthesis temperature and Fe:BTC ratio. Within the synthesized Fe-BTCs, the highest micropore volume belongs to Fe-BTC-150-5 (0.468±0.0296 cm<sup>3</sup>/g) and the highest total pore volume (1.45±0.12 cm<sup>3</sup>/g) belongs to Fe-

BTC-130-3. Remarkably, it is Fe-BTC-150-3 that possess ultramicropores ( $0.19 \text{ cm}^3/\text{g}$ ) in its pore size distribution while none of the Fe-BTCs synthesized in this study possess ultramicropores.

#### 6.3.4.3. FTIR analysis

FTIR spectra of hierarchically porous Fe-BTCs can be found below in Figure 113-117.

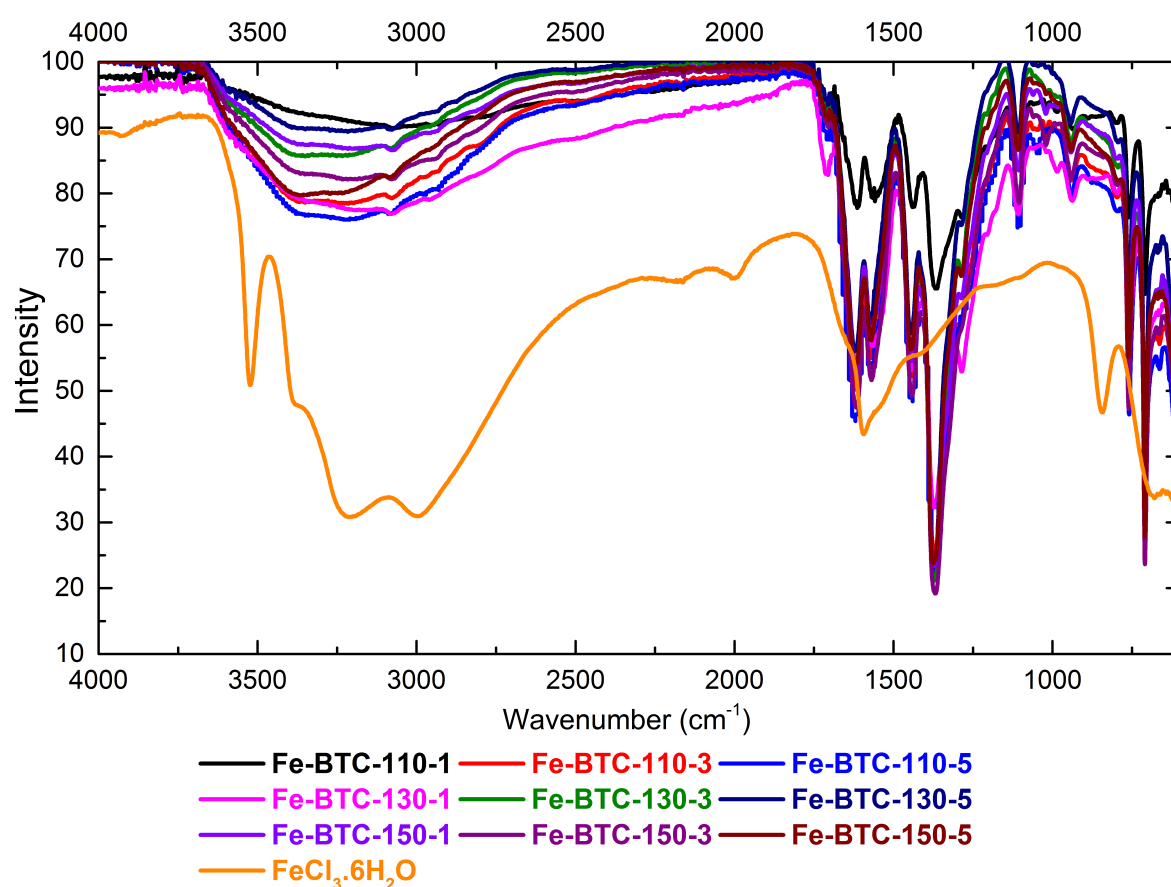


Figure 113. FTIR spectra of hierarchically porous Fe-BTCs and  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ .

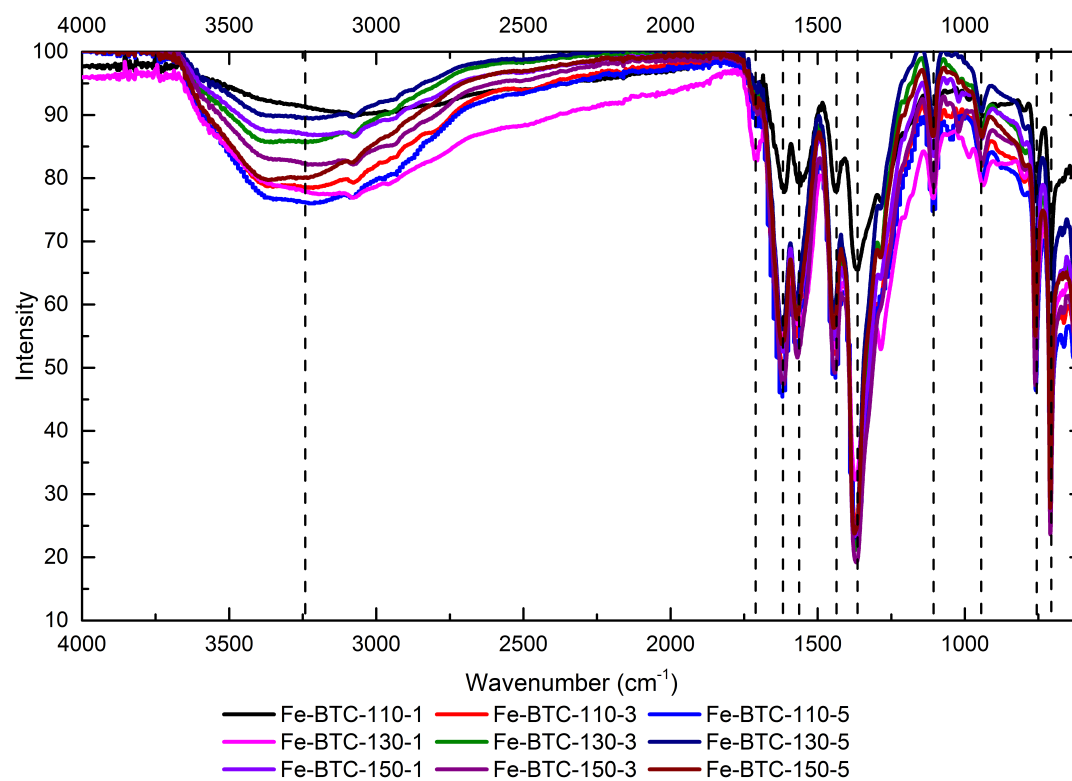


Figure 114. FTIR spectra of hierarchically porous Fe-BTCs.

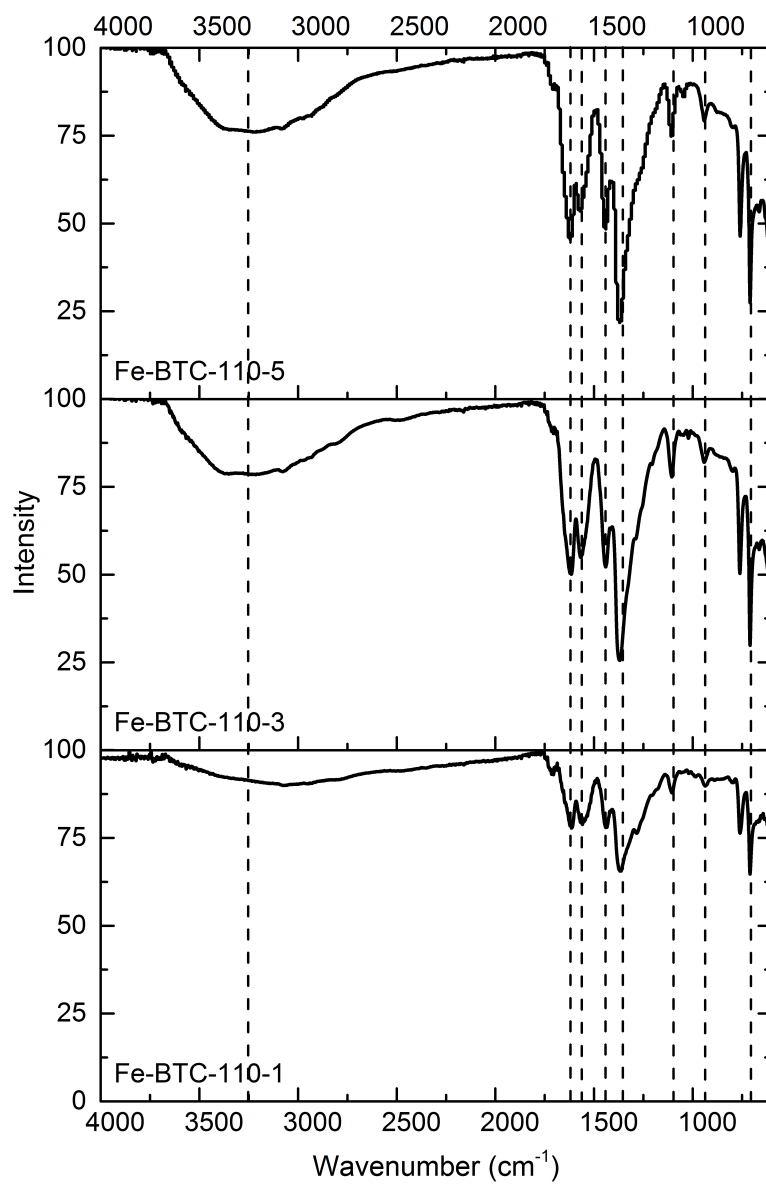


Figure 115. FTIR spectra of Fe-BTC-110-1, Fe-BTC-110-3, and Fe-BTC-110-5.

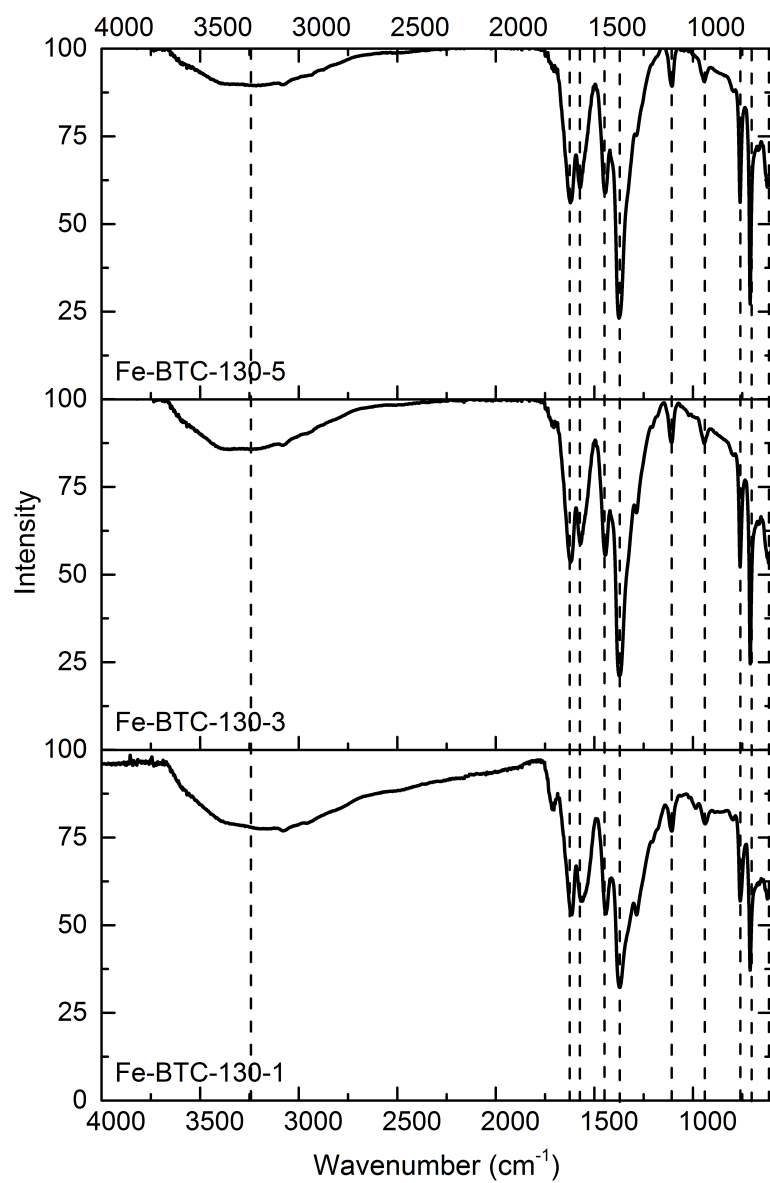


Figure 116. FTIR spectra of Fe-BTC-130-1, Fe-BTC-130-3, and Fe-BTC-130-5.

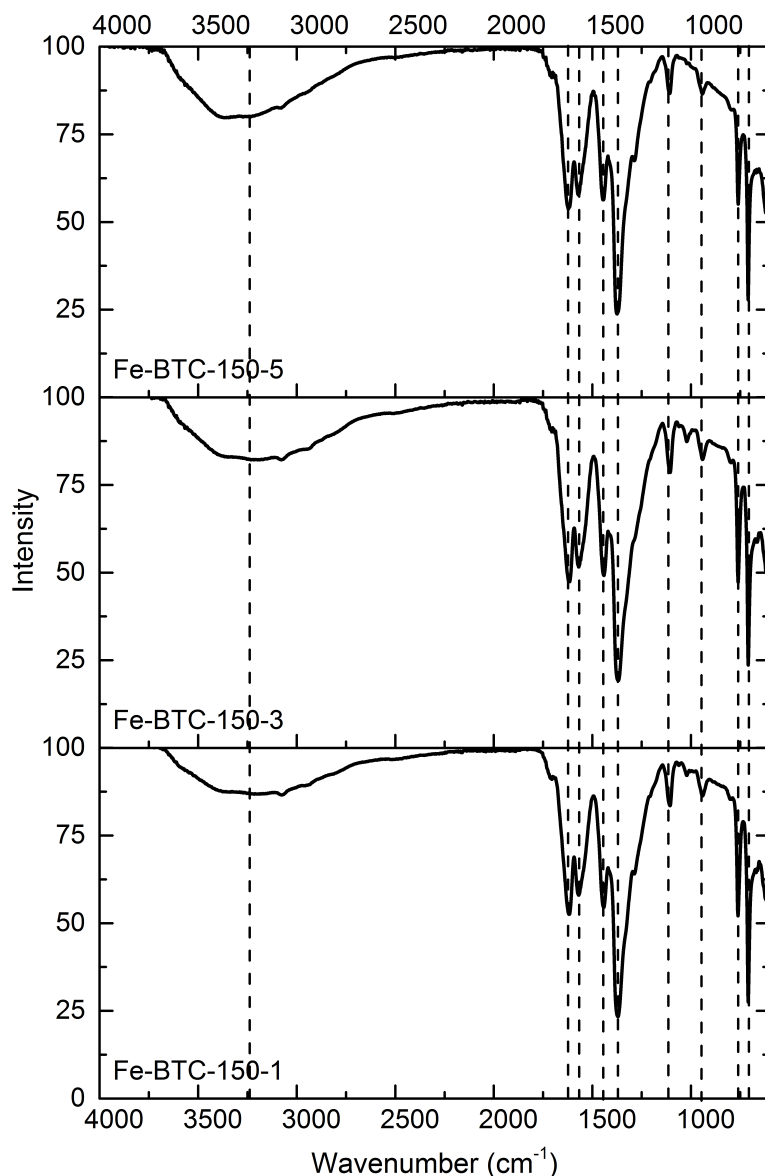


Figure 117. FTIR spectra of Fe-BTC-150-1, Fe-BTC-150-3, and Fe-BTC-150-5.

FTIR spectra of the hierarchically porous Fe-BTCs synthesized in this study, agree well with the FTIR spectra of the reported Fe-BTCs (Basolite F300) (Dhakshinamoorthy, Alvaro, Horcajada, et al., 2012; X. Hu et al., 2016; Oveisi, Khorramabadi-Zad, & Daliran, 2016). Fe-BTCs show broad bands in between 3000 and 3400  $\text{cm}^{-1}$ . Observed broad bands are assigned to OH groups that are hydrogen-bonded water molecules which are adsorbed during FTIR analysis conducted under air environment. The broadened OH bands demonstrate the increase in the number of adsorbed water molecules at the open metal sites which is due to the increased number of unsaturated metal sites. Presence of the peaks at

1370, 1441, 1569, and 1621  $\text{cm}^{-1}$  prove that  $-\text{COOFe}$  metallic esters are present in the synthesized Fe-BTC structure and BTC is successfully attached to Fe. The peaks at 1569 and 1621  $\text{cm}^{-1}$  are assigned to bending modes of molecular water which reveals that Fe sites are coordinated with water. A remarkable shift to lower frequencies (1369 and 1440  $\text{cm}^{-1}$ ) occurred in the characteristic peaks (1375 and 1450  $\text{cm}^{-1}$ ) of carboxylate symmetric stretching mode. This remarkable shift is attributed to elongated bonds. The peaks at 941 and 1105  $\text{cm}^{-1}$  are assigned to C-H in-plane and out-of-plane bending modes. The peaks at 709 and 760  $\text{cm}^{-1}$  are assigned to C-C ring out-of-plane bending mode and characteristic of Fe-BTC structure. Lastly, the peak at 612  $\text{cm}^{-1}$  is assigned to central oxygen in single  $\text{Fe}_3\text{O}$ .

Lastly, FTIR spectrum of hierarchically porous Fe-BTCs were compared with the FTIR spectra of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ . None of the peaks observed in the FTIR spectra of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$  (842  $\text{cm}^{-1}$ , 1594  $\text{cm}^{-1}$ , 2993  $\text{cm}^{-1}$ , 3212  $\text{cm}^{-1}$ , and 3523  $\text{cm}^{-1}$ ) were observed in the FTIR spectrum of hierarchically porous Fe-BTCs which proves that there are no metallic iron present.

#### 6.3.4.4.TGA

TGA curves of Fe-BTCs are presented below at Figure 118-127 and Table 34-36 show the percentage of mass loss during TGA.

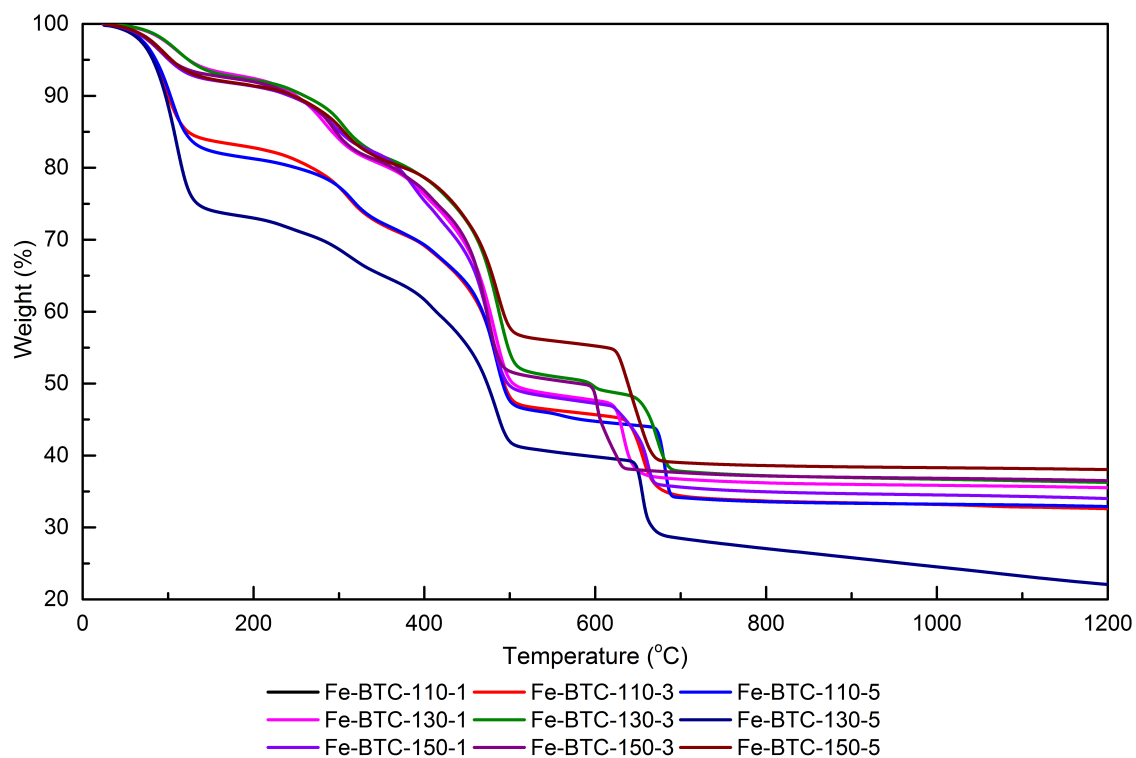


Figure 118. TGA curves of Fe-BTCs.

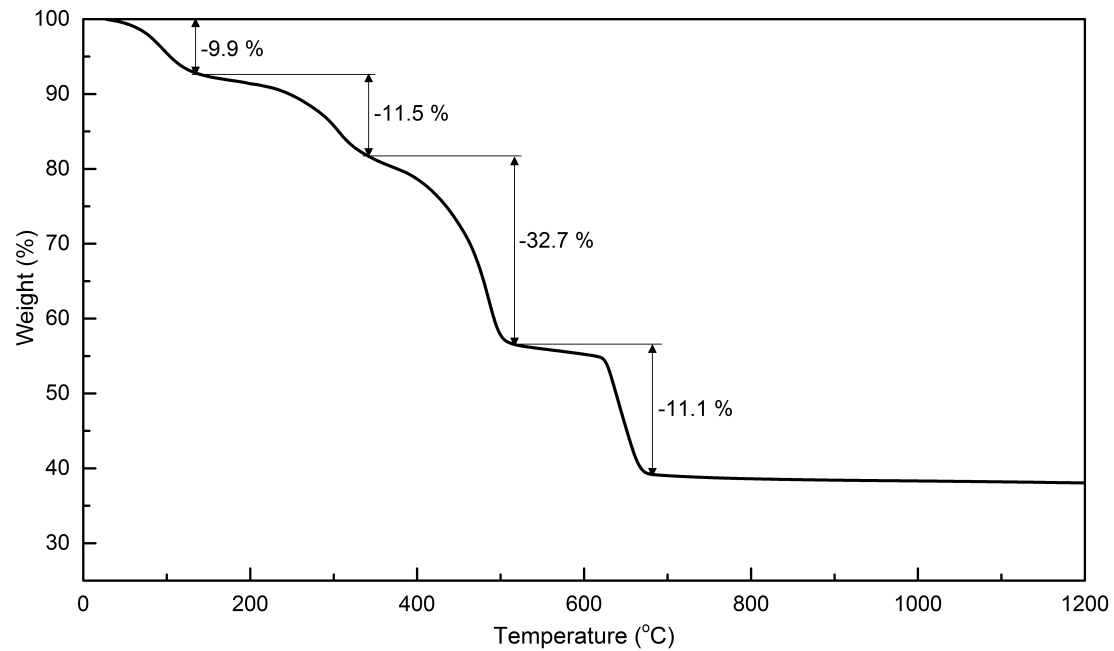


Figure 119. TGA curve of Fe-BTC-110-1.



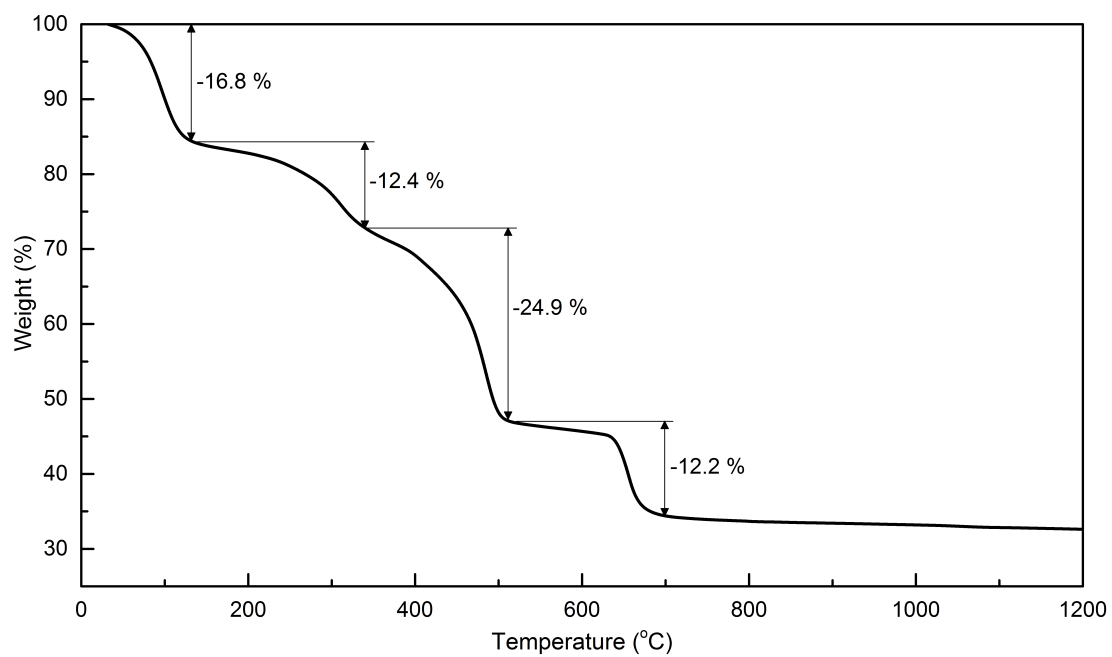


Figure 120. TGA curve of Fe-BTC-110-3.

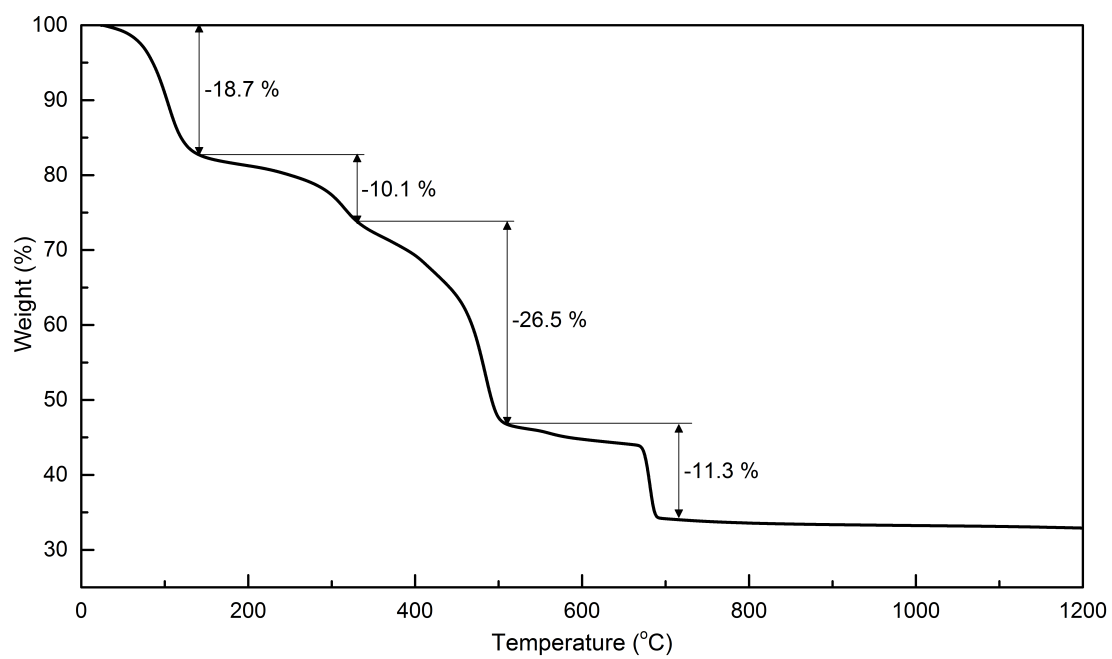


Figure 121. TGA curve of Fe-BTC-110-5.

Table 34. % mass loss during TGA of hierarchically porous Fe-BTCs synthesized at 110 °C.

| Temperature Range (°C) | Fe-BTC-110-1 (%) | Temperature Range (°C) | Fe-BTC-110-3 (%) | Temperature Range (°C) | Fe-BTC-110-5 (%) |
|------------------------|------------------|------------------------|------------------|------------------------|------------------|
| 25-189                 | -9.9             | 25-178                 | -16.8            | 25-195                 | -18.7            |
| 189-342                | -11.5            | 178-373                | -12.4            | 195-371                | -10.1            |
| 342-570                | -32.7            | 373-577                | -24.9            | 371-599                | -26.5            |
| 570-717                | -11.1            | 577-781                | -12.2            | 599-829                | -11.3            |

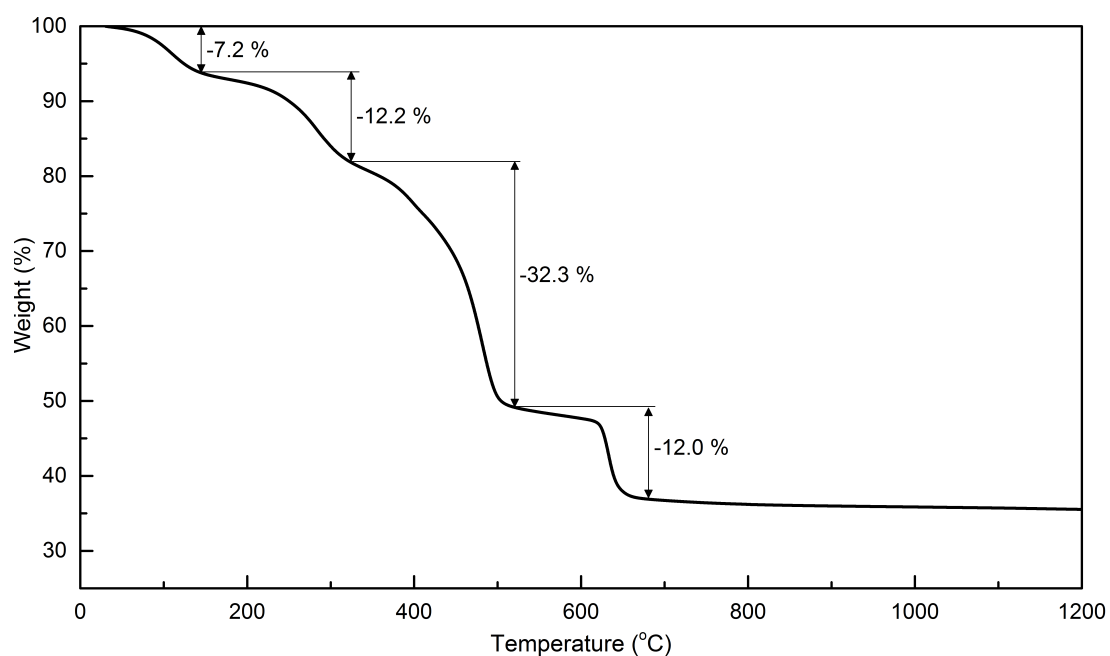


Figure 122. TGA curve of Fe-BTC-130-1.

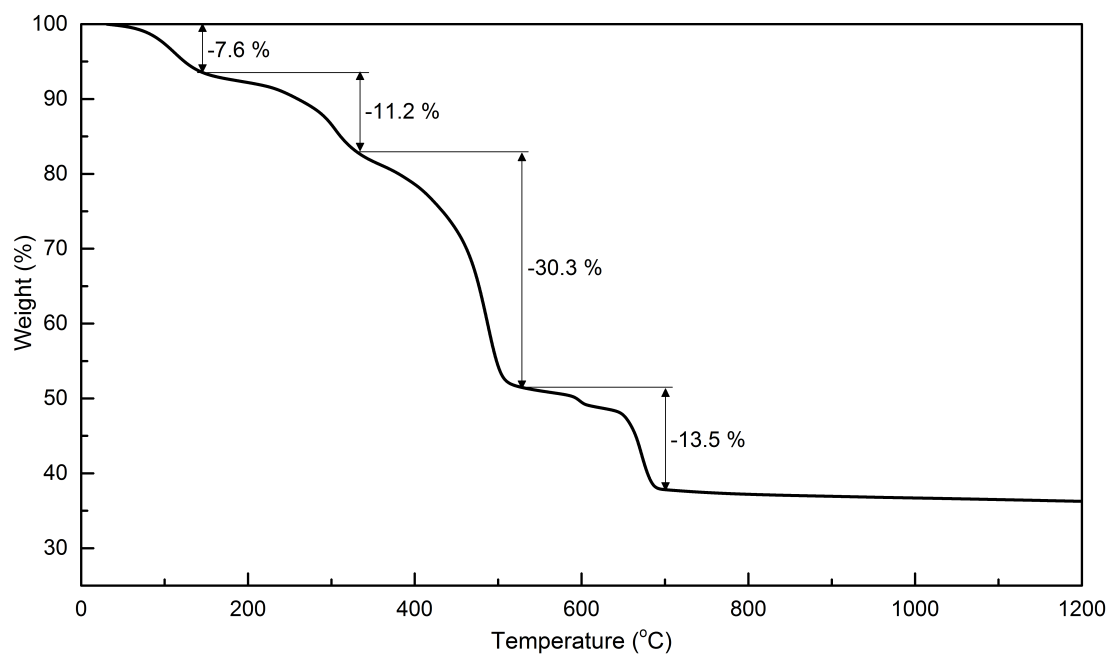


Figure 123. TGA curve of Fe-BTC-130-3.

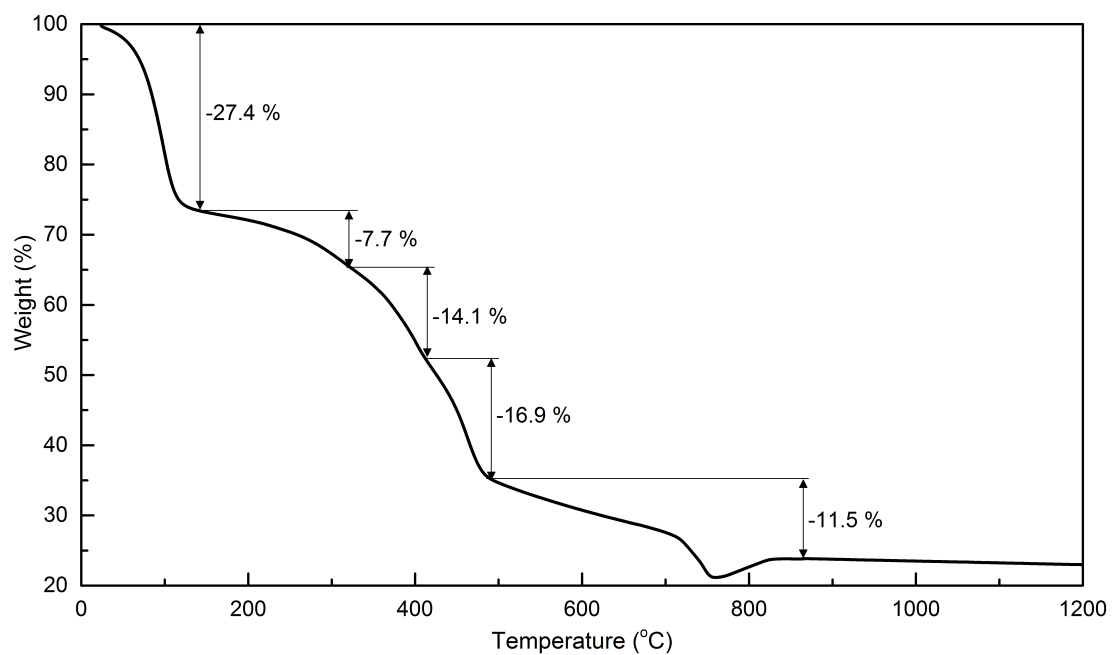


Figure 124. TGA curve of Fe-BTC-130-5.

Table 35. % mass loss during TGA analysis of hierarchically porous Fe-BTCs synthesized at 130 °C.

| Temperature Range (°C) | Fe-BTC-130-1 (%) | Temperature Range (°C) | Fe-BTC-130-3 (%) | Temperature Range (°C) | Fe-BTC-130-5 (%) |
|------------------------|------------------|------------------------|------------------|------------------------|------------------|
| 25-182                 | -7.2             | 25-191                 | -7.6             | 25-177                 | -27.4            |
| 182-347                | -12.2            | 191-359                | -11.2            | 177-327                | -7.7             |
| 347-564                | -32.3            | 359-554                | -30.3            | 327-421                | -14.1            |
| 564-781                | -12.0            | 554-623                | -13.5            | 421-515                | -16.9            |
|                        |                  |                        |                  | 515-796                | -11.5            |

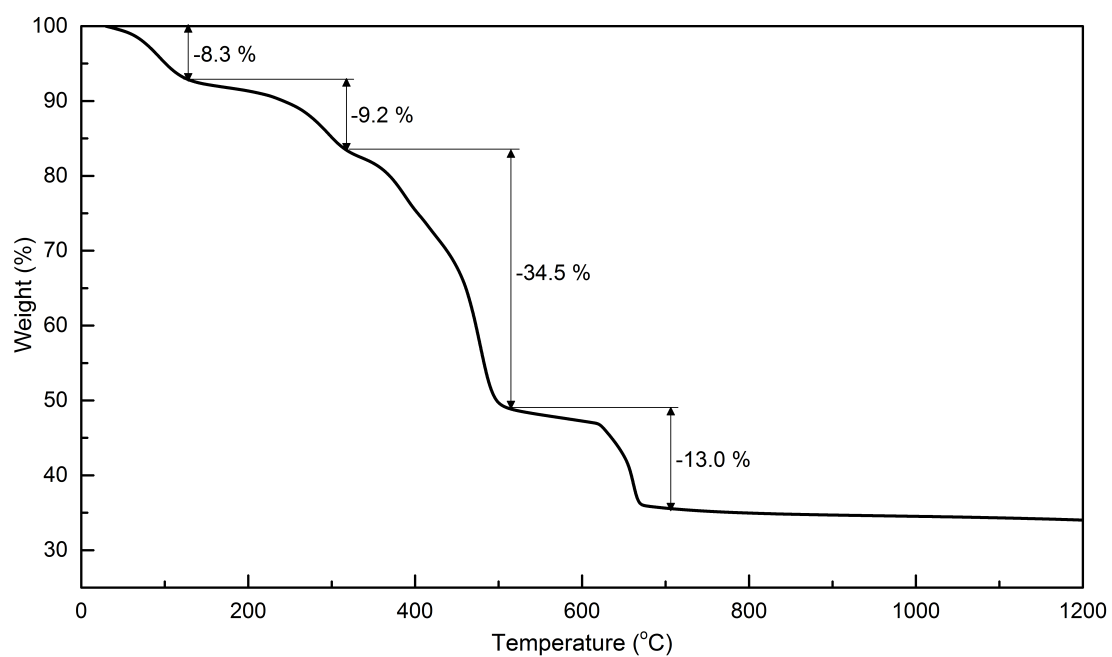


Figure 125. TGA curve of Fe-BTC-150-1.

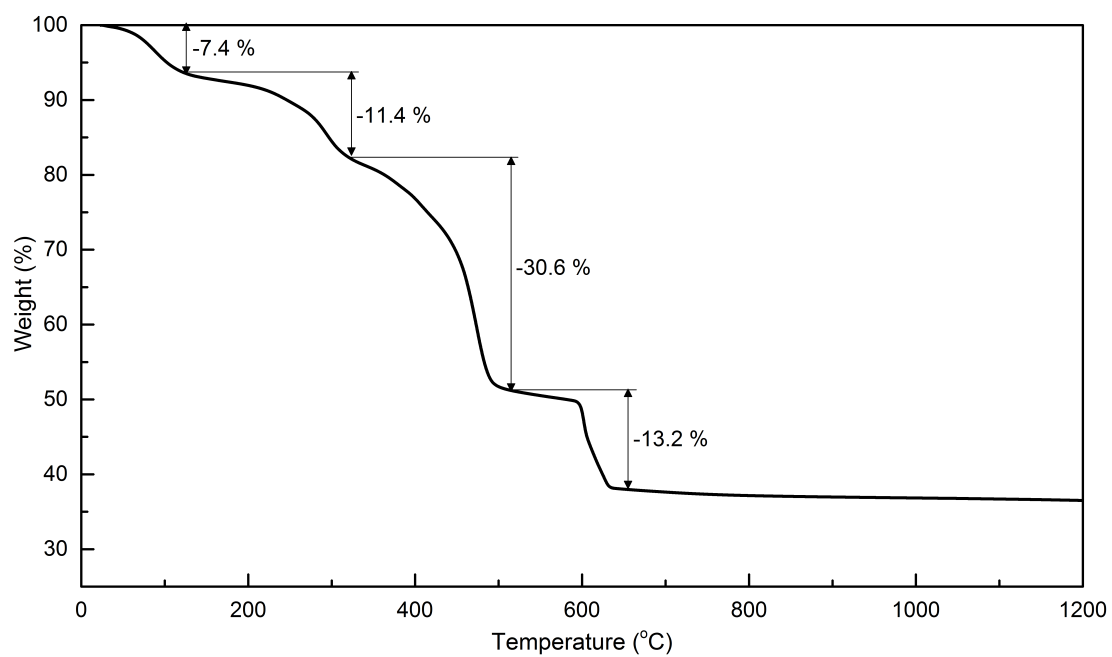


Figure 126. TGA curve of Fe-BTC-150-3.

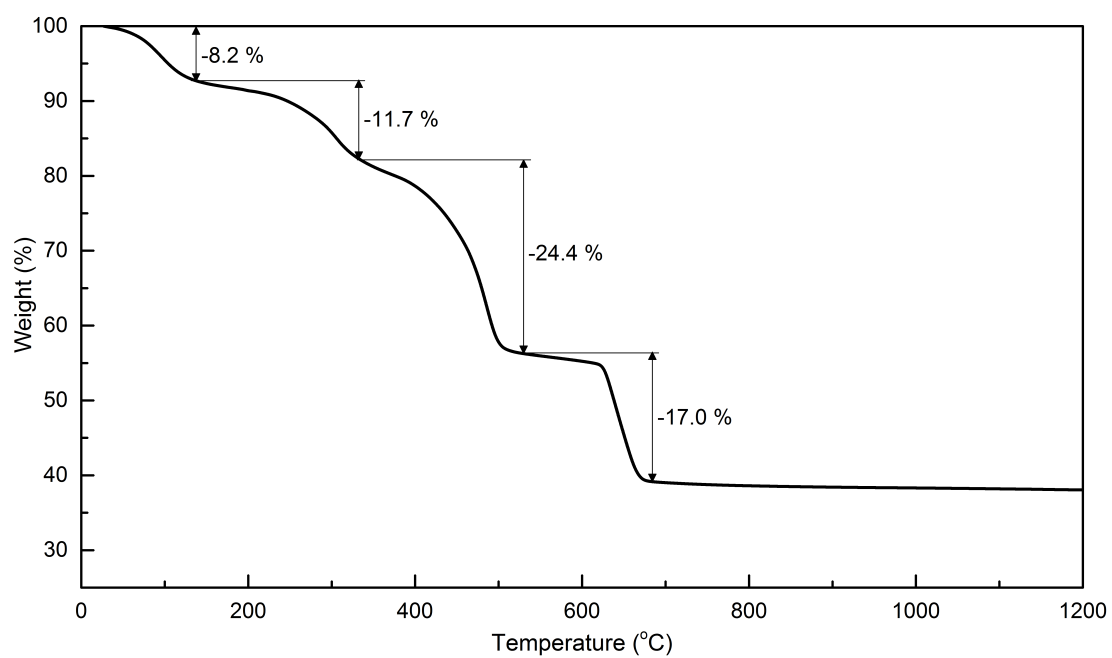


Figure 127. TGA curve of Fe-BTC-150-5.

Table 36. % mass loss during TGA analysis of hierarchically porous Fe-BTCs synthesized at 150 °C.

| Temperature Range (°C) | Fe-BTC-150-1 (%) | Temperature Range (°C) | Fe-BTC-150-3 (%) | Temperature Range (°C) | Fe-BTC-150-5 (%) |
|------------------------|------------------|------------------------|------------------|------------------------|------------------|
| 25-179                 | -8.3             | 25-168                 | -7.4             | 25-178                 | -8.2             |
| 179-334                | -9.2             | 168-342                | -11.4            | 178-374                | -11.7            |
| 334-556                | -34.5            | 342-547                | -30.6            | 374-570                | -24.4            |
| 556-776                | -13.0            | 547-754                | -13.2            | 570-766                | -17.0            |

Four major losses are issued. The first mass loss occurred in between 25 and 190 °C which is a consequence of the removal of adsorbed and coordinated water molecules. The second step (168-374 °C) is attributed to the loss of solvent molecules trapped in the pores. The third step illustrates the temperature at which BTC decomposes and structure collapse starts which thereby determines the stability of the synthesized Fe-BTC. Decomposition temperature of Fe-BTC varies with the synthesis conditions. The highest thermal stability is achieved by Fe-BTC-150-5 which decomposes at 374 °C while Fe-BTC-130-5 decomposes at a relatively lower temperature, 327 °C. By the perturbation assisted nanofusion synthesis strategy, an Fe-BTC that has higher thermal stability than those of reported Fe-BTCs and Basolite F300 is synthesized (X. Hu et al., 2016; Majano, Ingold, Yulikov, Jeschke, & Pérez-Ramírez, 2013). TGA analysis demonstrates that hierarchically porous MIL-88Bs are thermally stable under adsorption process conditions. Percentage of mass remains at the end of TGA can be found in Table 37.

Table 37. Percent residual mass at the end of TGA.

| Residual Mass (%) | 110 °C | 130 °C | 150 °C |
|-------------------|--------|--------|--------|
| Fe:BTC 1          | 34.7   | 36.3   | 35     |
| Fe:BTC 3          | 33.7   | 37.4   | 37.4   |
| Fe:BTC 5          | 33.6   | 22.4   | 38.7   |

### 6.3.5. CO<sub>2</sub> Adsorption Studies

Hierarchically porous Fe-BTCs are investigated for their CO<sub>2</sub> uptake capacities. Different CO<sub>2</sub> uptake capacities are obtained for hierarchically porous Fe-BTCs. These differences in CO<sub>2</sub> uptake capacities are attributed to the different pore size distribution of hierarchically porous Fe-BTCs. Langmuir and Freundlich isotherm models are investigated for the best fit. The calculated Langmuir and Freundlich isotherm parameters, respective equations, and R<sup>2</sup> values can be found below.

#### Langmuir Model:

$$\frac{C_e}{q_e} = \frac{1}{KQ^0} + \frac{C_e}{Q^0} \quad (6.1)$$

#### Freundlich Model:

$$\log q_e = \log K_F + \frac{1}{n} \log C_e \quad (6.2)$$

Table 38. Respective equations obtained from models

| Hierarchically porous Fe-BTCs | Langmuir Model                           | Freundlich Model                         |
|-------------------------------|------------------------------------------|------------------------------------------|
| Fe-BTC-110-1                  | $y = 0.1686x + 669.57$<br>$R^2 = 0.9791$ | $y = 0.639x - 1.8419$<br>$R^2 = 0.9969$  |
| Fe-BTC-110-3                  | $y = 0.0821x + 796.06$<br>$R^2 = 0.9944$ | $y = 0.7741x - 2.2584$<br>$R^2 = 0.9952$ |
| Fe-BTC-110-5                  | $y = 0.0828x + 719.25$<br>$R^2 = 0.9876$ | $y = 0.7741x - 2.2584$<br>$R^2 = 0.9952$ |

Table 39. Langmuir and Freundlich isotherm parameters

| Hierarchically porous Fe-BTCs | Langmuir Model                                                                      | Freundlich Model                                                          |
|-------------------------------|-------------------------------------------------------------------------------------|---------------------------------------------------------------------------|
| Fe-BTC-110-1                  | $Q_m = 5.93 \text{ mg/g}$<br>$K_a = 2.5\text{E-}04 \text{ mg-}1$<br>$R^2 = 0.9791$  | $K_F = 1.44\text{E-}02 \text{ mg/g}$<br>$\eta_F = 1.56$<br>$R^2 = 0.9969$ |
| Fe-BTC-110-3                  | $Q_m = 12.2 \text{ mg/g}$<br>$K_a = 1.03\text{E-}04 \text{ mg-}1$<br>$R^2 = 0.9944$ | $K_F = 5.5\text{E-}03 \text{ mg/g}$<br>$\eta_F = 1.29$<br>$R^2 = 0.9952$  |
| Fe-BTC-110-5                  | $Q_m = 12.1 \text{ mg/g}$<br>$K_a = 1.25\text{E-}04 \text{ mg-}1$<br>$R^2 = 0.9622$ | $K_F = 5.52\text{E-}03 \text{ mg/g}$<br>$\eta_F = 1.29$<br>$R^2 = 0.9952$ |



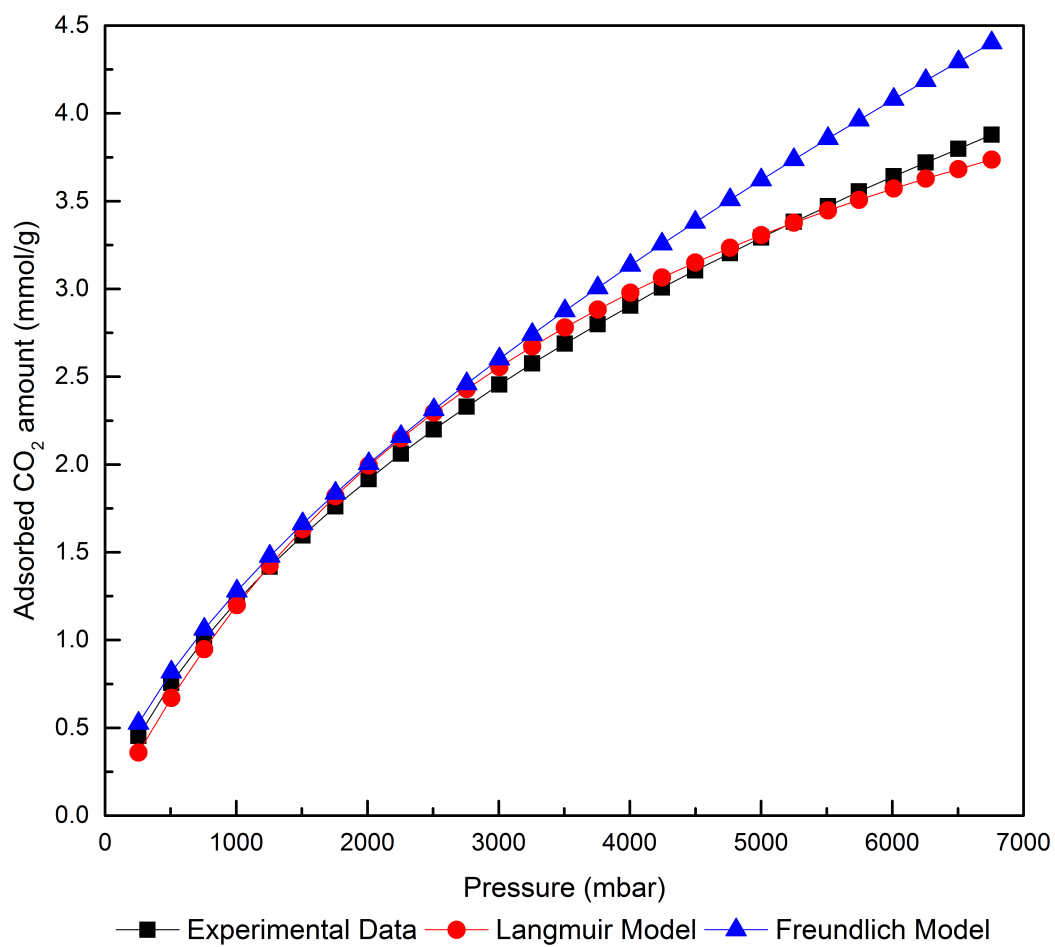


Figure 128. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich Model of Fe-BTC-110-1.

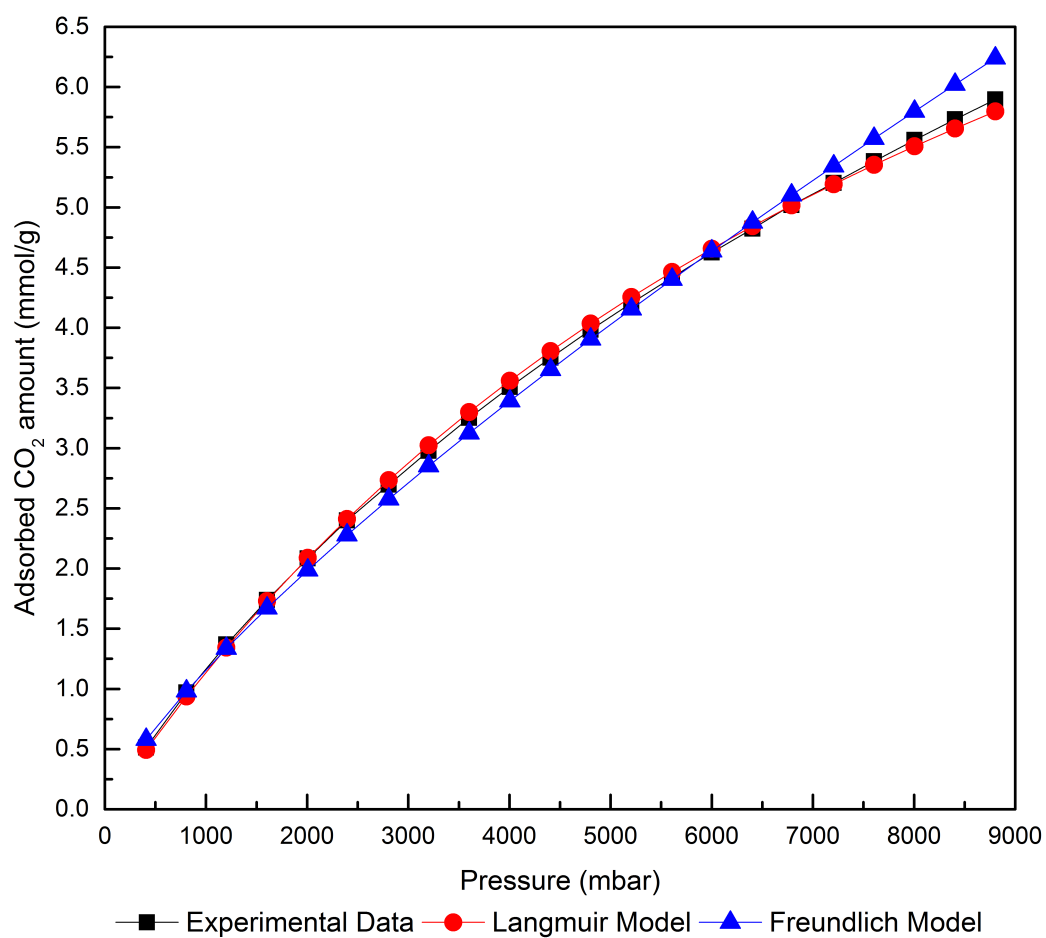


Figure 129. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich Model of Fe-BTC-110-3.

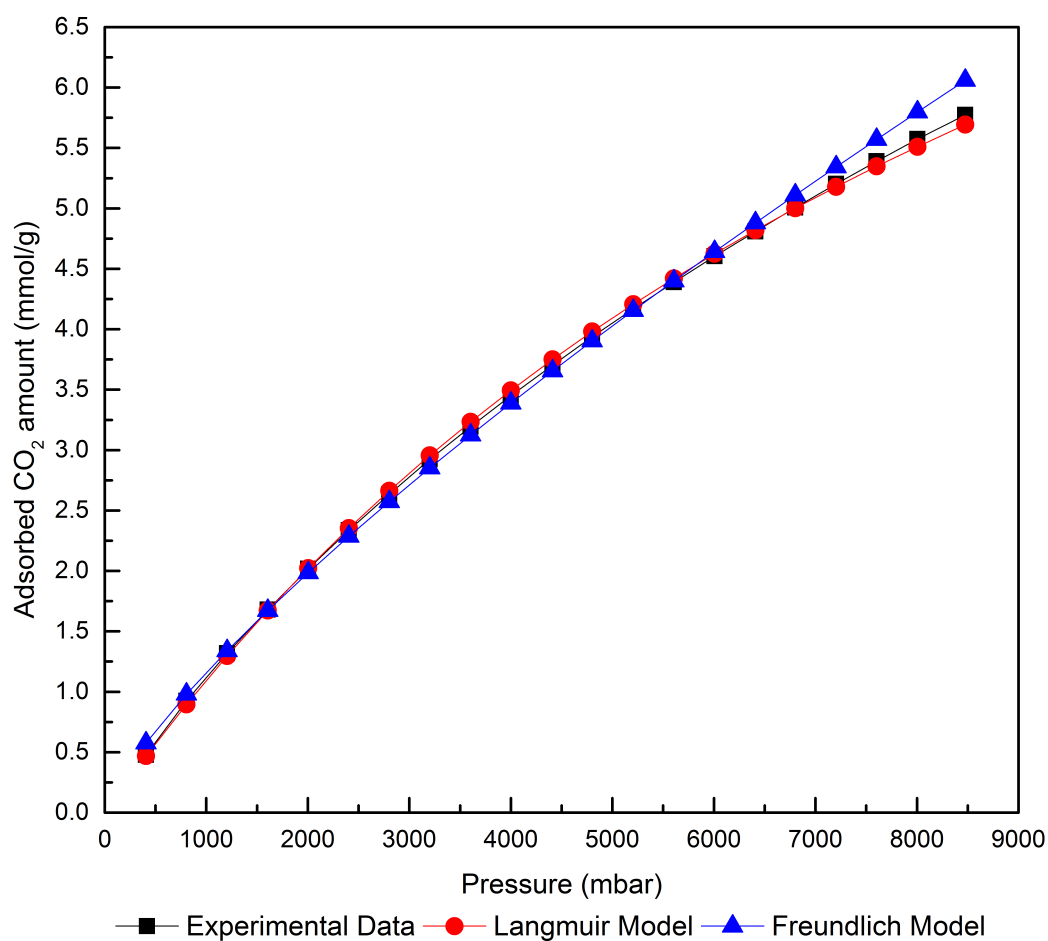


Figure 130. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich Model of Fe-BTC-110-5.

Table 40. Respective equations obtained from models

| Hierarchical porous<br>Fe-BTCs | Langmuir Model                           | Freundlich Model                         |
|--------------------------------|------------------------------------------|------------------------------------------|
| Fe-BTC-130-1                   | $y = 0.1153x + 946.06$<br>$R^2 = 0.9921$ | $y = 0.7736x - 2.35$<br>$R^2 = 0.9931$   |
| Fe-BTC-130-3                   | $y = 0.1107x + 656.9$<br>$R^2 = 0.9704$  | $y = 0.7458x - 2.1252$<br>$R^2 = 0.9995$ |
| Fe-BTC-130-5                   | $y = 0.0806x + 855.78$<br>$R^2 = 0.9967$ | $y = 0.8119x - 2.4075$<br>$R^2 = 0.9951$ |

Table 41. Langmuir and Freundlich isotherm parameters

| Hierarchical porous Fe-BTCs | Langmuir Model                                                                  | Freundlich Model                                                   |
|-----------------------------|---------------------------------------------------------------------------------|--------------------------------------------------------------------|
| Fe-BTC-130-1                | $Q_m = 8.67 \text{ mg/g}$<br>$K_a = 1.2E-04 \text{ mg}^{-1}$<br>$R^2 = 0.9921$  | $K_F = 4.45E-03 \text{ mg/g}$<br>$\eta_F = 1.29$<br>$R^2 = 0.9931$ |
| Fe-BTC-130-3                | $Q_m = 9.03 \text{ mg/g}$<br>$K_a = 1.69E-04 \text{ mg}^{-1}$<br>$R^2 = 0.9704$ | $K_F = 7.5E-03 \text{ mg/g}$<br>$\eta_F = 1.34$<br>$R^2 = 0.9995$  |
| Fe-BTC-130-5                | $Q_m = 12.4 \text{ mg/g}$<br>$K_a = 9.42E-05 \text{ mg}^{-1}$<br>$R^2 = 0.9967$ | $K_F = 3.91E-03 \text{ mg/g}$<br>$\eta_F = 1.23$<br>$R^2 = 0.9951$ |

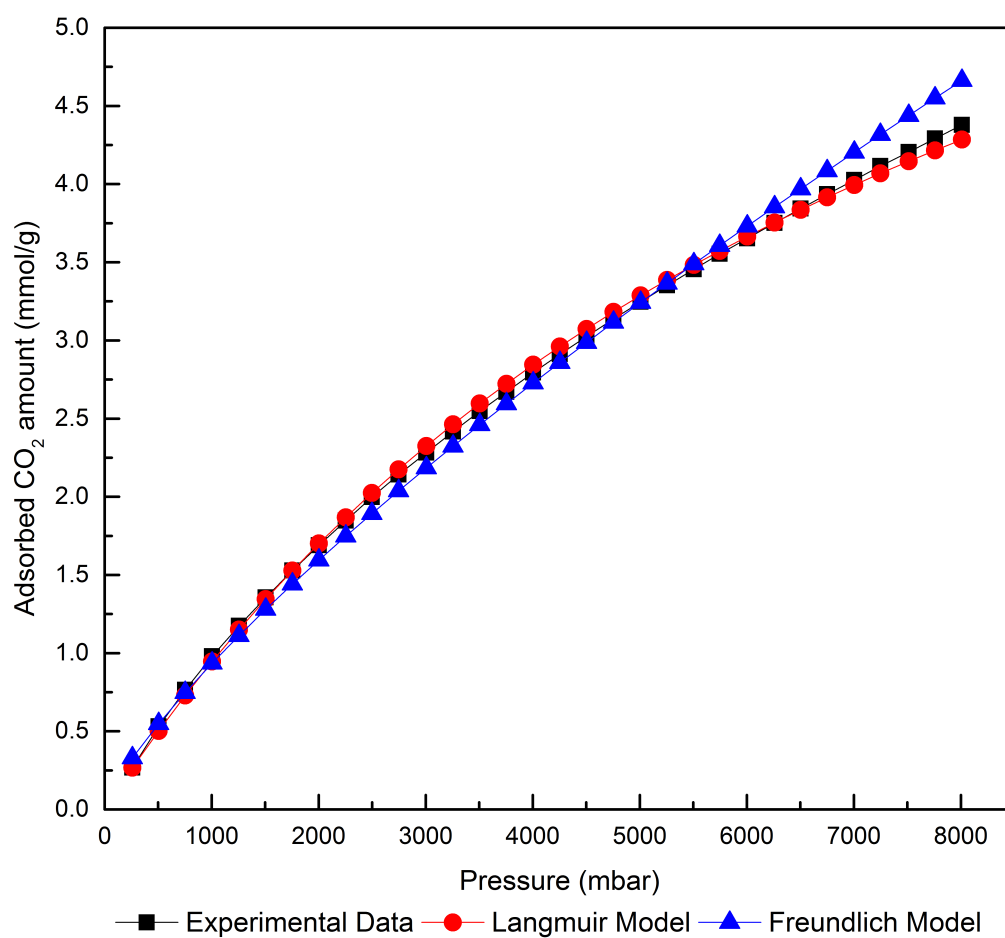


Figure 131. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich Model of Fe-BTC-130-1.

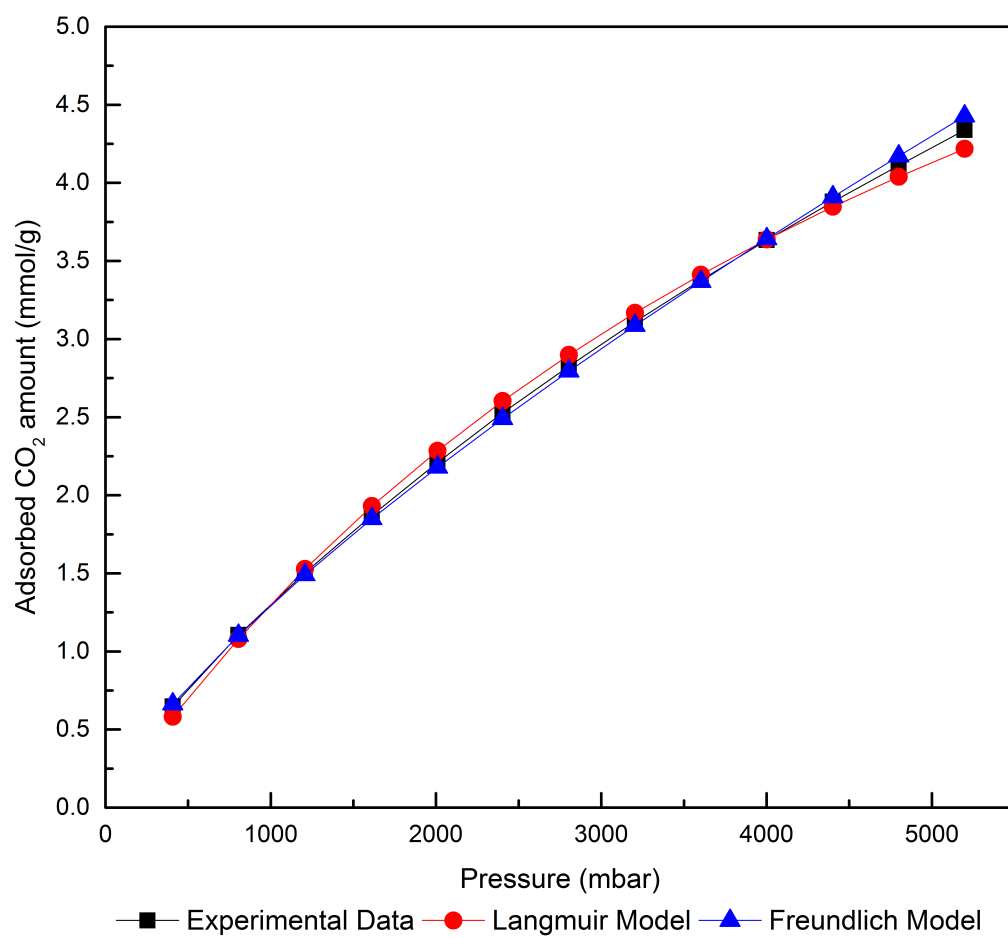


Figure 132. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich Model of Fe-BTC-130-3.

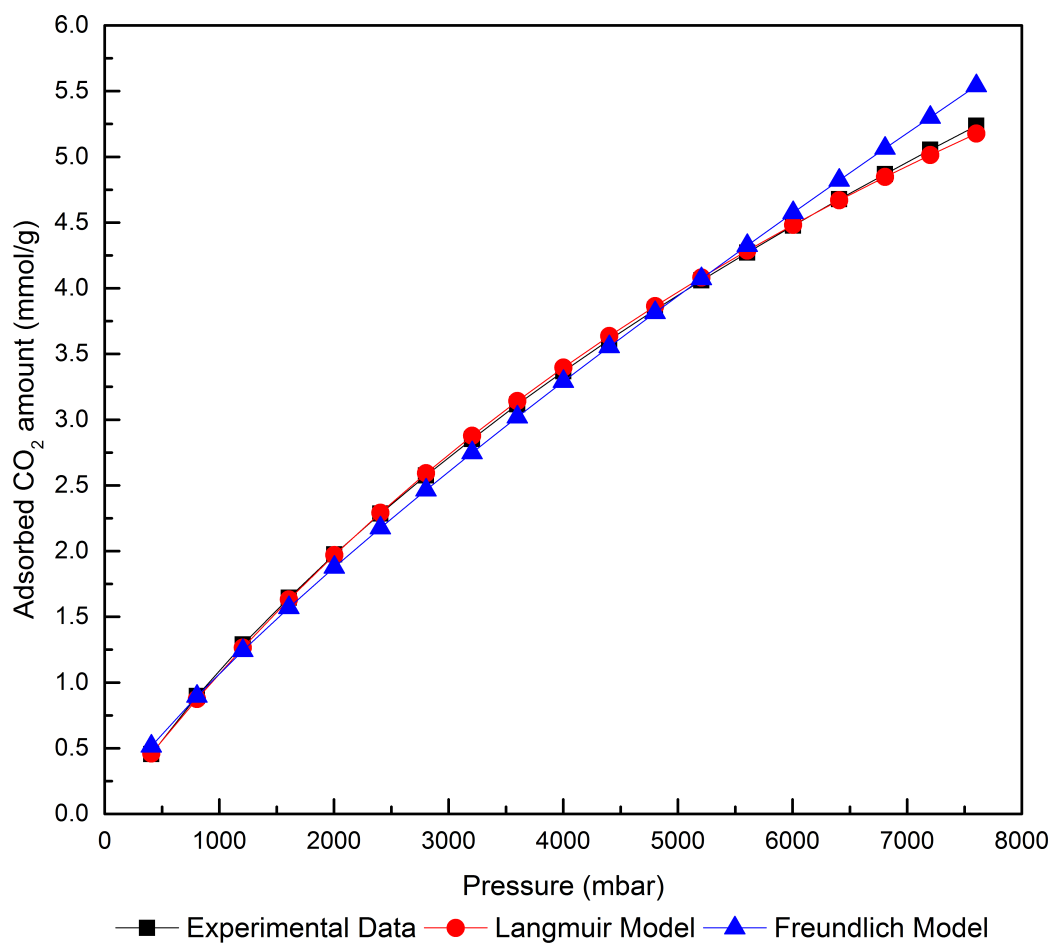


Figure 133. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich Model of Fe-BTC-130-5.

Table 42. Respective equations obtained from models

| Hierarchically<br>porous Fe-BTCs | Langmuir Model                           | Freundlich Model                        |
|----------------------------------|------------------------------------------|-----------------------------------------|
| Fe-BTC-150-1                     | $y = 0.0846x + 785.5$<br>$R^2 = 0.9931$  | $y = 0.7708x - 2.24$<br>$R^2 = 0.9965$  |
| Fe-BTC-150-3                     | $y = 0.0683x + 797.35$<br>$R^2 = 0.9974$ | $y = 0.8044x - 2.3425$<br>$R^2 = 0.996$ |
| Fe-BTC-150-5                     | $y = 0.09x + 972.86$<br>$R^2 = 0.982$    | $y = 0.781x - 2.3546$<br>$R^2 = 0.9984$ |

Table 43. Langmuir and Freundlich isotherm parameters

| Hierarchically porous Fe-BTCs | Langmuir                         | Freundlich       |
|-------------------------------|----------------------------------|------------------|
| Fe-BTC-150-1                  | $Q_m = 11.82 \text{ mg/g}$       | $K_F = 5.7E-03$  |
|                               | $K_a = 1.08E-04 \text{ mg}^{-1}$ | $\eta_F = 1.29$  |
|                               | $R^2 = 0.9931$                   | $R^2 = 0.9965$   |
| Fe-BTC-150-3                  | $Q_m = 14.64 \text{ mg/g}$       | $K_F = 4.5E-03$  |
|                               | $K_a = 8.57E-05 \text{ mg}^{-1}$ | $\eta_F = 1.24$  |
|                               | $R^2 = 0.9974$                   | $R^2 = 0.996$    |
| Fe-BTC-150-5                  | $Q_m = 11.1 \text{ mg/g}$        | $K_F = 4.42E-03$ |
|                               | $K_a = 9.25E-05 \text{ mg}^{-1}$ | $\eta_F = 1.28$  |
|                               | $R^2 = 0.982$                    | $R^2 = 0.9984$   |



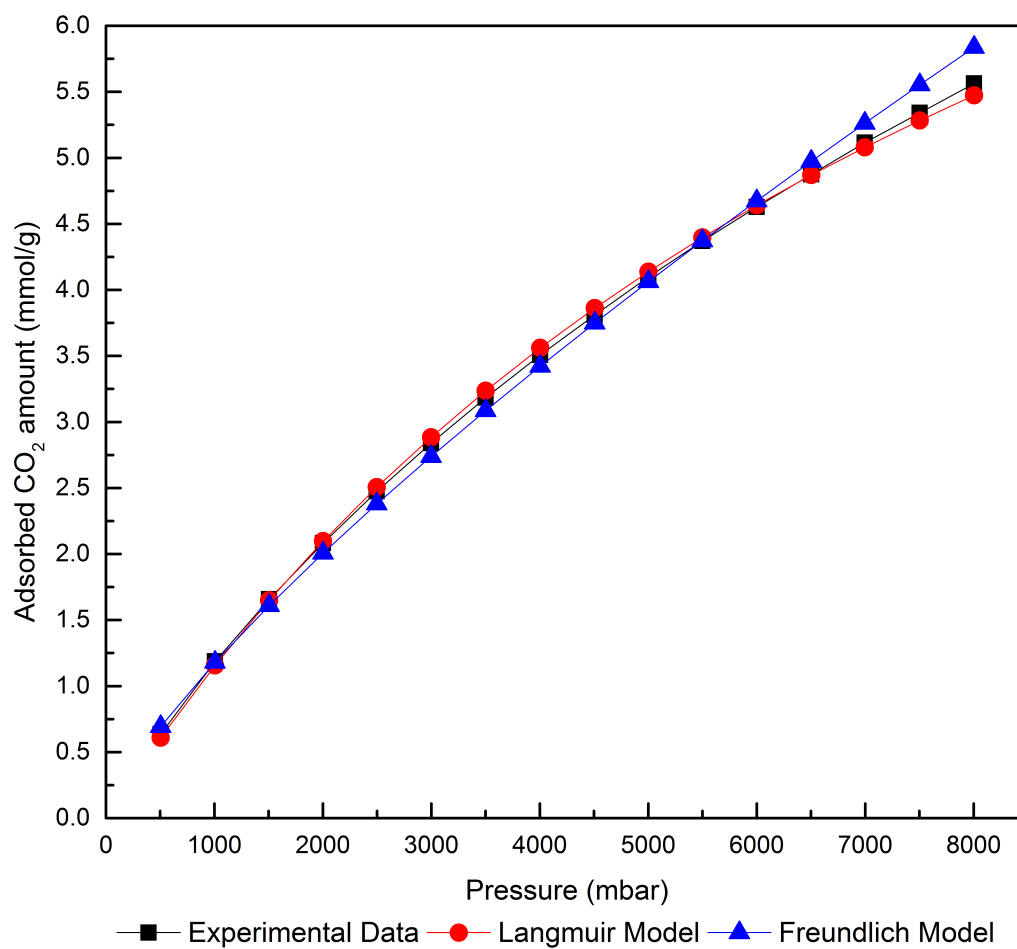


Figure 134. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich Model of Fe-BTC-150-1.

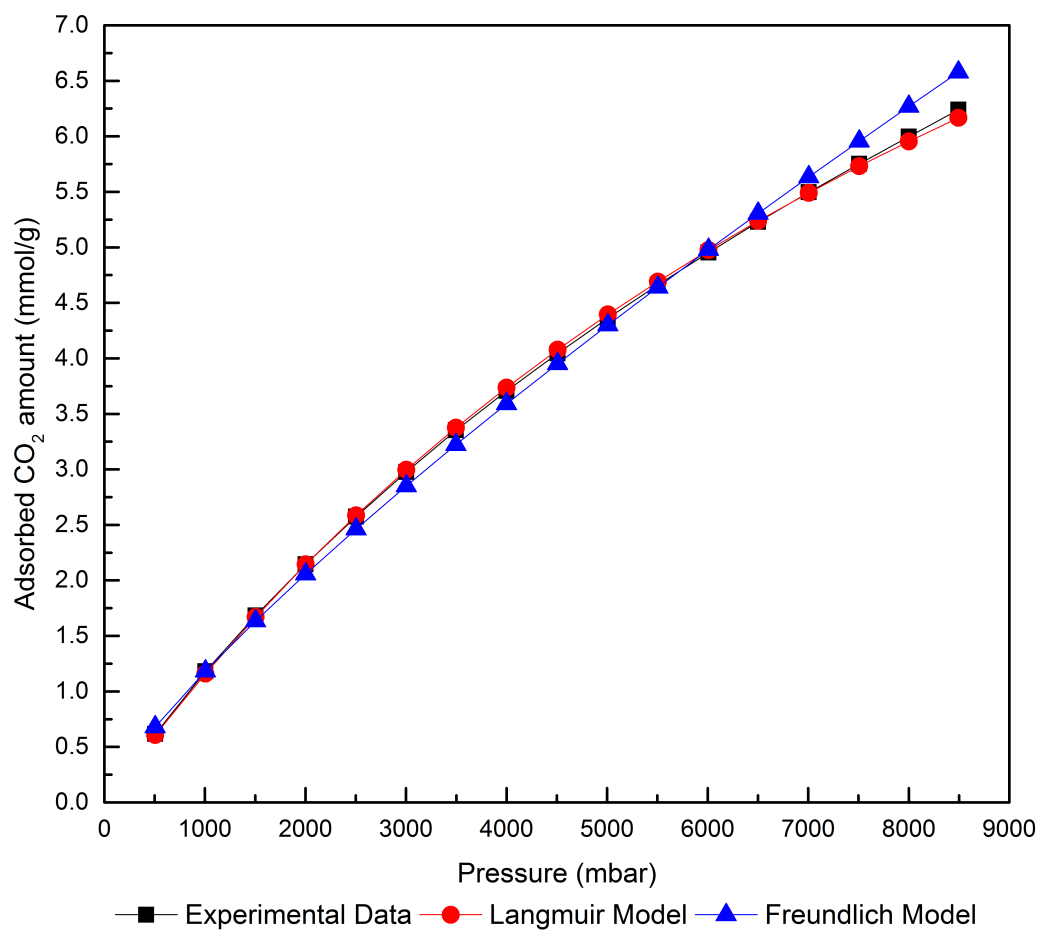


Figure 135. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich Model of Fe-BTC-150-3.

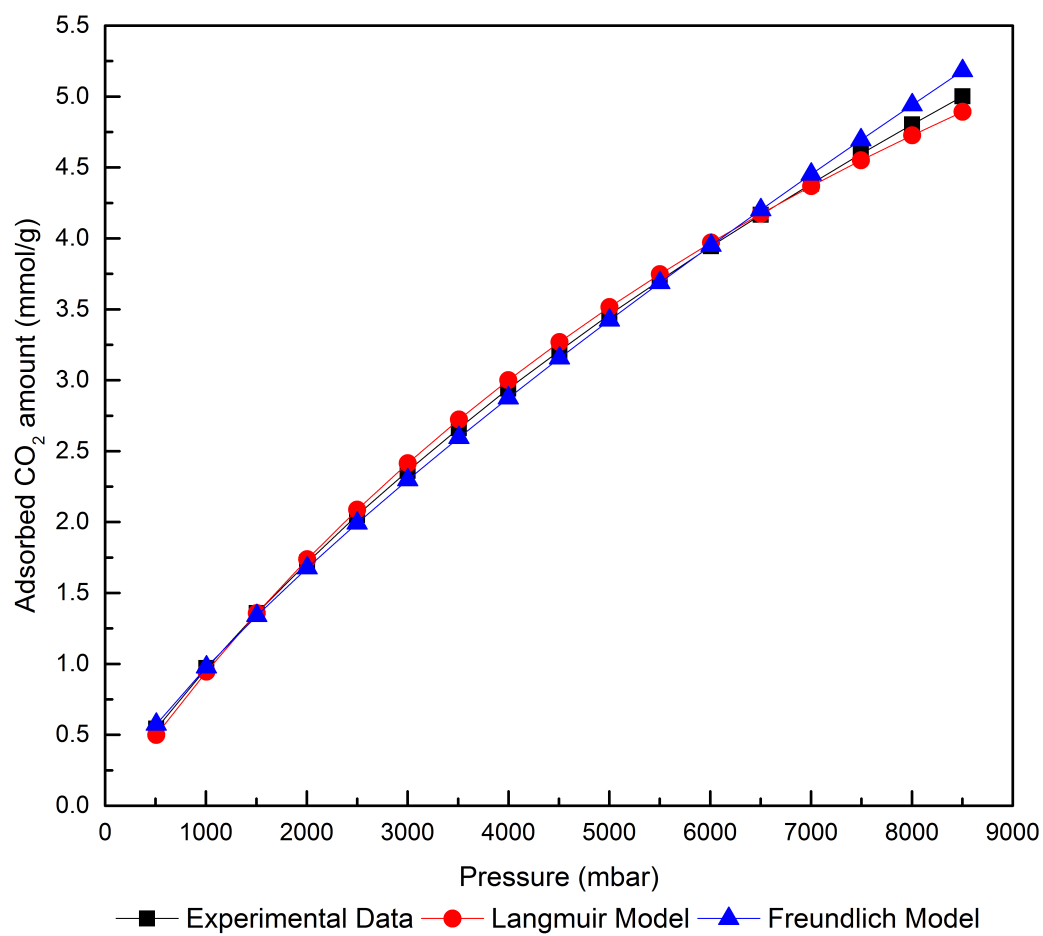


Figure 136. Comparison of experimental data and nonlinear fitting of Langmuir and Freundlich Model of Fe-BTC-150-5.

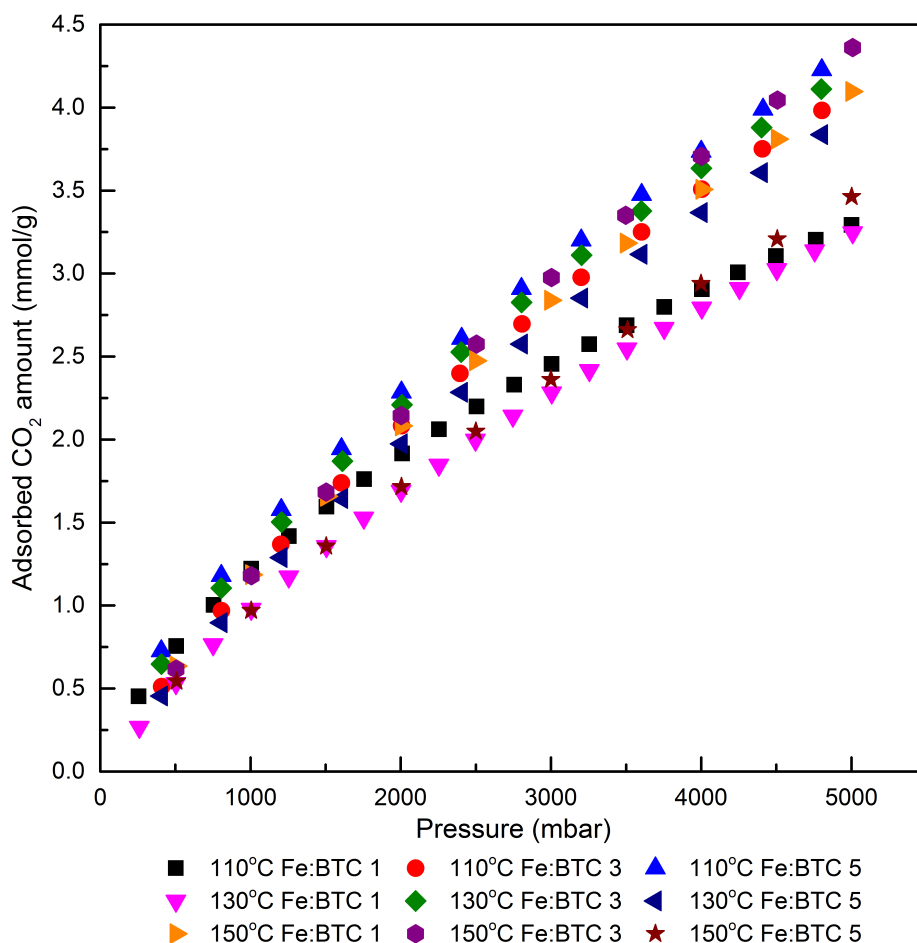


Figure 137. CO<sub>2</sub> adsorption isotherm of hierarchically porous Fe-BTCs.

Langmuir and Freundlich isotherm parameters show that Freundlich model describes the CO<sub>2</sub> adsorption (298 K) behavior of hierarchically porous Fe-BTCs better. However, as the adsorption studies were conducted till 5 bar, the shape of the isotherm may be misleading.

Among the synthesized hierarchically porous Fe-BTCs the highest CO<sub>2</sub> adsorption capacity is attained by Fe-BTC-150-3 while Fe-BTC-130-1 possesses the lowest CO<sub>2</sub> adsorption capacity. This differences in CO<sub>2</sub> adsorption capacities are attributed to their different pore size distributions. Figure 137 illustrates the amount of CO<sub>2</sub> adsorbed in between 0 and 5 bar and Table 44 shows the volume of ultramicropores, narrow micropores, fraction of narrow micropores to micropores and the CO<sub>2</sub> adsorption capacities (mmol/g) measured at 5 bar and 298 K. Figure 138-142 show the dependence of CO<sub>2</sub> adsorption capacity on the textural properties (narrow micropore, micropore, mesopore volume, total pore volume and BET surface area) of Fe-BTCs.

Table 44. Volume of ultramicropores (pore diameter < 0.7 nm), narrow micropores and micropores, and CO<sub>2</sub> adsorption capacities of Fe-BTC type crytallites measured at 5 bar and 298 K.

|                      | BET Surface<br>Area (m <sup>2</sup> /g) | Vpores < 0.7nm<br>(cm <sup>3</sup> /g) | Vpores <1<br>nm (cm <sup>3</sup> /g) | Vpores <2 nm<br>(cm <sup>3</sup> /g) | V<1nm/<br>V<2nm | CO <sub>2</sub><br>adsorption<br>capacity<br>(mmol/g) <sup>[a]</sup> |
|----------------------|-----------------------------------------|----------------------------------------|--------------------------------------|--------------------------------------|-----------------|----------------------------------------------------------------------|
| Fe-<br>BTC-<br>110-1 | 950.4±9.1E1                             | -                                      | 0.265±1.9E-2                         | 0.35±1.9E-2                          | 75.7            | 3.29                                                                 |
| Fe-<br>BTC-<br>110-3 | 1024.1±1.8E2                            | -                                      | 0.291±6.3E-2                         | 0.334±7.5E-2                         | 87.1            | 4.09                                                                 |
| Fe-<br>BTC-<br>110-5 | 1302.6±1.5E2                            | -                                      | 0.365±3.3E-2                         | 0.444±5.2E-2                         | 82.2            | 4.34                                                                 |
| Fe-<br>BTC-<br>130-1 | 692.9±1.1E2                             | -                                      | 0.198±7.0E-2                         | 0.23±7.7E-2                          | 86.0            | 3.25                                                                 |
| Fe-<br>BTC-<br>130-3 | 1207.1±6.0E1                            | -                                      | 0.33±7.0E-3                          | 0.389±3.8E-2                         | 85.6            | 4.22                                                                 |
| Fe-<br>BTC-<br>130-5 | 1024.6±1.5E2                            | -                                      | 0.292±2.6E-2                         | 0.348±5.0E-2                         | 83.9            | 3.95                                                                 |
| Fe-<br>BTC-<br>150-1 | 1139.1±2.1E1                            | -                                      | 0.318±8.3E-3                         | 0.373±8.1E-3                         | 85.3            | 4.10                                                                 |
| Fe-<br>BTC-<br>150-3 | 1312.7±1.1E1                            | 0.19                                   | 0.326±4.0E-3                         | 0.453±6.3E-3                         | 71.9            | 4.36                                                                 |
| Fe-<br>BTC-<br>150-5 | 1355.9±4.2E1                            | -                                      | 0.367±0.0148                         | 0.468±3.0E-2                         | 78.4            | 3.46                                                                 |

<sup>[a]</sup> Measured at 5 bar and 298 K.

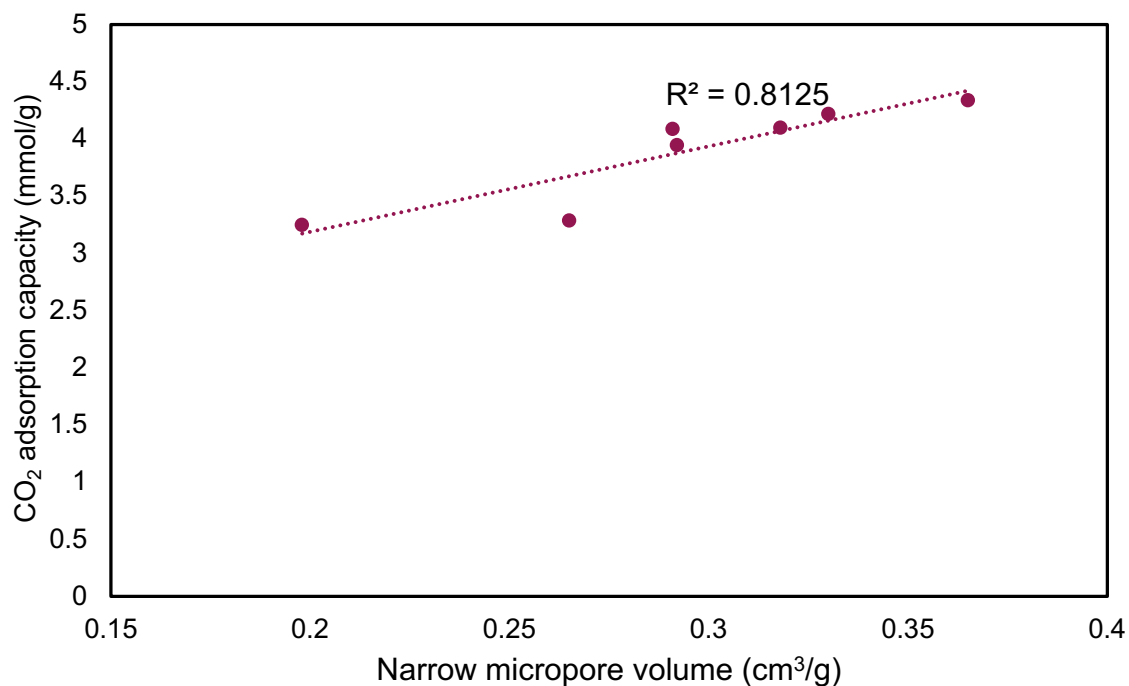


Figure 138. Dependence of CO<sub>2</sub> adsorption capacity of hierarchically porous Fe-BTCs on narrow micropore volume.

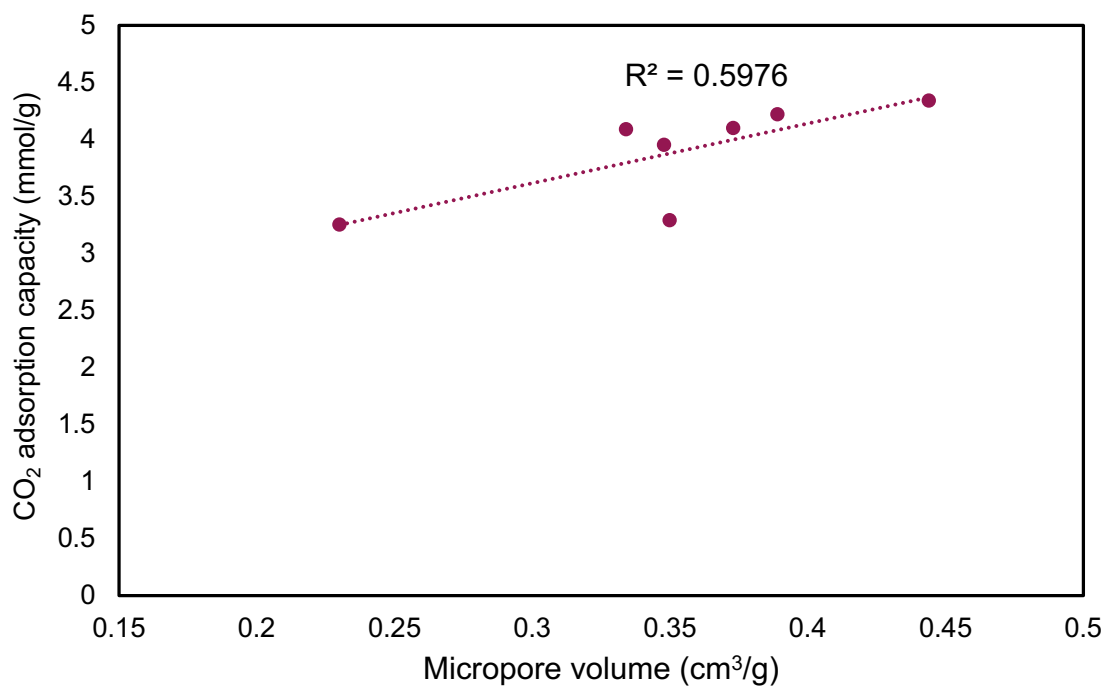


Figure 139. Dependence of CO<sub>2</sub> adsorption capacity on micropore volume of hierarchically porous Fe-BTCs.

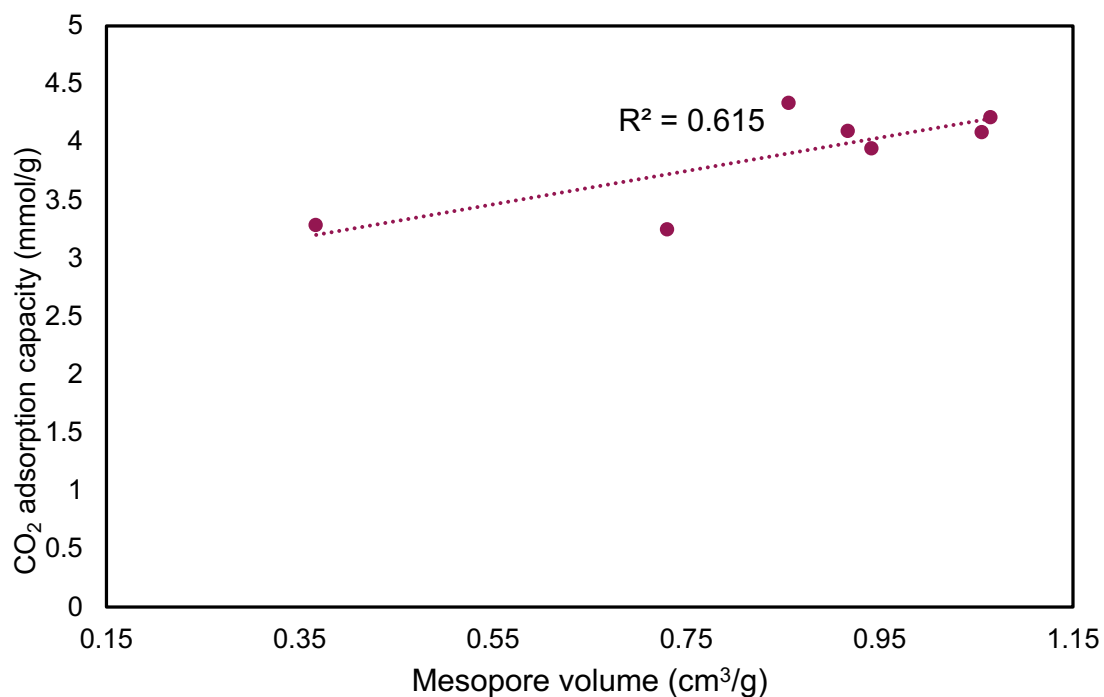


Figure 140. Dependence of CO<sub>2</sub> adsorption capacity on mesopore volume of hierarchically porous Fe-BTCs.

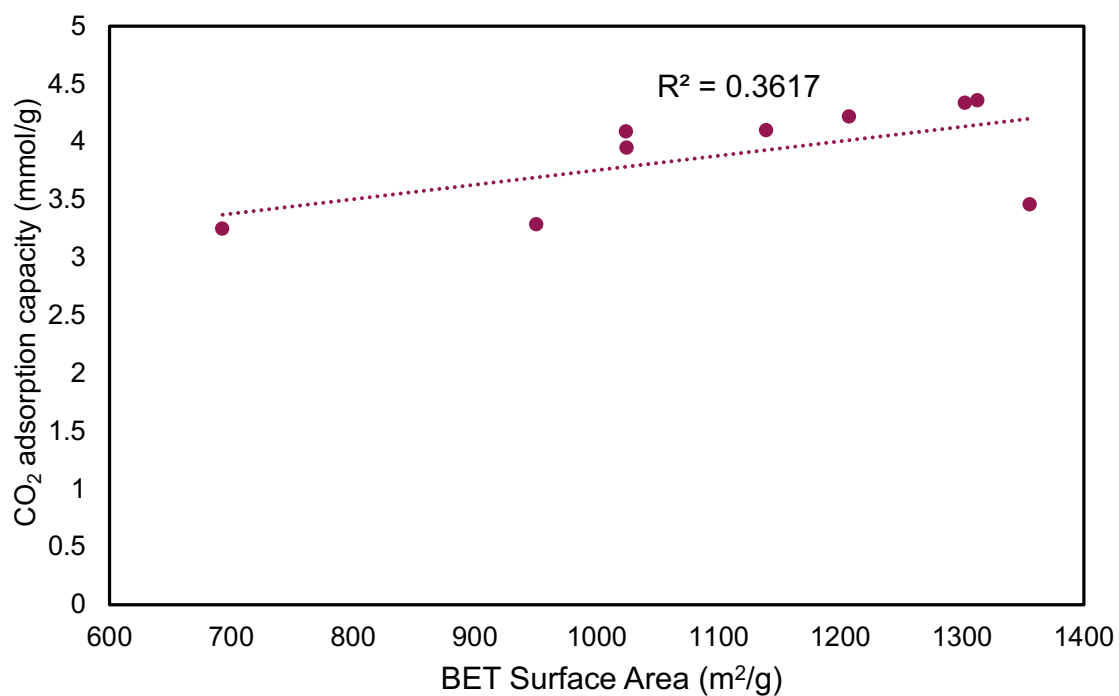


Figure 141. Dependence of CO<sub>2</sub> adsorption capacity on the BET surface area of hierarchically porous Fe-BTCs.

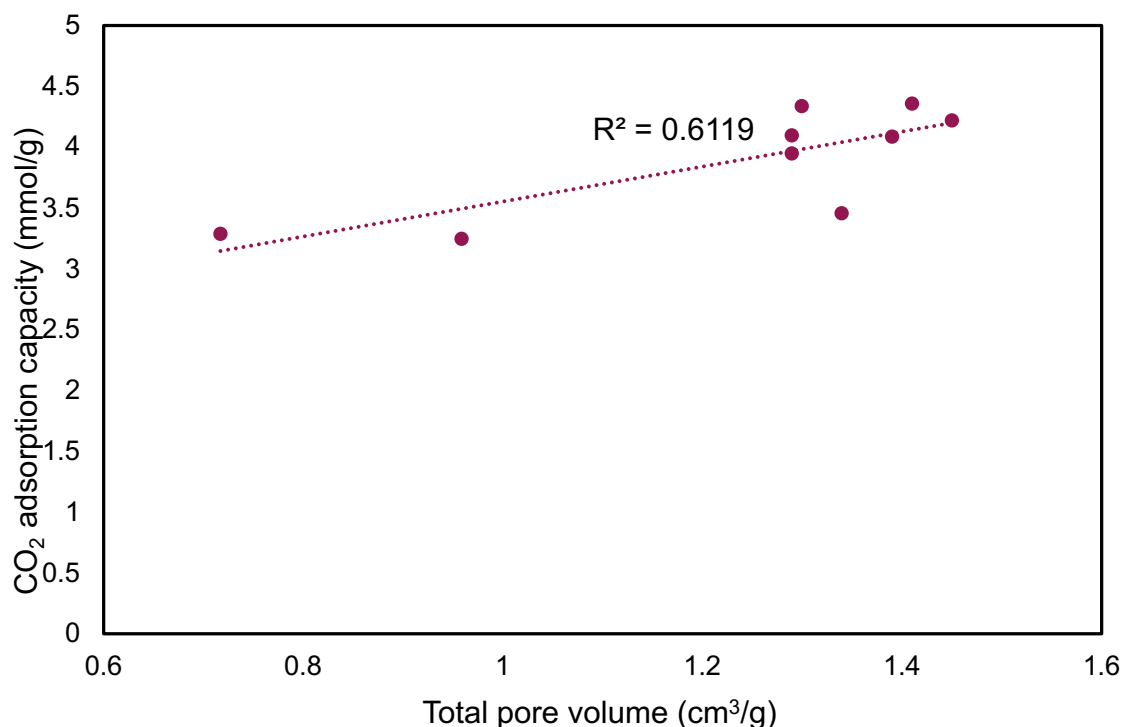


Figure 142. Dependence of CO<sub>2</sub> adsorption capacity on the BET surface area of hierarchically porous Fe-BTCs.

BET surface area ( $R^2$ , 0.36), micropore volume ( $R^2$ , 0.59), mesopore volume ( $R^2$ , 0.61), and total pore volume ( $R^2$ , 0.61), are found to be weakly correlated with the CO<sub>2</sub> adsorption capacity of Fe-BTCs. It is the narrow micropore volume ( $R^2$ , 0.81) that is strongly correlated with the CO<sub>2</sub> adsorption capacity of Fe-BTCs. Correlation coefficients indicate that among the various parameters (BET surface area, micro-, mesopore volume and total pore volume) investigated, narrow micropore volume affect the adsorbed CO<sub>2</sub> amount the most. Figure 143 illustrates the NLDFT plot of Fe-BTC in between the pore diameters of 0 and 3 nm and Figure 144 illustrates the narrow micropore volumes of hierarchically porous Fe-BTCs.



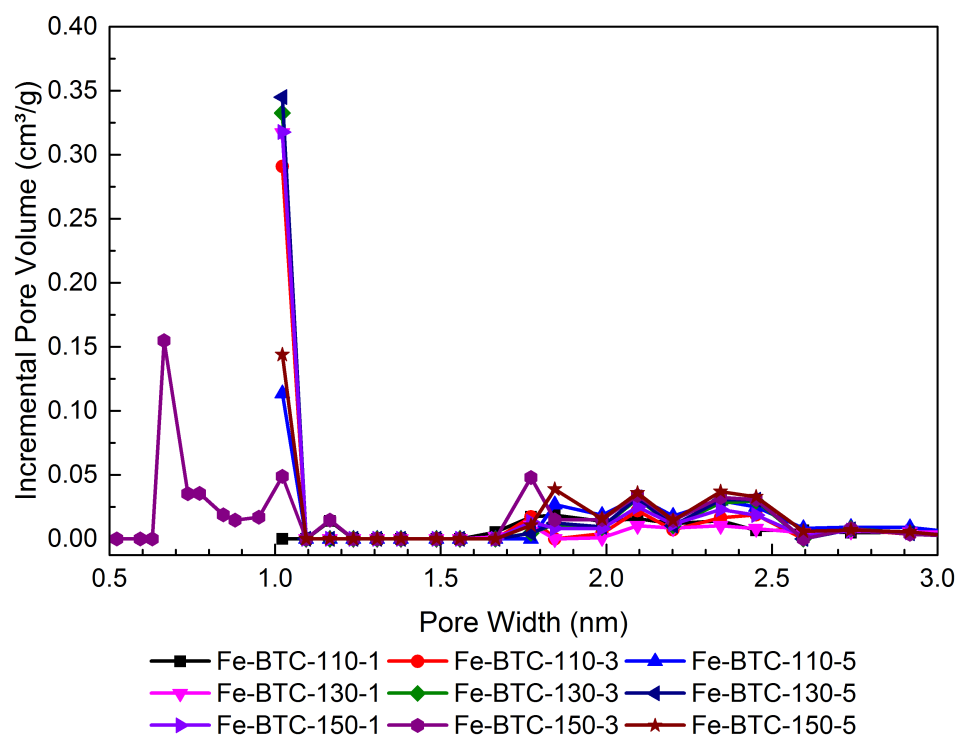


Figure 143. NLDFT plot of hierarchically porous Fe-BTCs.

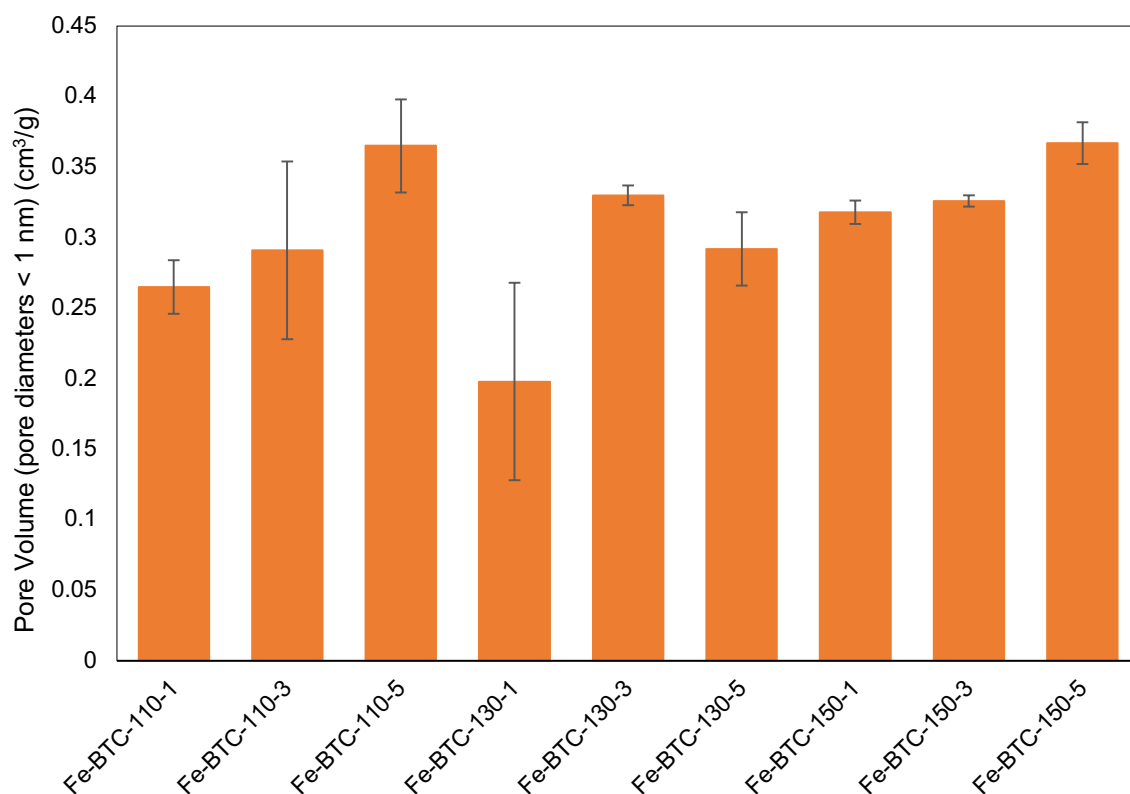


Figure 144. Narrow micropore volumes of hierarchically porous Fe-BTCs.

NLDFT plots show that Fe-BTC-150-3 is the only Fe-BTC that possesses ultramicropores in its pore structure. The volume of ultramicropores (pore diameters smaller than 0.7 nm) form 58.2% of the volume of narrow micropores and the highest CO<sub>2</sub> uptake capacity belongs to Fe-BTC-150-3. Even though the volume of narrow micropores is higher in Fe-BTC-150-5 (0.367 cm<sup>3</sup>/g), its CO<sub>2</sub> adsorption capacity (3.46 mmol/g) is 1.3 times lower than the CO<sub>2</sub> adsorption capacity of Fe-BTC-150-3 (4.36 mmol/g). Figure 145 illustrates the CO<sub>2</sub> adsorption capacities and the narrow micropore volumes of Fe-BTC-150-3 and Fe-BTC-150-5.

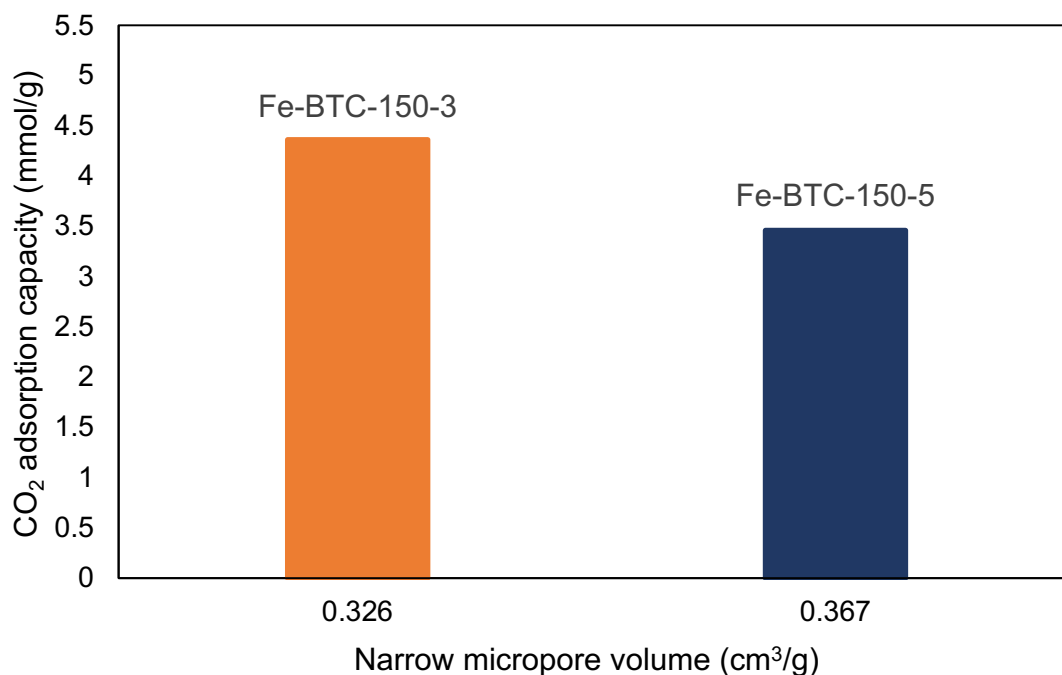


Figure 145. Comparison of the CO<sub>2</sub> adsorption capacities (5 bar and 298 K) and the narrow micropore volumes of Fe-BTC-150-3 and Fe-BTC-150-5

A similar trend is observed for Fe-BTC-110-5 and Fe-BTC-150-5. Fe-BTC-110-5 and Fe-BTC-150-5 possess similar narrow micropore volumes. However, their CO<sub>2</sub> adsorption capacities differ, considerably. Figure 146 illustrates the CO<sub>2</sub> adsorption isotherms of Fe-BTC-110-5 and Fe-BTC-150-5 and Figure 147 illustrates the CO<sub>2</sub> adsorption capacities and the narrow micropore volumes of Fe-BTC-110-5 and Fe-BTC-150-5.

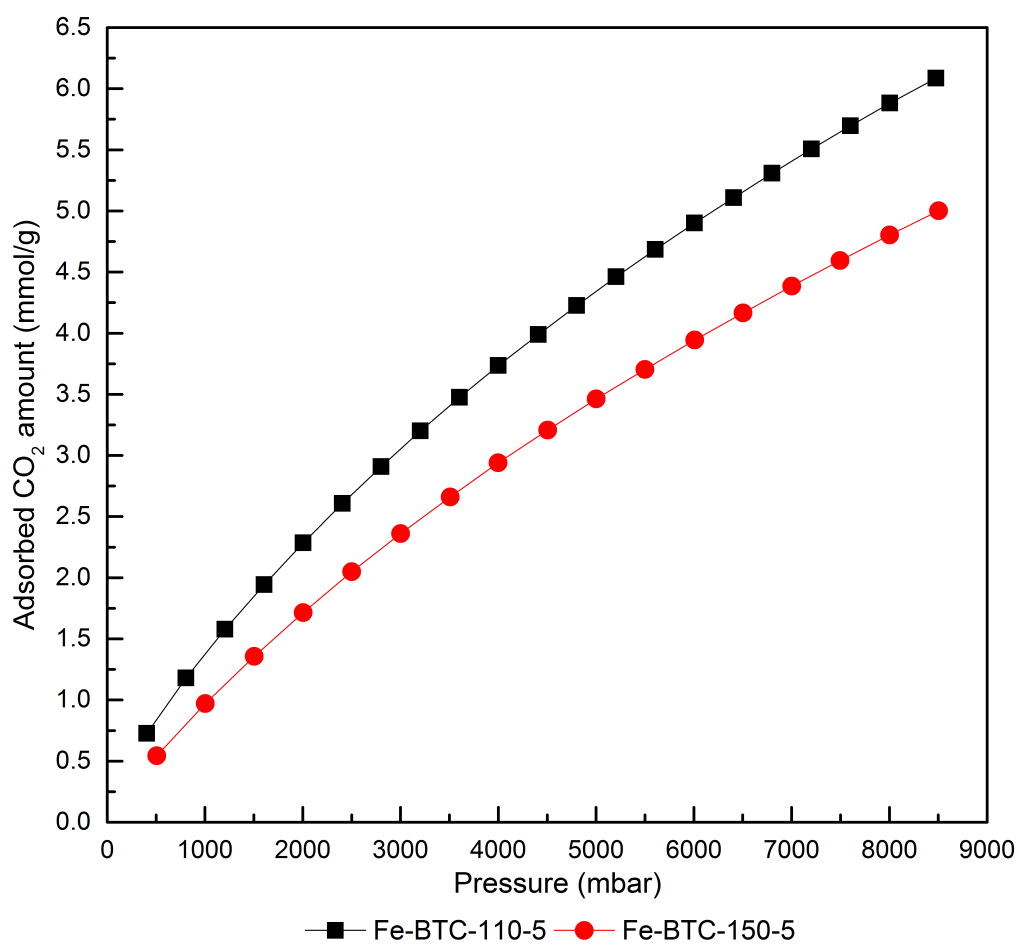


Figure 146. CO<sub>2</sub> adsorption isotherm (298 K) of Fe-BTC-110-5, and Fe-BTC-150-5.

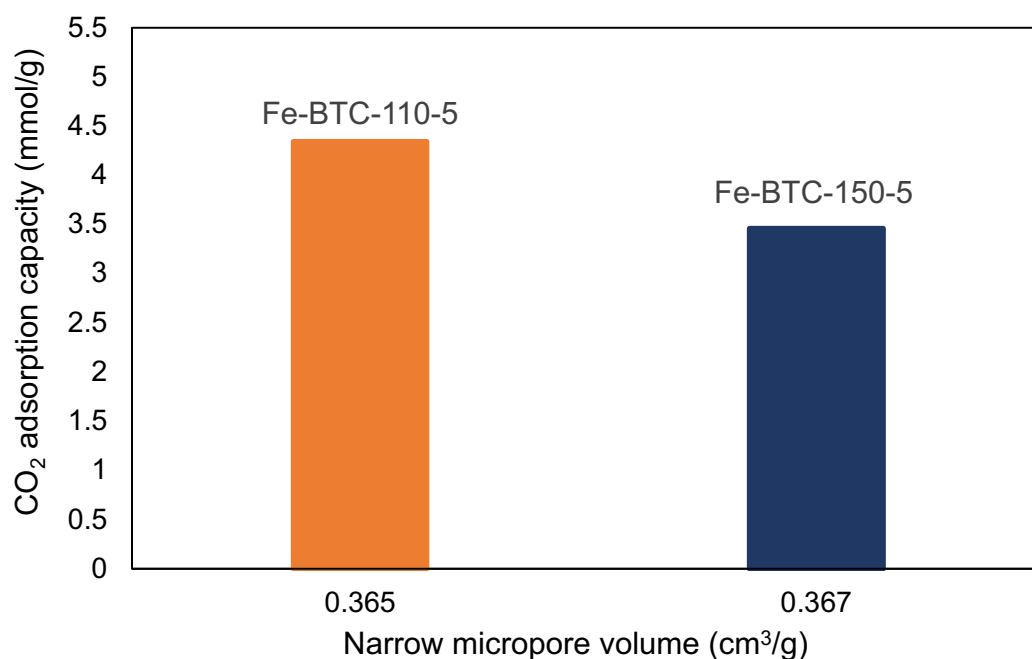


Figure 147. Comparison of the CO<sub>2</sub> adsorption capacities measured at 5 bar and 298 K and the narrow micropore volumes of Fe-BTC-110-5 and Fe-BTC-150-5.

The higher CO<sub>2</sub> adsorption capacity of Fe-BTC-110-5 is attributed to the narrow distribution of the narrow micropores through the micropore size range. The volume of narrow micropores corresponds to 82.2% of the volume of micropores in Fe-BTC-110-5 while the volume of narrow micropores corresponds to 78.4% of the volume of micropores in Fe-BTC-150-5. Thereby, we conclude that it is not only the volume of narrow micropores, but their distribution through the micropore size range that has significant effect on the adsorbed CO<sub>2</sub> amount. Figure 148 shows the CO<sub>2</sub> adsorption isotherms of Fe-BTC synthesized at 110, 130 and 150 °C.

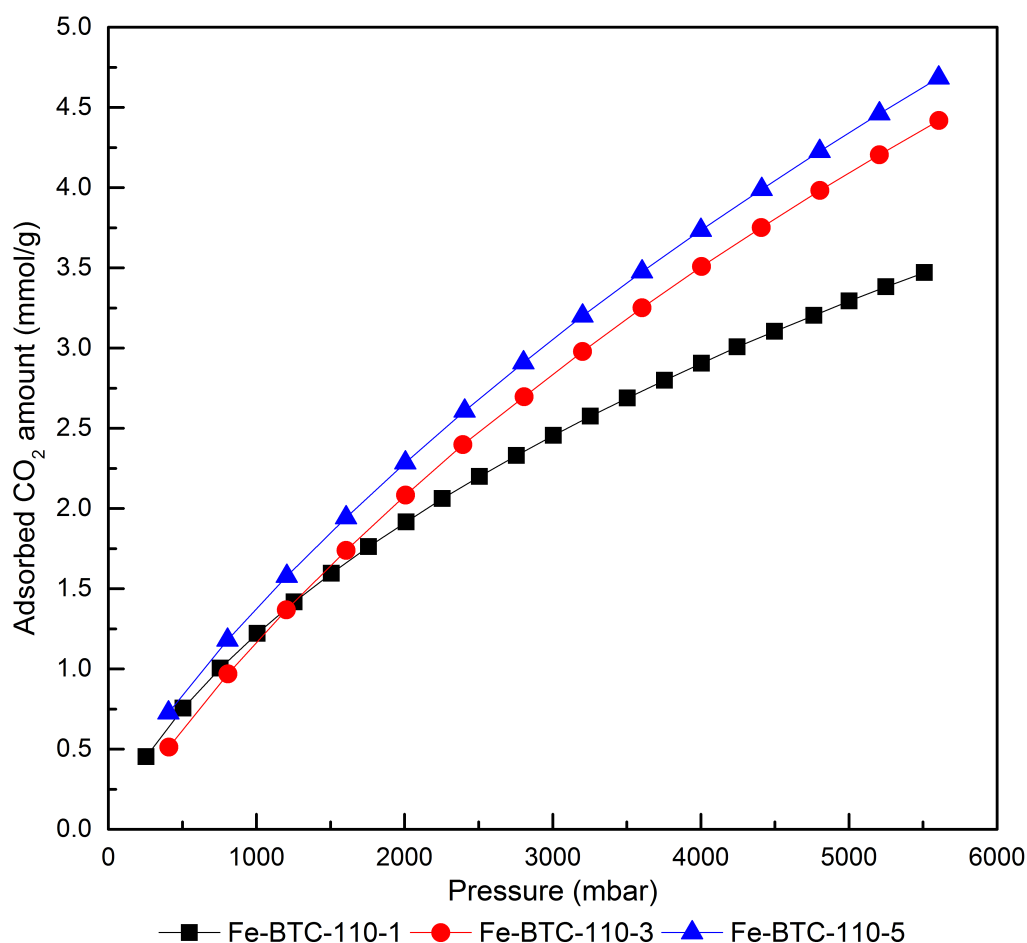


Figure 148. CO<sub>2</sub> adsorption isotherm (298 K) of Fe-BTC-110-1, Fe-BTC-110-3, and Fe-BTC-110-5.

Among the hierarchically porous Fe-BTCs synthesized at 110 °C, Fe-BTC-110-5 adsorbed the highest amount of CO<sub>2</sub> at 5 bar and 298 K. This higher CO<sub>2</sub> adsorption capacity of Fe-BTC-110-5 is attributed to its higher narrow micropore volume (0.365 cm<sup>3</sup>/g). Fe-BTC-110-1 has a relatively lower CO<sub>2</sub> adsorption capacity than Fe-BTC-110-3 and Fe-BTC-110-5. This lower CO<sub>2</sub> adsorption capacity is due to its relatively lower narrow micropore volume (0.265 cm<sup>3</sup>/g) and the broader micropore size distribution (75.7% of the micropores are formed of narrow micropores). As the narrow micropore volume increases and a narrower micropore size distribution is achieved, the adsorbed CO<sub>2</sub> amount increases.

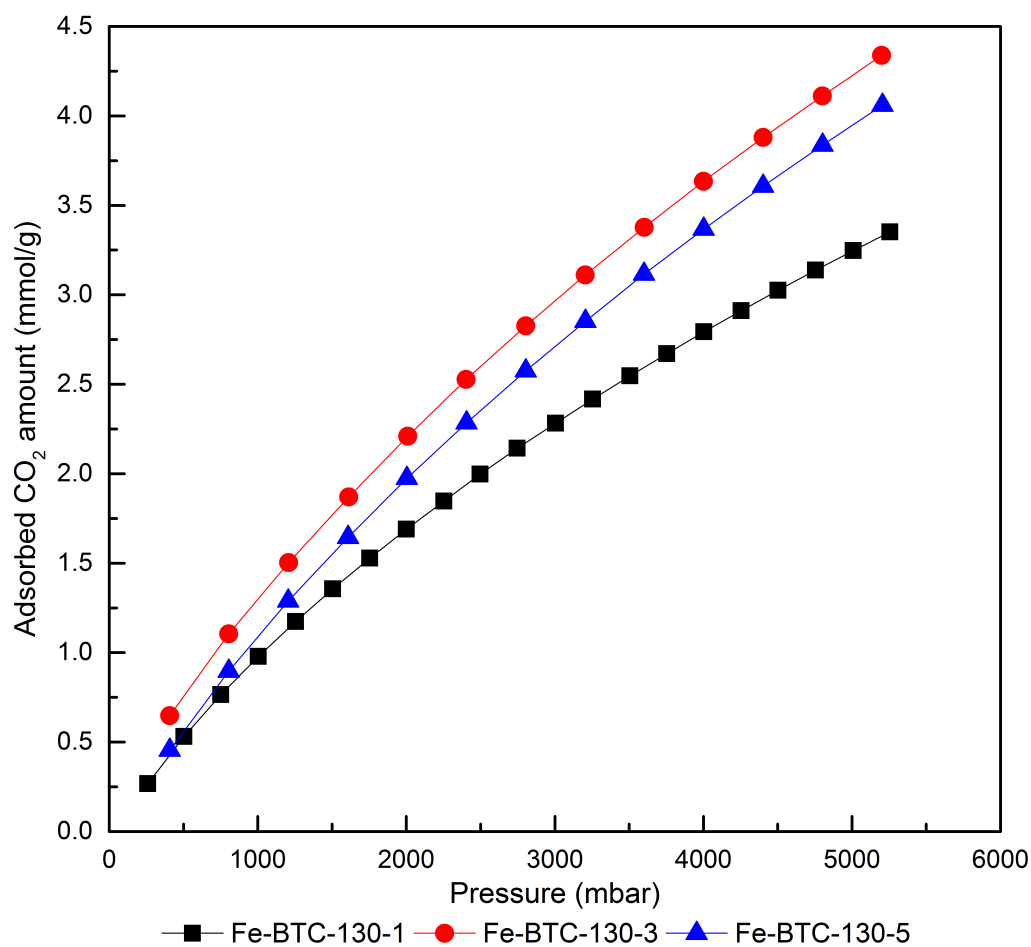


Figure 149. CO<sub>2</sub> adsorption isotherm (298 K) of Fe-BTC-130-1, Fe-BTC-130-3, and Fe-BTC-130-5.

Among the Fe-BTCs synthesized at 130 °C, the lowest CO<sub>2</sub> uptake capacity is achieved by Fe-BTC-130-1. This lower CO<sub>2</sub> uptake capacity is attributed to its lower narrow micropore volume (0.198 cm<sup>3</sup>/g). In the meantime, among the Fe-BTCs synthesized at 130 °C, the highest CO<sub>2</sub> adsorption capacity belongs to Fe-BTC-130-3 (4.22 mmol/g) which is attributed to its relatively high volume (0.33 cm<sup>3</sup>/g) of narrow micropores.

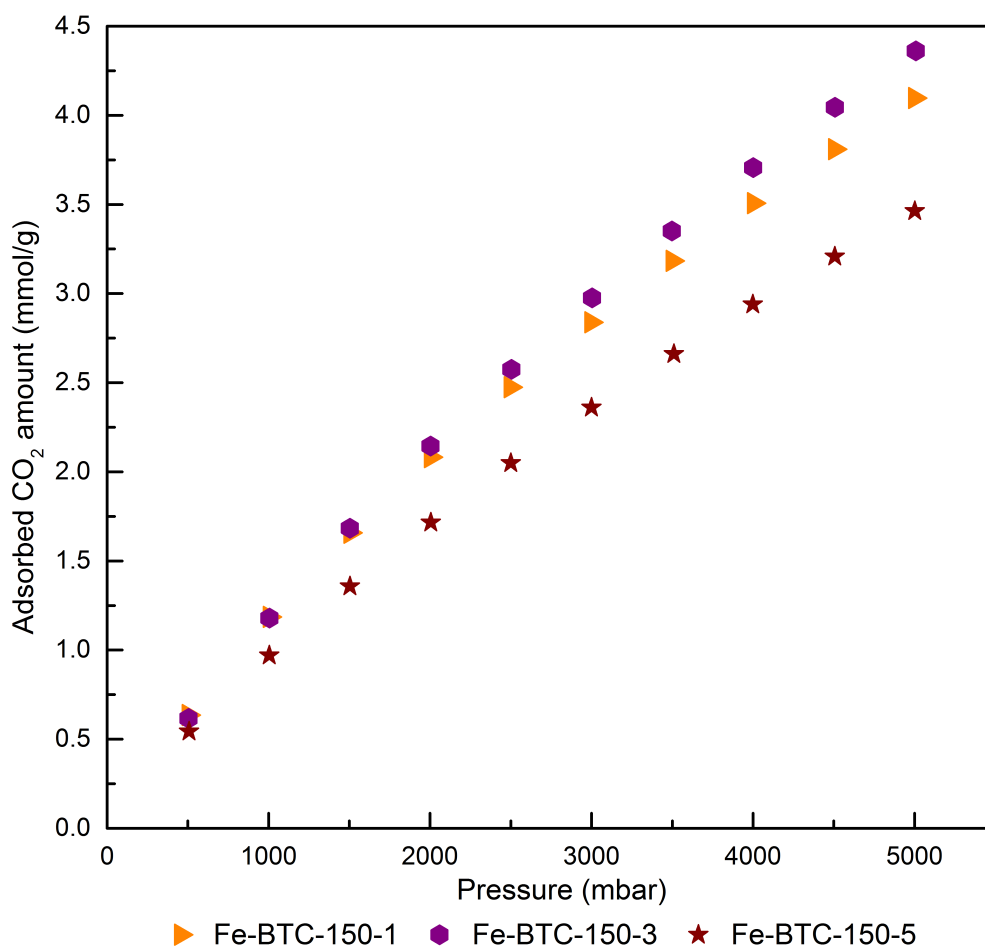


Figure 150. CO<sub>2</sub> adsorption isotherm (298 K) of Fe-BTC-150-1, Fe-BTC-150-3, and Fe-BTC-150-5.

The narrow distribution of the narrow micropores of Fe-BTC-150-1 has remarkable contribution on the CO<sub>2</sub> uptake capacity of Fe-BTC-150-1. Fe-BTC-150-1 (0.373 cm<sup>3</sup>/g) possesses a lower micropore volume than Fe-BTC-150-5 (0.468 cm<sup>3</sup>/g). However, its CO<sub>2</sub> adsorption capacity is 1.18 times greater than the CO<sub>2</sub> adsorption capacity of Fe-BTC-150-5. This higher CO<sub>2</sub> adsorption capacity of Fe-BTC-150-5 is attributed to its narrower micropore size distribution.

Fe-BTC-150-3 achieves a CO<sub>2</sub> uptake capacity 1.06 and 1.26 times greater than Fe-BTC-150-1 and Fe-BTC-150-5, respectively. As pointed earlier, Fe-BTC-150-3 is the only Fe-BTC that possesses ultramicropores (0.19 cm<sup>3</sup>/g) in its pore structure. In line with the studies conducted in literature, we have attributed the enhanced CO<sub>2</sub> adsorption capacity of Fe-BTC-150-3 to the presence of ultramicropores. Theoretical studies show that as the pore size decreases below 0.7 nm, adsorption potential of opposite ultramicropore walls overlap



and a stronger binding energy is achieved (Ello et al., 2013) and thereby, ultramicropores can attract more CO<sub>2</sub> molecules.

In conclusion, obtained results reveal that CO<sub>2</sub> adsorption capacity depends on: i) the volume of ultramicropores (pore diameter < 0.7 nm); ii) the volume of narrow micropores; and iii) the the narrow distribution of narrow micropores through the micropores.

#### **6.4.Comparison of the Properties of Fe-BTC Synthesized and Used in Other Studies with Fe-BTC Synthesized in This Study**

Table 45 illustrates the BET surface areas, total pore volumes, and decomposition temperatures of Fe-BTCs synthesized in different studies. The BET surface area and the total pore volume reported in this study is the highest of those reported for Fe-BTC (Basolite F300).

Table 45. BET surface areas, total pore volume and decomposition temperature of Fe-BTCs synthesized in different studies

| BET Surface Area<br>(m <sup>2</sup> /g) | Total Pore Volume<br>(cm <sup>3</sup> /g) | Decomposition<br>Temperature (° C) | Reference                                                                                                                                  |
|-----------------------------------------|-------------------------------------------|------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------|
| 687.0                                   | -                                         | 350                                | (Majano et al., 2013)                                                                                                                      |
| 840.0                                   | 0.45                                      | -                                  | (Dhakshinamoorthy, Alvaro, Chevreau, et al., 2012;<br>Dhakshinamoorthy et al., 2011;<br>Dhakshinamoorthy, Alvaro, Horcajada, et al., 2012) |
| 1010.0                                  | 0.90                                      | 341                                |                                                                                                                                            |
| 1024.3                                  | 0.60                                      | 348                                | (Torres et al., 2018)                                                                                                                      |
| 1060.0                                  | -                                         | -                                  | (Opanasenko et al., 2013)                                                                                                                  |
| 1116.0                                  | -                                         | -                                  | (Zukal et al., 2015)                                                                                                                       |
| 1125.0                                  | 0.61                                      | 307                                | (X. Hu et al., 2016)                                                                                                                       |
| 1312.0                                  | 1.41                                      | 342                                | This Study                                                                                                                                 |

The perturbation assisted nanofusion synthesis strategy resulted BET surface area and total pore volume to increase by a factor of 1.6 and 3.1, respectively<sup>13–15</sup>. More importantly, by controlling the Fe:BTC ratio and synthesis temperature, an Fe-BTC that consists ultramicropores in its pore structure has been synthesized.

## **6.5. Comparison with Literature**

### **6.5.1. Comparison of the Properties of Fe-BTC Synthesized and Used in Other Studies with Hierarchically Porous Fe-BTCs**

Table 46 illustrates the BET surface areas, total pore volumes, and decomposition temperatures of Fe-BTCs synthesized in different studies. The BET surface area and the total pore volume reported in this study is the highest of those reported for Fe-BTC (Basolite F300).

Table 46. BET surface areas, total pore volume and decomposition temperature of Fe-BTCs synthesized in different studies

| BET Surface Area<br>(m <sup>2</sup> /g) | Total Pore Volume<br>(cm <sup>3</sup> /g) | Decomposition<br>Temperature (° C) | Reference                                                                                                                             |
|-----------------------------------------|-------------------------------------------|------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------|
| 687.0                                   | -                                         | 350                                | (Majano et al., 2013)                                                                                                                 |
| 840.0                                   | 0.45                                      | -                                  | (Dhakshinamoorthy , Alvaro, Chevreau, et al., 2012; Dhakshinamoorthy et al., 2011; Dhakshinamoorthy, Alvaro, Horcajada, et al., 2012) |
| 1010.0                                  | 0.90                                      | 341                                |                                                                                                                                       |
| 1024.3                                  | 0.60                                      | 348                                | (Torres et al., 2018)                                                                                                                 |
| 1060.0                                  | -                                         | -                                  | (Opanasenko et al., 2013)                                                                                                             |
| 1116.0                                  | -                                         | -                                  | (Zukal et al., 2015)                                                                                                                  |
| 1125.0                                  | 0.61                                      | 307                                | (X. Hu et al., 2016)                                                                                                                  |
| 1312.0                                  | 1.41                                      | 342                                | This Study                                                                                                                            |

The perturbation assisted nanofusion synthesis strategy resulted BET surface area and total pore volume to increase by a factor of 1.6 and 3.1, respectively (Dhakshinamoorthy, Alvaro, Chevreau, et al., 2012; Dhakshinamoorthy et al., 2011; Dhakshinamoorthy, Alvaro, Horcajada, et al., 2012). More importantly, by controlling the Fe:BTC ratio and synthesis temperature, an Fe-BTC that consists ultramicropores in its pore structure has been synthesized.

### **6.5.2. Comparison of the CO<sub>2</sub> Adsorption Studies of Hierarchically Porous Fe-BTCs and the other MOFs Reported in Literature**

Highly porous MOFs have been investigated for their gas adsorption capacities. Table 47 represents the CO<sub>2</sub> adsorption capacities of several MOFs. Our results indicate that BET surface area is not the only parameter effecting CO<sub>2</sub> a capacity. But volume of narrow micropores and the distribution of narrow micropores through micropore size distribution and ultramicropores have significant effect on the amount of CO<sub>2</sub> adsorbed. Among the Fe-BTCs synthesized in this study, the highest CO<sub>2</sub> adsorption capacity belongs to Fe-BTC-150-3 (5.2 wt. % or 1.18 mmol/g at 1 bar and 298 K). CO<sub>2</sub> uptake capacity of Fe-BTC-150-3 is found to be higher than those of reported MOFs listed below.

Table 47. BET surface areas, and CO<sub>2</sub> uptake capacities of some of those reported MOFs

| MOF                       | BET Surface Area (m <sup>2</sup> /g) | Pressure (bar) | Temperature (K) | CO <sub>2</sub> Uptake Capacity         |
|---------------------------|--------------------------------------|----------------|-----------------|-----------------------------------------|
| Fe-BTC-150-3 (This study) | 1312.7                               | 1              | 298             | 5.20 wt. %; 1.18 mmol/g                 |
| Fe-BTC                    | 1009.0                               | 1              | 298             | 0.71 mmol/g (M. Du et al., 2016)        |
| MOF-177                   | 5400.0                               | 1              | 298             | 3.6 wt. % (Mason et al., 2011b)         |
| UMCM-1                    | 4034.0                               | 1              | 298             | 3.8 wt. % (A. Ö. Yazaydin et al., 2009) |
| MIL-101(Cr)               | 2674.0                               | 1              | 298             | 4.2 wt. % (Gumma et al., 2009)          |
| ZIF-8                     | 1135.0                               | 1              | 298             | 4.3 wt. % (A. Ö. Yazaydin et al., 2009) |
| MOF-5                     | 2833.0                               | 1              | 298             | 4.5 wt. % (Millward & Yaghi, 2005a)     |
| IRMOF-3                   | 2160.0                               | 1              | 298             | 5.1 wt. % (Millward & Yaghi, 2005a)     |
| ZIF-25                    | 1110.0                               | 1              | 298             | 4.7 wt. % (W. Morris et al., 2010)      |
| IRMOF-6                   | 2516.0                               | 1.2            | 298             | 4.6 wt. % (Millward & Yaghi, 2005a)     |
| ZIF-97                    | 564.0                                | 1.1            | 298             | 4.5 wt. % (W. Morris et al., 2010)      |
| ZIF-100                   | 595.0                                | 1              | 298             | 3.8 wt. % (Phan et al., 2010)           |
| ZIF-95                    | 1050.0                               | 1              | 298             | 3.7 wt. % (Phan et al., 2010)           |
| ZIF-71                    | 652.0                                | 1              | 298             | 2.8 wt. % (W. Morris et al., 2010)      |
| Mg-MOF-1                  |                                      | 1              | 298             | 2.7 wt. % (Mallick et al., 2010)        |
| SNU-31                    |                                      | 1              | 298             | 2.6 wt. % (H. J. Park et al., 2010)     |
| MOF-2                     | 345.0                                | 1              | 298             | 2.4 wt. % (Millward & Yaghi, 2005a)     |

## 6.6. Concluding Remarks

Here, we report the CO<sub>2</sub> adsorption capacities of hierarchically porous Fe-BTCs synthesized by a perturbation assisted nanofusion synthesis strategy that limits the growth of single crystal MOFs, and enhances BET surface area, micropore volume, total pore volume and thermal stability. The reported synthesis strategy increases the BET surface area and total pore volume by 1.6, and 3.1 times, respectively. A BET surface area of 1312 m<sup>2</sup>/g and a total pore volume of 1.41 cm<sup>3</sup>/g is achieved which are the highest BET surface area and total pore volume that have been reported for Fe-BTC, to date.

Among the synthesized hierarchically porous Fe-BTCs, Fe-BTC that possesses ultramicropores (58.2% of the micropore volume is formed of ultramicropores) in its pore structure achieves the highest CO<sub>2</sub> adsorption capacity (5.2 wt. % or 1.18 mmol/g at 1 bar and 298 K; 27.5 wt.% or 6.24 mmol/g at 8.5 bar and 298 K) which points out the significant contribution of ultramicropores on the CO<sub>2</sub> adsorption capacity.

By this study, we experimentally show the crucial role of ultramicropores on the adsorbed CO<sub>2</sub> amount. As pore size decreases below 0.7 nm, adsorption potential of opposite ultramicropore walls overlap and a stronger binding energy is achieved (Ello et al., 2013) and ultramicropores attract more CO<sub>2</sub> molecules. In addition, hierarchically porous Fe-BTCs with higher narrow micropore volumes and narrower micropore size distributions possess higher CO<sub>2</sub> adsorption capacities than the hierarchically porous Fe-BTCs that possess lower micropore volumes or the hierarchically porous Fe-BTCs that possess higher narrow micropore volumes but broader micropore size distributions.

Our results reveal that adsorbed CO<sub>2</sub> amount is controlled by: i) the presence of ultramicropores; ii) the volume of narrow micropores; and iii) the narrow distribution of narrow micropores through the micropore size range.

By synthesizing Fe-BTCs via the perturbation assisted nanofusion synthesis strategy, we report a BET surface area, pore volume, and CO<sub>2</sub> uptake capacity that is the highest of all those BET surface areas, pore volume, and CO<sub>2</sub> uptake capacities reported for hierarchically porous Fe-BTC, to date. We clearly showed that synthesizing a MOF that is formed of ultramicropores with a high ultramicropore volume and a narrow micropore size distribution would be the key factor to enhance the adsorbed CO<sub>2</sub> amount. Last but not least, considerable efforts have to be spent on the development of porous materials that are formed

mainly of ultramicropores with high pore volumes to increase the measured CO<sub>2</sub> uptake capacities at 1 bar and 298 K.

## Chapter VII

### Hydrogen adsorption capacity of hierarchically porous Fe-BTCs: influence of pore size distribution

#### 7.1. Background

The energy consumption rate in 2018 has been the highest since 2010 (Teter, Cazzola, & Petropoulos, n.d.) and the energy consumption by the transportation sector corresponds to 21% (“Energy demand by sector | Energy economics | Home,” n.d.). The International Energy Agency (IEA) has reported that transportation sector contributes by 24% to the CO<sub>2</sub> emissions (Teter et al., n.d.) which originates from fuel combustion and road vehicles contribute by three quarters (Teter et al., n.d.). There rises the necessity to develop and improve technologies alternative to fossil fuels which would decrease or eliminate CO<sub>2</sub> emissions (Fakioğlu et al., 2004; Louis Schlapbach & Züttel, 2002; Wilberforce et al., 2017; Yürüm et al., 2009a; Fan Zhang, Zhao, Niu, & Maddy, 2016; Zuo, E, & Lin, 2018; Zuo, Li, Zhang, & Li, 2019; Zuo, Jiaqiang, Liu, Peng, Zhao, et al., 2016; Zuo, Jiaqiang, Liu, Peng, Deng, et al., 2016; Andreas Züttel, Remhof, Borgschulte, & Friedrichs, 2010b).

Metal-organic frameworks (MOFs) are highly crystalline and porous materials formed of an organic and an inorganic part (O M Yaghi et al., 1995). Their high BET surface areas, and pore volumes make these materials promising in various application areas: adsorption/desorption studies, separation studies, and catalysis (H. C. Zhou, Long, & Yaghi, 2012). MOFs are found to be promising in H<sub>2</sub> adsorption studies (Moradi & Groth, 2019; Murray, Dincă, et al., 2009; Yürüm et al., 2009a). Fe-BTC is one of the five MOFs that has been commercialized by BASF (“basolite | Sigma-Aldrich,” n.d.). Basolite F300 (Fe-BTC) and MIL-100(Fe) are formed by the reaction of the same starting materials: Fe(III) and BTC (benzene-1,3,5-tricarboxylic acid). However, Basolite F300 and MIL-100(Fe) have different properties. For instance, Basolite F300 has a disordered nature whilst MIL-100(Fe) is a highly crystallite material (Dhakshinamoorthy, Alvaro, Horcajada, et al., 2012). BET surface area (1600 to 1900 m<sup>2</sup>/g) and pore volume (0.79 to 1.0 cm<sup>3</sup>/g) of MIL-100(Fe) (Huo & Yan,



2012; Jeremias, Khutia, Henninger, & Janiak, 2012; Fumin Zhang et al., 2015) is greater than the BET surface area (800 to 1300 m<sup>2</sup>/g) and pore volume (0.4 to 0.6 cm<sup>3</sup>/g) of Basolite F300 (Dhakshinamoorthy, Alvaro, Chevreau, et al., 2012; Dhakshinamoorthy et al., 2011; Dhakshinamoorthy, Alvaro, Horcajada, et al., 2012; X. Hu et al., 2016; Majano et al., 2013; Opanasenko et al., 2013; Torres et al., 2018; Zukal et al., 2015). Even though Fe-BTC is as non-toxic and highly porous as MIL-100(Fe) (Horcajada et al., 2010a), there are a few reports investigating the potential application areas of Basolite F300.

Despite the very high H<sub>2</sub> adsorption capacities of MOFs at cryogenic temperatures and high pressures (Moradi & Groth, 2019; Murray, Dincă, et al., 2009), H<sub>2</sub> adsorption capacities of MOFs decrease drastically at ambient conditions (Henrietta W Langmi, Ren, North, Mathe, & Bessarabov, 2017; Murray, Dincă, et al., 2009; Rowsell & Yaghi, 2005). To achieve higher H<sub>2</sub> adsorption capacities at 298 K, significant amount of effort has to be put on to figure out ways that enhance the interactions of H<sub>2</sub> molecules with the surface of MOFs. Two strategies have been suggested to enhance the binding energies of H<sub>2</sub> molecules to the surface of MOFs at ambient temperatures: i) formation of narrow micropores (Dinča et al., 2006; Michael Hirscher & Panella, 2007; Michael Hirscher, Panella, & Schmitz, 2010; Y. H. Hu & Zhang, 2010; Latroche, Surlé, Serre, Mellot-Draznieks, Llewellyn, Lee, Chang, Sung, et al., 2006b; R. E. Morris & Wheatley, 2008; Barbara Panella et al., 2008; Schmitz et al., 2008); and ii) introducing unsaturated metal sites to the framework. (Dinča et al., 2006; Dincă & Long, 2005). In line with what has been suggested, researchers showed that hydrogen adsorbed in the narrower pores were desorbed at higher temperatures and illustrated the direct correlation of the desorption temperature and the pore size (Michael Hirscher et al., 2010; Barbara Panella et al., 2008). Based on the thermal desorption studies and temperature dependent adsorption isotherm measurements, it has been concluded that the pore size determines the heat of adsorption of H<sub>2</sub> and emphasized on the necessity to develop frameworks with high specific surface areas and narrow pores which has been a great challenge (Michael Hirscher et al., 2010; Barbara Panella et al., 2008; Schmitz et al., 2008).

To date, there have been several strategies used in MOF synthesis to enhance BET surface area, pore volume and gas adsorption efficiencies (Topologies, Stock, & Biswas, 2012). However, formation of hierarchical porous MOFs has not drawn particular attention as a consequence of the complicated synthesis procedures and the formation of unstable

mesoporous MOF structures (Bradshaw, El-Hankari, & Lupica-Spagnolo, 2014; G. Cai & Jiang, 2017b; L. Peng et al., 2014a; S. Yuan et al., 2017; Y. Yue, Fulvio, et al., 2015; Y. Yue et al., 2013b). Perturbation assisted nanofusion synthesis strategy come to the fore with its easy, template free and relatively environmentally friendly synthesis procedure (Cao et al., 2016; Y. Yue, Fulvio, et al., 2015; Y. Yue et al., 2013a). By the perturbation assisted nanofusion synthesis strategy textural mesopores are introduced to the pore structure. By this way, both micro- and mesopores would be present and the synthesized material would benefit from the two-pore system (Bradshaw et al., 2014; Cao et al., 2016). In a pore structure at which micro- and mesopores are present, micropores increases the surface area and provide benefits in gas adsorption studies and catalysis reactions mesopores provide larger molecules diffuse easily and enhance the mass transport (Groen, Peffer, Moulijn, & Pérez-Ramírez, 2005; Yueju Zhao et al., 2011). Additionally, one can easily tune the textural porosity via synthesis parameters which provides the opportunity to tune the textural pores with respect to the application area used.

In our study, free of a template, just by vigorously stirring, hierarchical pores were formed. We showed that introducing textural pores enhances the BET surface area and total pore volume, 1.6 and 3.1 times, respectively and a BET surface area and total pore volume higher than those of reported Fe-BTCs have been achieved. With its easy and relatively environmentally friendly synthesis procedure, Fe-BTCs with a BET surface area, and total pore volume higher than those of reported Fe-BTCs have been reported.

Herein, we report the i) synthesis; ii) H<sub>2</sub> adsorption capacity; and iii) role of ultramicropores on the H<sub>2</sub> adsorption capacity of Fe-BTC. To the best of our knowledge, this is the first study to report the H<sub>2</sub> adsorption capacity of Fe-BTC measured at 298 K. By the perturbation assisted nanofusion synthesis strategy, hierarchical pores are formed; BET surface area, and total pore volume are increased by 1.6 and 3.1 times, respectively. Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5 synthesized with different Fe-BTC ratios and different pore size distributions possess different H<sub>2</sub> adsorption capacities. The highest H<sub>2</sub> adsorption capacity belongs to the hierarchically porous Fe-BTC that possesses ultramicropores in its pore structure (1.10 wt.% at 7.6 bar and 298 K). The presence of ultramicropores increases the H<sub>2</sub> adsorption capacity by 2.6 times which signifies the role of ultramicropores on the adsorbed H<sub>2</sub> amount. Here we report a study that suggests a way to enhance H<sub>2</sub> adsorption capacity of Fe-BTC via forming ultramicropores in its pore structure. By this study, not only the H<sub>2</sub>

adsorption capacity of Fe-BTC has been increased, but also the role of ultramicropores on the H<sub>2</sub> adsorption capacity has been shown experimentally (Aysu Yurduşen, Yürüm, & Yürüm, 2020a).

## **7.2. Experimental**

### **7.2.1. Materials**

Purchased chemicals were not further treated prior to their use. Iron(III) chloride hexahydrate (FeCl<sub>3</sub>·6H<sub>2</sub>O) (ACS Reagent Grade, 98% pure) was purchased from Merck Millipore, benzene-1,3,5-tricarboxylic acid (95% pure), N,N-Dimethylformamide (DMF) (99% pure, HPLC grade), and methanol (99.8% pure) were purchased from Sigma Aldrich.

### **7.2.2. Synthesis of Hierarchically Porous Fe-BTCs**

3.1 mmol of FeCl<sub>3</sub>·6H<sub>2</sub>O, benzene-1,3,5-tricarboxylic acid (3.1 mmol or 1.03 mmol or 0.62 mmol) and 80 mL of N, N-Dimethylformamide (DMF) were mixed vigorously via a magnetic stirrer with a stirring rate of 800 rpm for an hour at 25 °C. A clear solution of FeCl<sub>3</sub>·6H<sub>2</sub>O, benzene-1,3,5-tricarboxylic acid and DMF was obtained at the end of the first hour. Prepared clear solution was poured into glass vials (20 mL) capped with Teflon caps and then heated in an isothermal oven for 2 days at 150 °C. After two days of heating, precipitates were formed. Precipitates and the solution were transferred into falcon tubes (50 mL). Precipitates and the solution were washed with DMF (3 days) and methanol (3 days) for 6 days. Finally, the precipitates were dried under vacuum for 30 hours at 100 °C. Figure 151 is the schematic representation of the experimental procedure and Table 48 represents the sample abbreviations of Fe-BTC synthesized with different Fe:BTC ratio.

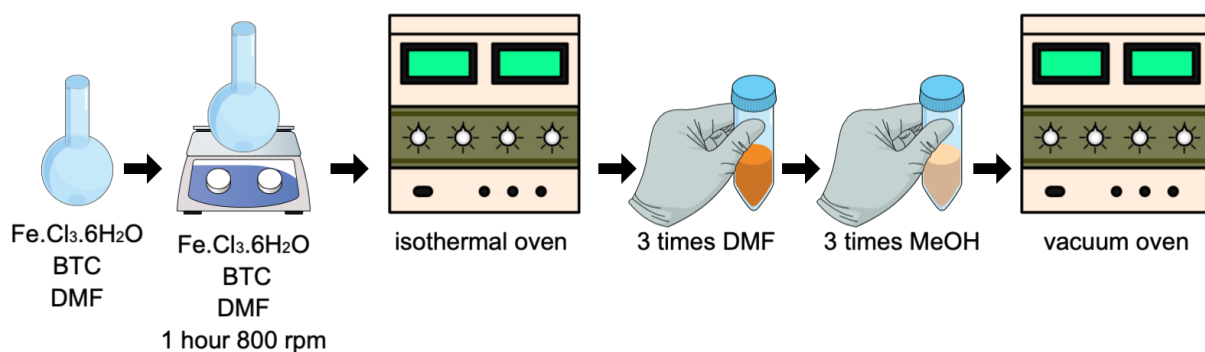


Figure 151. Schematic representation of experimental procedure.

Table 48. Sample abbreviations of hierarchically porous Fe-BTCs synthesized with different Fe:BTC ratio

| Sample Abbreviation | Fe:BTC ratio (mmol/mmol) <sup>[a]</sup> |
|---------------------|-----------------------------------------|
| Fe-BTC-1            | 1:1                                     |
| Fe-BTC-3            | 3:1                                     |
| Fe-BTC-5            | 5:1                                     |

<sup>[a]</sup> (mmol FeCl<sub>3</sub>.6H<sub>2</sub>O) (mmol BTC)

### 7.2.3. Characterization Analysis

#### 7.2.3.1.X-Ray diffraction

A Bruker D2 Phaser XRD was used in X-ray diffraction analysis. X-ray diffraction analysis was conducted in between a  $2\theta$  range of 2 to 90° with a step size of 0.02°.

#### 7.2.3.2.Scanning electron microscopy (SEM)

For SEM analysis a Leo Supra 35VP field emission scanning electron microscope was used. Fe-BTC-1, and Fe-BTC-3 were imaged while the voltage value was set to 3 kV and working distance was set to 8.1 mm. In the meanwhile, Fe-BTC-5 was imaged while the voltage was set to 1.5 kV and working distance was set to 8.3 mm.

#### **7.2.3.3. Brunauer-Emmett-Teller (BET) surface area and pore size distribution analysis**

A Micromeritics 3Flex Instrument was used in BET surface area and pore size distribution analysis. Prior to each analysis  $0.35 \pm 0.05$  grams (g) of Fe-BTC was degassed at 120 °C for 6 hours. For surface area measurements BET model; for micropore volume estimations t-plot method and NLDFT method, and for pore size distribution analysis NLDFT method was used.

#### **7.2.3.4. Fourier transform infrared spectroscopy (FT-IR) analysis**

FTIR analysis was conducted with A Thermo Scientific Nicolet Is10 in between the wavelengths of 600 to 4000  $\text{cm}^{-1}$ . Background noise was corrected, and scans were repeated for 32 times.

#### **7.2.3.5. Thermogravimetric analysis (TGA)**

A TG-DTA (Shimadzu DTG-60H simultaneous thermal analysis) was used to measure the mass losses. Fe-BTCs were heated from 25 °C to 1200 °C under a  $\text{N}_2$  flow (20 mL/min) with the step size of 10 K/min.

#### **7.2.3.6. $\text{H}_2$ sorption studies**

An Intelligent Gravimetric Analyzer (IGA) was used to measure the adsorbed  $\text{H}_2$  amount.  $\text{H}_2$  adsorption studies were conducted at room temperature (298 K) in between 0 and 8 bar. A stainless-steel vacuum pressure reactor ( $\pm 1.0 \mu\text{g}$  sensitivity) was used for a precise measurement. Prior to  $\text{H}_2$  adsorption studies, Fe-BTCs were outgassed for 6 hours at 120 °C.

### 7.3. Results and Discussion

#### 7.3.1. XRD Analysis

Figure 152 illustrates the XRD patterns of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5. Single crystal X-ray crystallography analyses showed that micro-sized single crystals were not formed and there were no metallic-iron present.

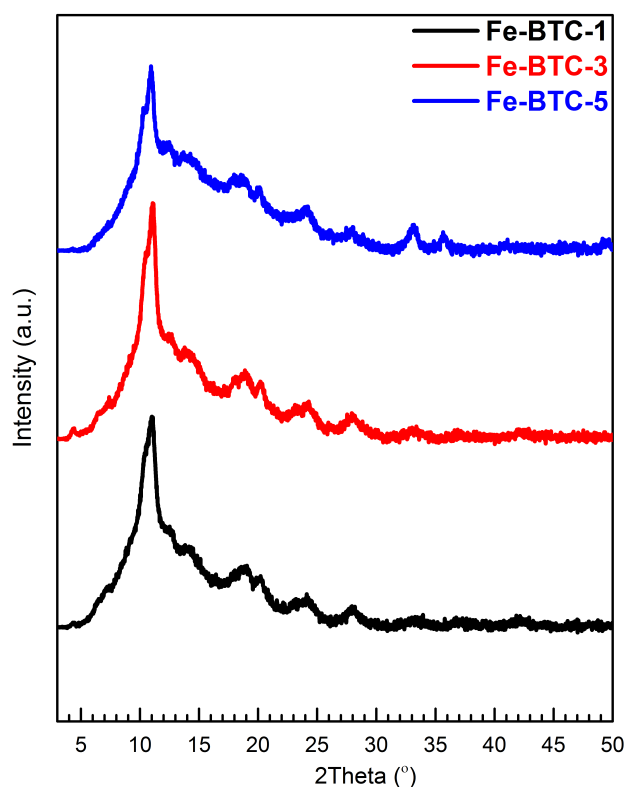


Figure 152. XRD patterns of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5.

XRD patterns of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5 matched well with the XRD pattern of Basolite F300. The well matched XRD patterns revealed that by the perturbation assisted nanofusion synthesis strategy Basolite F300 like Fe-BTCs were synthesized successfully.

The broad Bragg peaks and low intensities confirmed that the synthesized Fe-BTCs possess a disordered nature. In addition to the disordered nature of Fe-BTC, nanocrystal building units formed by the perturbation assisted nanofusion synthesis strategy lead to

broadening in the PXRD patterns. Therefore, we have attributed the broadening in the PXRD patterns to the i) disordered nature of Fe-BTC; and ii) the nanosized Fe-BTC crystals.

### 7.3.2. SEM Images

Figure 153-155 illustrates the SEM images of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5, respectively.

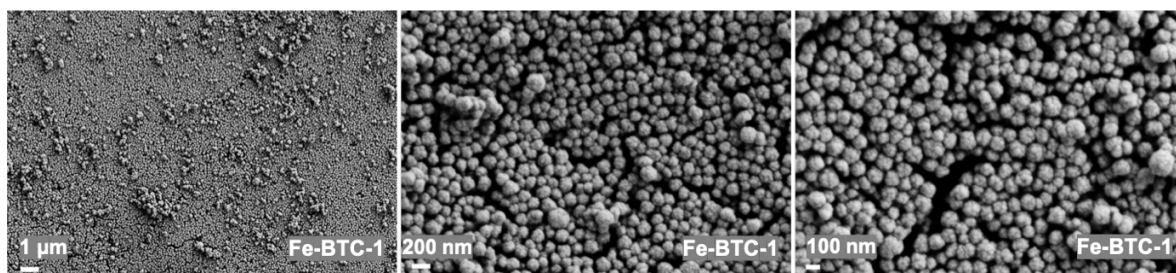


Figure 153. SEM images of Fe-BTC-1.

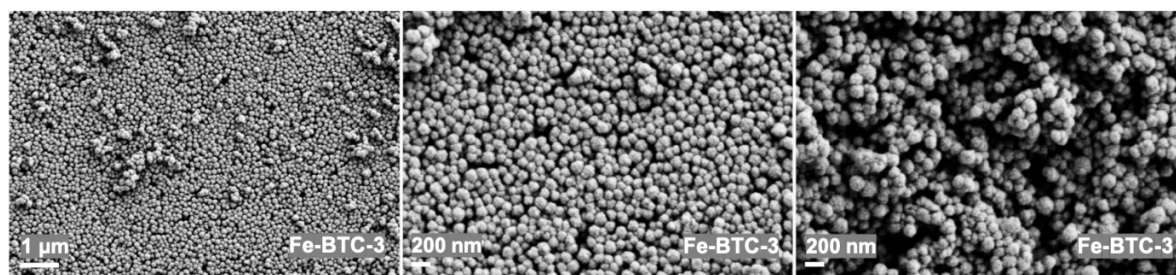


Figure 154. SEM images of Fe-BTC-3.

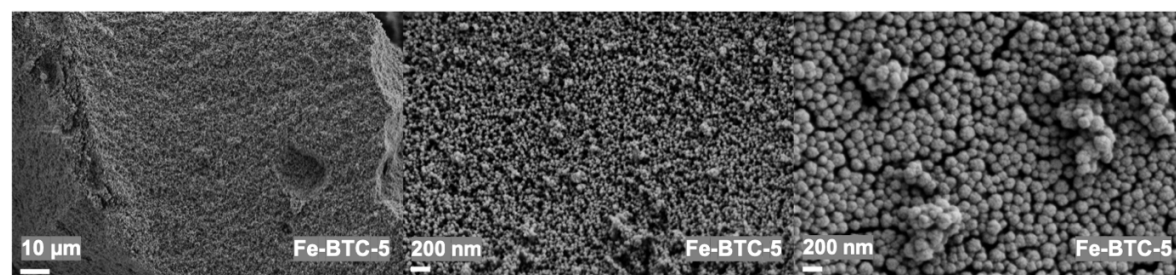


Figure 155. SEM images of Fe-BTC-5.

SEM images of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5 illustrate that Fe-BTCs synthesized via a perturbation assisted nanofusion synthesis strategy i) have an interconnected highly porous structure, and ii) were formed of aggregated nanosized crystallites.

Vigorous stirring of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ , BTC, and DMF prevented the single crystal formation. SBUs aggregate into nanosized Fe-BTC crystallites which were embedded on an amorphous matrix which can be clearly seen in the SEM images.

The nanosized Fe-BTC crystallites embed on an amorphous matrix and textural mesopores form spontaneously from the self-assembly of the nanosized Fe-BTC crystallites. The amorphous matrix and the interparticle voids created in between the aggregated nanosized Fe-BTCs can be clearly seen in the SEM images of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5.

### 7.3.3. $\text{N}_2$ Sorption Isotherms

$\text{N}_2$  sorption isotherms of Fe-BTC-1, Fe-BTC-3 and Fe-BTC-5 are shown in Figure 156-157.

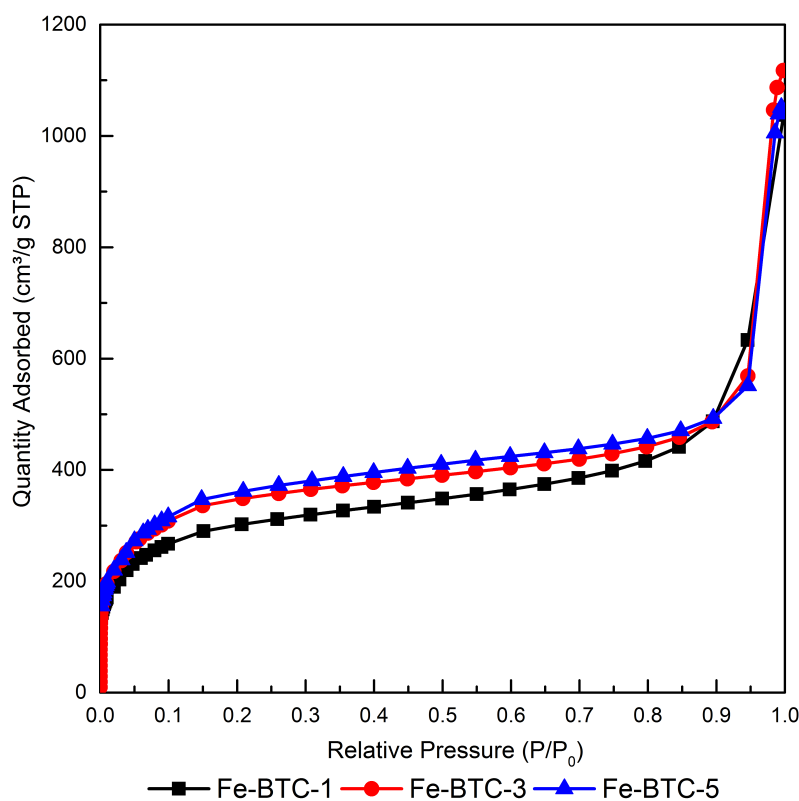


Figure 156.  $\text{N}_2$  sorption isotherms of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5.



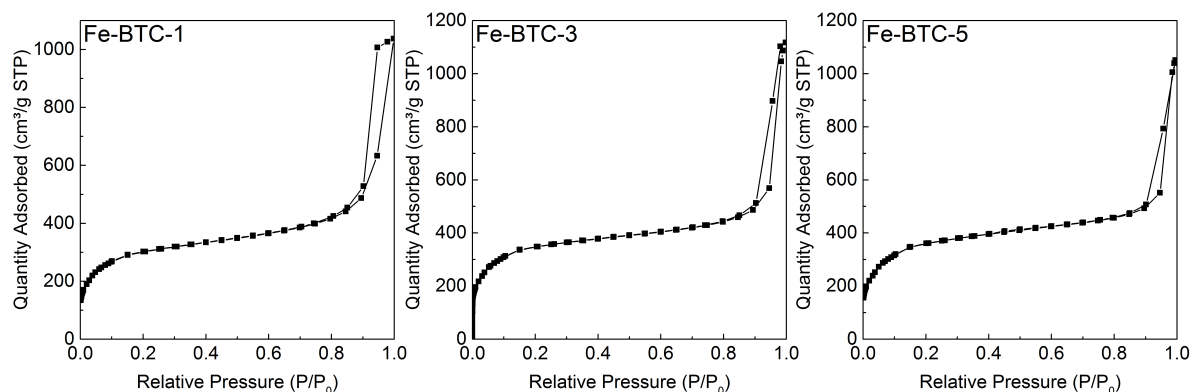


Figure 157. N<sub>2</sub> sorption isotherms of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5.

N<sub>2</sub> sorption isotherms of hierarchically porous Fe-BTCs synthesized with different Fe:BTC ratio follow the features of IUPAC Type IV isotherms with some microporosity present. High N<sub>2</sub> uptakes at low pressures ( $P/P_0 < 0.1$ ) are attributed to micropores present in the pore structure. Slope observed in between the relative pressures of 0.2 and 0.9 is a consequence of mesopore filling. Lastly, the high N<sub>2</sub> uptakes at pressures close to saturation pressure ( $P/P_0 > 0.9$ ) are a consequence of the mesopores (pore sizes ranging in between 42 to 50 nm) present in the pore structure. Table 49 illustrates the BET surface area ( $m^2/g$ ), and the total pore volume ( $cm^3/g$ ) of the synthesized Fe-BTCs.

Table 49. BET surface area ( $m^2/g$ ) and total pore volume ( $cm^3/g$ ) of Fe-BTCs

| Fe-BTC   | BET surface area ( $m^2/g$ ) | Total pore volume ( $cm^3/g$ ) |
|----------|------------------------------|--------------------------------|
| Fe-BTC-1 | 1139.1 $\pm$ 2.1E1           | 1.29 $\pm$ 6.4E-2              |
| Fe-BTC-3 | 1312.7 $\pm$ 1.1E1           | 1.41 $\pm$ 5.7E-2              |
| Fe-BTC-5 | 1355.9 $\pm$ 4.2E1           | 1.34 $\pm$ 2.6E-1              |

Reported BET surface, and total pore volume of Fe-BTC-1, Fe-BTC-3 and Fe-BTC-5 are higher than those of reported BET surface, and total pore volume of Fe-BTCs (Dhakshinamoorthy, Alvaro, Chevreau, et al., 2012; Dhakshinamoorthy et al., 2011; Dhakshinamoorthy, Alvaro, & Garcia, 2012; X. Hu et al., 2016; Majano et al., 2013; Opanasenko et al., 2013; Torres et al., 2018; Zukal et al., 2015). By synthesizing hierarchically porous Fe-BTCs via a perturbation assisted nanofusion synthesis strategy, hierarchical pores were formed. Introducing hierarchical pores enhanced the BET surface area, and the total pore volume of Fe-BTC.

### 7.3.4. t-plot Method

t-plot method is used to estimate the micropore volume (Lowell et al., 2004a). t-plots of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5 can be found in Figure 158 and Table 50 represents the micro- and mesopore areas, fraction of microporosities and micropore volumes estimated by t-plot method.

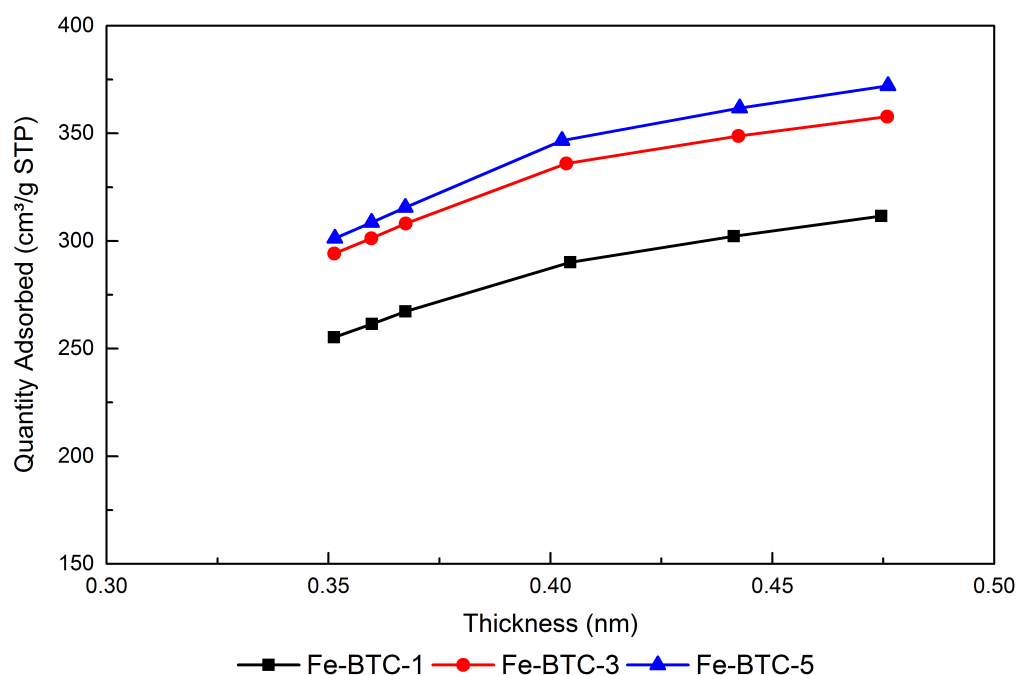


Figure 158. t-plots of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5.

Table 50. Micro-, and mesopore area, micropore to total pore area fraction and micropore volume estimated by t-plot method

| Hierarchically porous Fe-BTCs | S <sub>micro</sub> (m <sup>2</sup> /g) | S <sub>meso</sub> (m <sup>2</sup> /g) | S <sub>micro</sub> (%) | V <sub>micro</sub> (cm <sup>3</sup> /g) |
|-------------------------------|----------------------------------------|---------------------------------------|------------------------|-----------------------------------------|
| Fe-BTC-1                      | 425.5±5.3E1                            | 713.6±7.4E1                           | 37.4                   | 0.151±2.6-2                             |
| Fe-BTC-3                      | 509.6±6.0E-1                           | 803.2±1.2E1                           | 38.8                   | 0.181                                   |
| Fe-BTC-5                      | 458.7±1.5E2                            | 897.2±7.7                             | 33.8                   | 0.159±7.8E-2                            |

t-plots of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5 are formed of two linear parts which deviated towards downwards. Deviations illustrated the presence of micropores. Different micropore volumes were estimated for hierarchically porous Fe-BTCs synthesized with

different Fe:BTC ratios and the highest micropore volume belongs to Fe-BTC-3 which is 1.2, and 1.14 times greater than the micropore volume of Fe-BTC-1 and Fe-BTC-5, respectively.

### 7.3.5. NLDFT Method

Figure 159 shows the incremental pore volume versus pore width plots of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5 and Table 51 illustrates the pore volumes of narrow micropores, micropores, mesopores, upper mesopores, total pore volume, and fraction of microporosity.

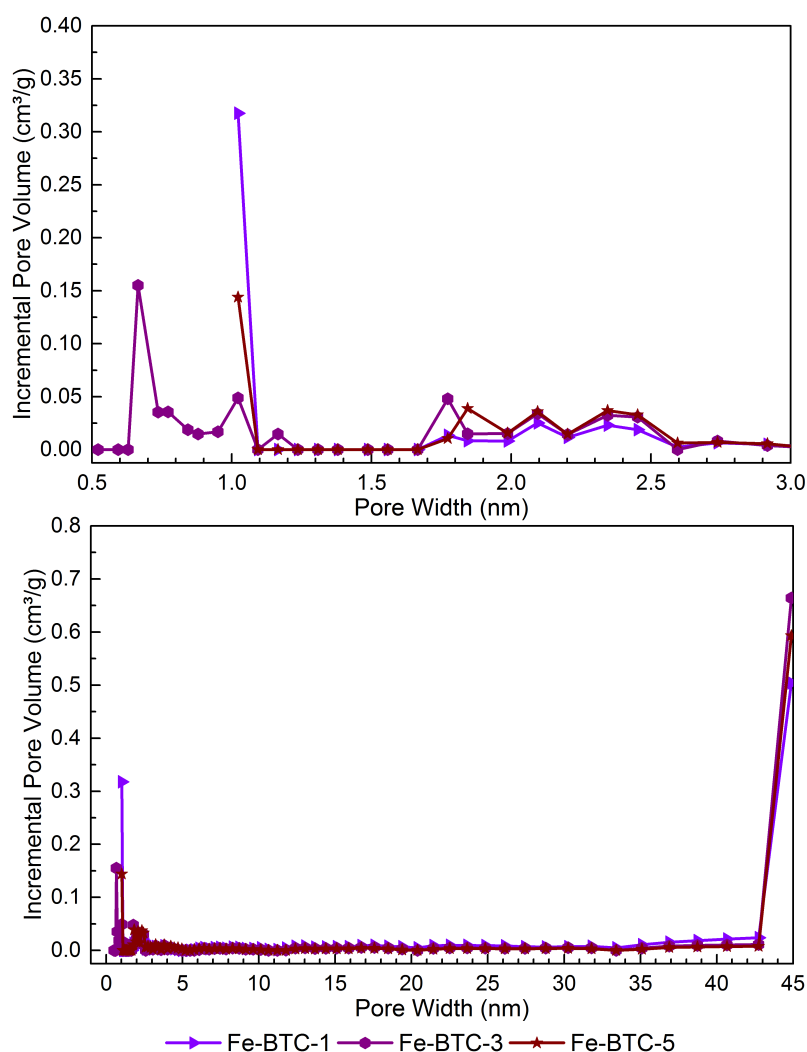


Figure 159. NLDFT plots of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5.

Table 51. Narrow micro-, micro-, uppermeso-, meso- and total pore volume estimated by NLDFT method

|          | Vpores <1 nm<br>(cm <sup>3</sup> /g) | Vmicro<br>(cm <sup>3</sup> /g) | Vuppermeso<br>(cm <sup>3</sup> /g) | Vmeso<br>(cm <sup>3</sup> /g) | Vtotal<br>(cm <sup>3</sup> /g) | Vmicro<br>(%) |
|----------|--------------------------------------|--------------------------------|------------------------------------|-------------------------------|--------------------------------|---------------|
| Fe-BTC-1 | 0.318±8.3E-3                         | 0.373±8.1E-3                   | 0.504±8.7E-2                       | 0.917±6.5E-2                  | 1.29±6.4E-2                    | 28.9          |
| Fe-BTC-3 | 0.326±4.0E-3                         | 0.453±6.3E-3                   | 0.664±4.3E-2                       | 0.957±6.3E-2                  | 1.41±5.7E-2                    | 32.1          |
| Fe-BTC-5 | 0.367±0.0148                         | 0.468±3.0E-2                   | 0.59±2.8E-1                        | 0.872±2.9E-1                  | 1.34±2.6E-1                    | 34.9          |

The highest micropore volume belongs to Fe-BTC-5 while the fraction of microporosity of Fe-BTC-3 and Fe-BTC-5 are estimated to be similar. The micropore volume of Fe-BTC-5 is 1.25 and 1.03 times higher than the micropore volume of Fe-BTC-1, and Fe-BTC-3, respectively. Volume of narrow micropores present in Fe-BTC-5 is 1.15 and 1.13 times higher than the volume of narrow micropores present in Fe-BTC-1, and Fe-BTC-3, respectively. The highest total pore volume belongs to Fe-BTC-3 (1.41 cm<sup>3</sup>/g) while the lowest total pore volume belongs to Fe-BTC-1.

### 7.3.6. FTIR Analysis

FTIR spectra of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5 are provided in Figure 160 while Table 52 shows the FTIR frequencies of Fe-BTCs. FTIR spectra of the synthesized Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5 match well with the FTIR spectrum of the commercial Basolite F300 reported in the literature.

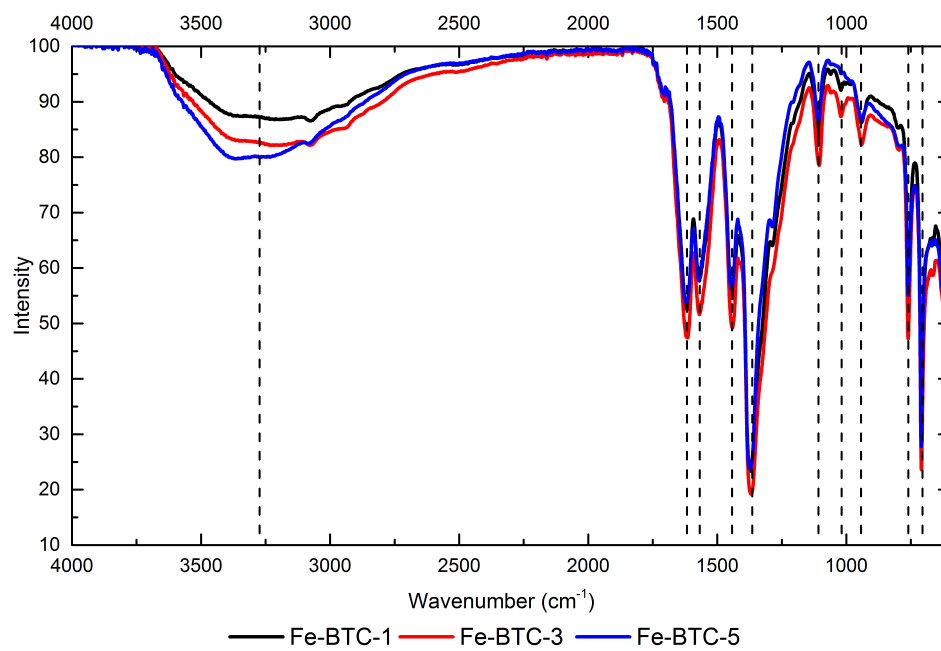


Figure 160. FTIR spectra of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5.

Table 52. FTIR frequencies of Fe-BTCs

|                  | Fe-BTC-1              | Fe-BTC-3              | Fe-BTC -5             | Assigned mode                               | Reference             |
|------------------|-----------------------|-----------------------|-----------------------|---------------------------------------------|-----------------------|
| 1 <sup>st</sup>  | 3075 cm <sup>-1</sup> | 3232 cm <sup>-1</sup> | 3367 cm <sup>-1</sup> | O-H bond stretching                         | (Torres et al., 2018) |
| 2 <sup>nd</sup>  | 1616 cm <sup>-1</sup> | 1615 cm <sup>-1</sup> | 1621 cm <sup>-1</sup> | asymmetric (COO) stretching mode            | (Dhumal et al., 2016) |
| 3 <sup>rd</sup>  | 1569 cm <sup>-1</sup> | 1569 cm <sup>-1</sup> | 1569 cm <sup>-1</sup> | H <sub>2</sub> O bending mode               | (X. Hu et al., 2016)  |
| 4 <sup>th</sup>  | 1442 cm <sup>-1</sup> | 1441 cm <sup>-1</sup> | 1445 cm <sup>-1</sup> | asymmetric (COO) stretching mode            | (Dhumal et al., 2016) |
| 5 <sup>th</sup>  | 1370 cm <sup>-1</sup> | 1367 cm <sup>-1</sup> | 1374 cm <sup>-1</sup> | symmetric (COO) stretching mode             | (Dhumal et al., 2016) |
| 6 <sup>th</sup>  | 1105 cm <sup>-1</sup> | 1105 cm <sup>-1</sup> | 1107 cm <sup>-1</sup> | C-O-Fe stretching, skeletal modes of Fe-BTC | (X. Hu et al., 2016)  |
| 7 <sup>th</sup>  | 942 cm <sup>-1</sup>  | 941 cm <sup>-1</sup>  | 941 cm <sup>-1</sup>  | Trimesate bands                             | (X. Hu et al., 2016)  |
| 8 <sup>th</sup>  | 761 cm <sup>-1</sup>  | 760 cm <sup>-1</sup>  | 760 cm <sup>-1</sup>  | Fe-O stretching mode                        |                       |
| 9 <sup>th</sup>  | 709 cm <sup>-1</sup>  | 709 cm <sup>-1</sup>  | 709 cm <sup>-1</sup>  | Fe-O stretching mode                        |                       |
| 10 <sup>th</sup> | 618 cm <sup>-1</sup>  | 619 cm <sup>-1</sup>  | 621 cm <sup>-1</sup>  | Central oxygen in single Fe <sub>3</sub> O  | (Vuong et al., 2013a) |

Broad bands in between 3000 and 3400 cm<sup>-1</sup> are assigned to OH groups. Peaks at 1370, 1441, 1569, and 1621 cm<sup>-1</sup> prove that BTC was successfully attached to Fe. The peaks at 1569 and 1621 cm<sup>-1</sup> illustrates that Fe sites are coordinated with water molecules. The characteristic peaks of carboxylate symmetric stretching mode, 1375 and 1450 cm<sup>-1</sup>, issues a shift to 1369 and 1440 cm<sup>-1</sup> which is a consequence of bond elongation. The peaks present at 941 and 1105 cm<sup>-1</sup> indicate that C-H in-plane and out-of-plane bending modes are present in the structure of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5. The peak at 612 cm<sup>-1</sup> is attributed

central oxygen in single  $\text{Fe}_3\text{O}$ . The characteristic peaks of Basolite F300 structure, 709 and  $760\text{ cm}^{-1}$ , confirm that a Basolite F300 like Fe-BTC was synthesized by the perturbation assisted nanofusion synthesis strategy. Moreover, FTIR spectrum of hierarchically porous Fe-BTCs were compared with the FTIR spectra of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ . None of the peaks observed in the FTIR spectra of  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$  ( $842\text{ cm}^{-1}$ ,  $1594\text{ cm}^{-1}$ ,  $2993\text{ cm}^{-1}$ ,  $3212\text{ cm}^{-1}$ , and  $3523\text{ cm}^{-1}$ ) were observed in the FTIR spectrum of hierarchically porous Fe-BTCs which proves that there are no metallic iron present.

### 7.3.7. TGA

Figure 161 illustrates the TGA curves of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5. A detailed representation of TGA analysis can be found in Table 53 and 54.

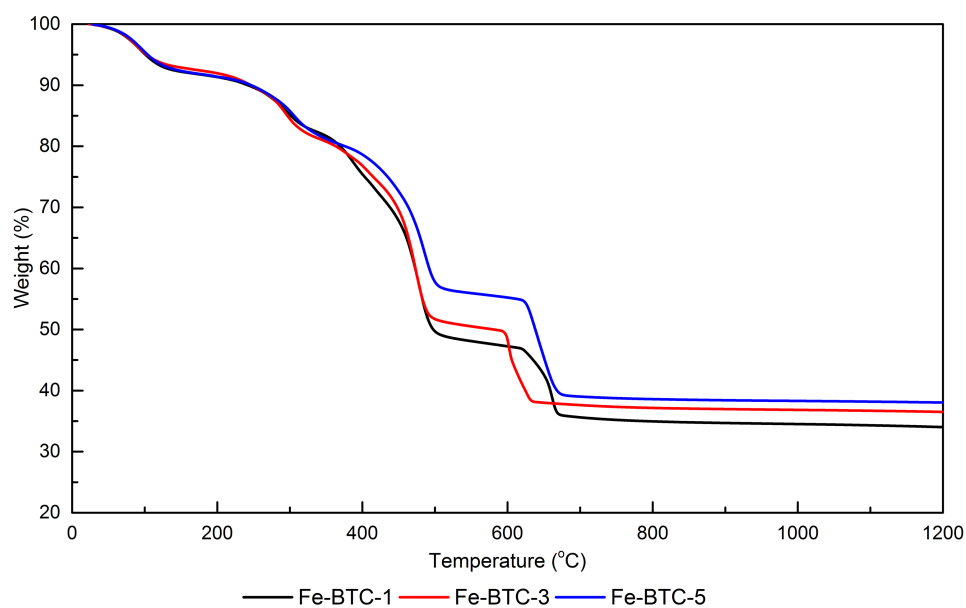


Figure 161. TGA curve of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5.

Table 53. % mass loss during TGA analysis of Fe-BTC synthesized at 150 °C.

| Temperature Range (°C) | Fe-BTC-1 (%) | Temperature Range (°C) | Fe-BTC-3 (%) | Temperature Range (°C) | Fe-BTC-5 (%) |
|------------------------|--------------|------------------------|--------------|------------------------|--------------|
| 25-179                 | -8.3         | 25-168                 | -7.4         | 25-178                 | -8.2         |
| 179-334                | -9.2         | 168-342                | -11.4        | 178-374                | -11.7        |
| 334-556                | -34.5        | 342-547                | -30.6        | 374-570                | -24.4        |
| 556-776                | -13.0        | 547-754                | -13.2        | 570-766                | -17.0        |

Table 54. Percent residual mass at the end of TGA.

|                   | Fe-BTC-1 | Fe-BTC-3 | Fe-BTC-5 |
|-------------------|----------|----------|----------|
| Residual Mass (%) | 35       | 37.4     | 38.7     |

Four main losses occurred when Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5 were heated to 1200 °C under N<sub>2</sub> environment. The first mass loss is a consequence of the removal of adsorbed and coordinated water molecules. The second mass loss is a consequence of the removal of the trapped solvent molecules. The third mass loss occurs as a consequence of BTC decomposition which determines the stability of Fe-BTC structure. The fourth and the last mass loss is a consequence of the decomposition of the carboxylates.

Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5 decomposed at 334, 342, and 374 °C, respectively. The highest thermal stability belongs to Fe-BTC-5 which was synthesized with the least amount of BTC. To the best of our knowledge, Fe-BTC-5 possesses a higher thermal stability than those of Fe-BTC reported in literature, so far (X. Hu et al., 2016; Majano et al., 2013; Torres et al., 2018). Moreover, TGA analysis show that Fe-BTCs synthesized in this study are thermally stable under adsorption process conditions.

### 7.3.8. H<sub>2</sub> Adsorption Studies

Figure 162 illustrates the H<sub>2</sub> sorption capacities of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5. The different H<sub>2</sub> sorption capacities of Fe-BTCs synthesized with different Fe:BTC ratio (Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5) are found to be dependent on the pore size distribution and textural properties of Fe-BTC. Langmuir and Freundlich models were



investigated for the best fit and respective isotherm parameters, respective equations, and  $R^2$  values are provided below.

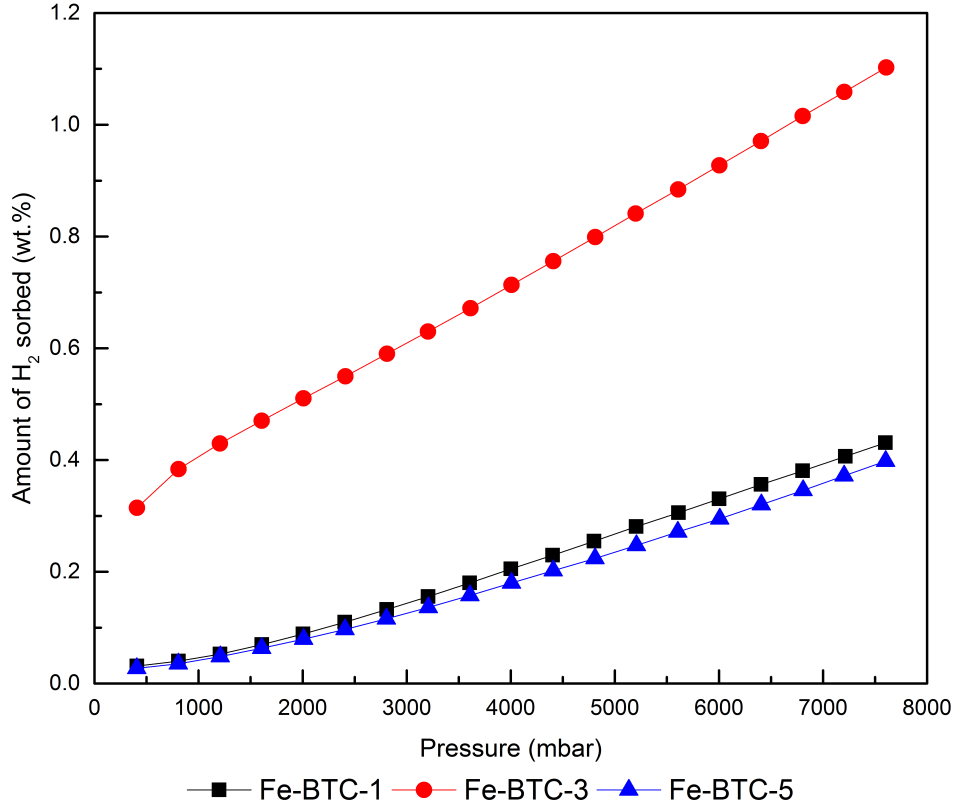


Figure 162.  $H_2$  sorption isotherms (298 K) of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5.

**Langmuir Model:**

$$\frac{C_e}{q_e} = \frac{1}{KQ^0} + \frac{C_e}{Q^0} \quad (7.1)$$

**Freundlich Model:**

$$\log q_e = \log K_F + \frac{1}{n} \log C_e \quad (7.2)$$

Table 55. Respective equations obtained from models

| Hierarchically porous Fe-BTCs | Langmuir Model                            | Freundlich Model                         |
|-------------------------------|-------------------------------------------|------------------------------------------|
| Fe-BTC-1                      | $y = -0.0835x + 4256.9$<br>$R^2 = 0.1534$ | $y = 1.0027x - 3.5996$<br>$R^2 = 0.9746$ |
| Fe-BTC-3                      | $y = 0.1428x + 453.16$<br>$R^2 = 0.9009$  | $y = 0.4454x - 1.0347$<br>$R^2 = 0.9639$ |
| Fe-BTC-5                      | $y = -0.1035x + 4819.7$<br>$R^2 = 0.185$  | $y = 1.0068x - 3.6643$<br>$R^2 = 0.9746$ |

Table 56. Langmuir and Freundlich isotherm parameters

| Hierarchically porous Fe-BTCs | Langmuir                                                                             | Freundlich                                                               |
|-------------------------------|--------------------------------------------------------------------------------------|--------------------------------------------------------------------------|
| Fe-BTC-1                      | $Q_m = 11.98 \text{ mg/g}$<br>$K_a = 1.96\text{E-}05 \text{ mg-}1$<br>$R^2 = 0.1534$ | $K_F = 2.5\text{E-}04 \text{ mg/g}$<br>$\eta_F = 0.99$<br>$R^2 = 0.9746$ |
| Fe-BTC-3                      | $Q_m = 7.0 \text{ mg/g}$<br>$K_a = 3.15\text{E-}04 \text{ mg-}1$<br>$R^2 = 0.9009$   | $K_F = 9.2\text{E-}02 \text{ mg/g}$<br>$\eta_F = 2.25$<br>$R^2 = 0.9639$ |
| Fe-BTC-5                      | $Q_m = 9.66 \text{ mg/g}$<br>$K_a = 2.15\text{E-}05 \text{ mg-}1$<br>$R^2 = 0.185$   | $K_F = 2.2\text{E-}04 \text{ mg/g}$<br>$\eta_F = 0.99$<br>$R^2 = 0.9746$ |

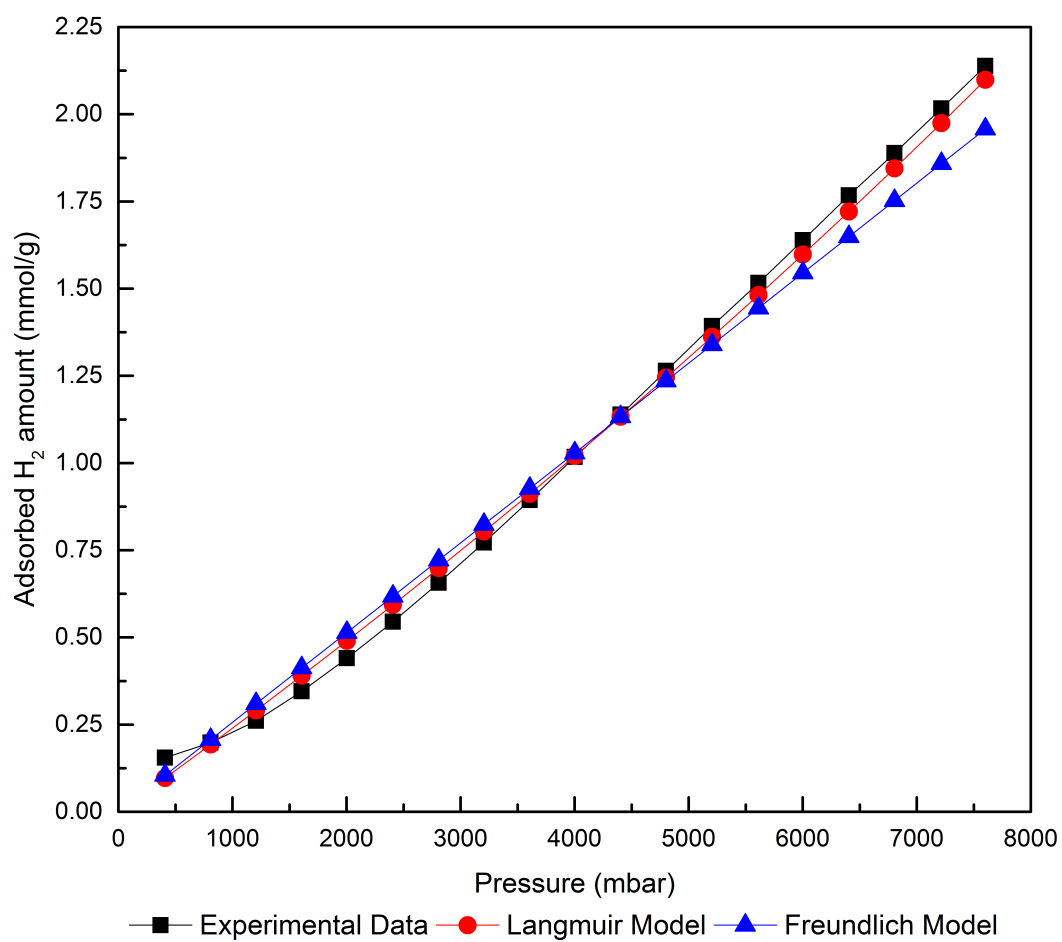


Figure 163. Comparison of the experimental and the estimated data (Fe-BTC-1).

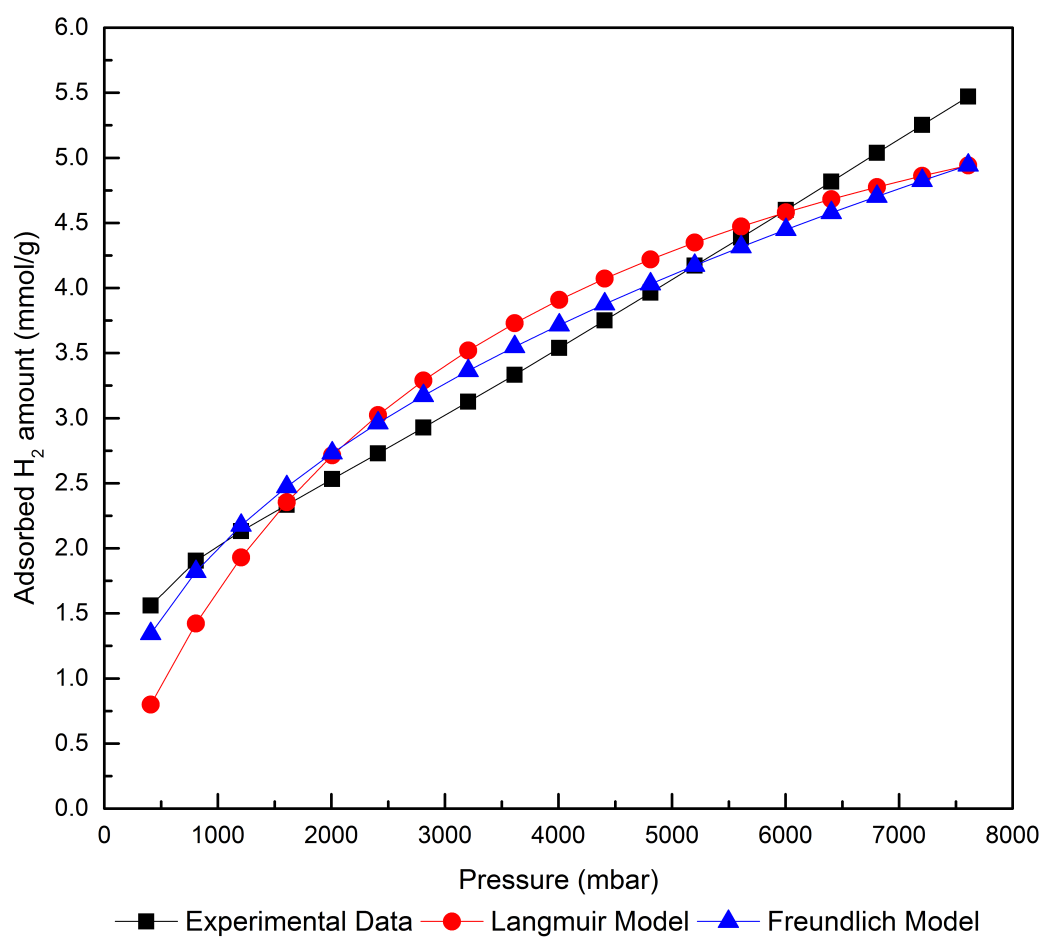


Figure 164. Comparison of the experimental and the estimated data (Fe-BTC-3).

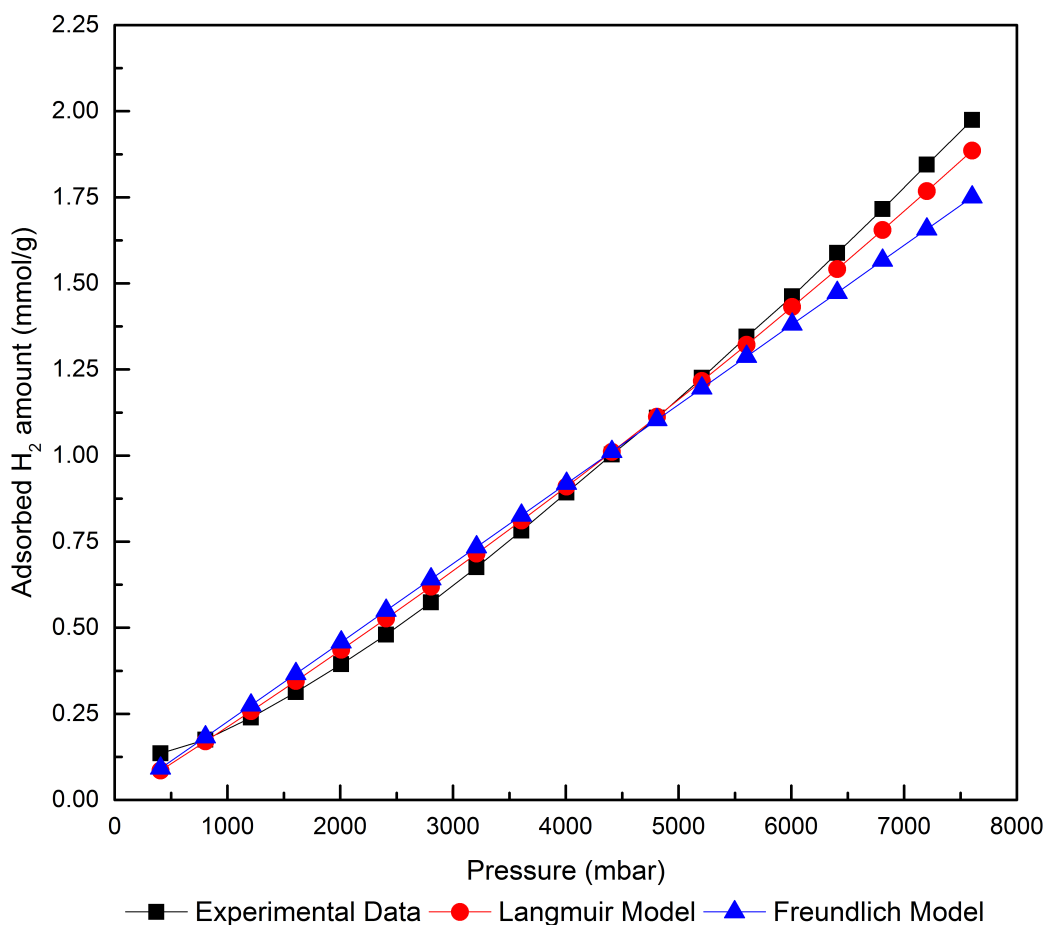


Figure 165. Comparison of the experimental and the estimated data (Fe-BTC-5).

Langmuir and Freundlich isotherm parameters show that Freundlich model describes the H<sub>2</sub> adsorption behavior (at 298 K) of hierarchically porous Fe-BTCs better. However, as the adsorption studies were conducted till 8 bars, the shape of the isotherm may be misleading.

The highest H<sub>2</sub> adsorption capacity belongs to Fe-BTC-3 while Fe-BTC-1 (2.56 times lower), and Fe-BTC-5 (2.82 times lower) possess a significantly lower H<sub>2</sub> adsorption capacities than Fe-BTC-3. The significant differences in H<sub>2</sub> sorption capacities are attributed to different pore size distribution of hierarchically porous Fe-BTCs synthesized with different Fe:BTC ratio. Table 57 illustrates BET surface area, volume of ultramicro-, narrow micro-, micropores and H<sub>2</sub> sorption capacities of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5 measured at 7.6 bar and 298 K. Figure 166 shows the narrow micro-, and micropore volume of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5.

Table 57. BET surface area, ultramicro-, narrow micro-, micropore volume, volume fraction of narrow micro- to micropores, and H<sub>2</sub> adsorption capacities of Fe-BTCs

|          | BET Surface Area (m <sup>2</sup> /g) | Vpores < 0.7 nm (cm <sup>3</sup> /g) | Vpores < 1 nm (cm <sup>3</sup> /g) | Vpores < 2 nm (cm <sup>3</sup> /g) | V<1nm/V<2nm | H <sub>2</sub> adsorption capacity (wt.%) [a] |
|----------|--------------------------------------|--------------------------------------|------------------------------------|------------------------------------|-------------|-----------------------------------------------|
| Fe-BTC-1 | 1139.1±2.1E1                         | -                                    | 0.318±8.3E-3                       | 0.373±8.1E-3                       | 85.3        | 0.43                                          |
| Fe-BTC-3 | 1312.7±1.1E1                         | 0.19                                 | 0.326±4.0E-3                       | 0.453±6.3E-3                       | 71.9        | 1.10                                          |
| Fe-BTC-5 | 1355.9±4.2E1                         | -                                    | 0.367±0.0148                       | 0.468±3.0E-2                       | 78.4        | 0.39                                          |

[a] Measured at 7.6 bar and 298 K

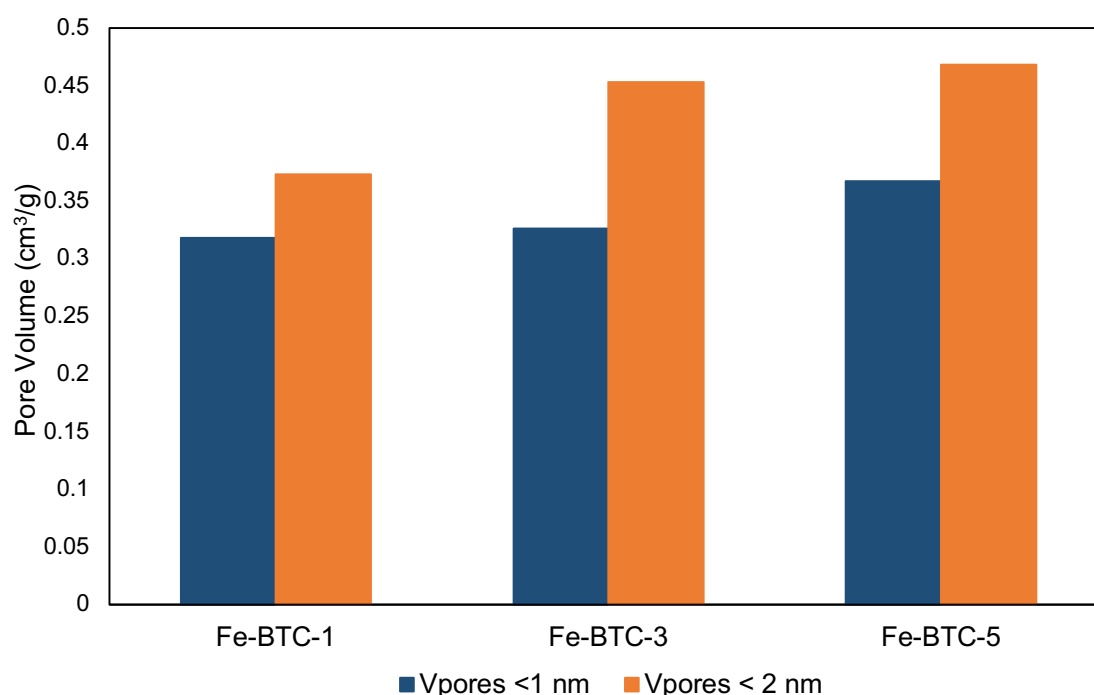


Figure 166. Volume of narrow- and micropores of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5

Despite its relatively low fraction (71.9%) of narrow micropores (volume of narrow micropores/volume of micropores), Fe-BTC-3 possesses the highest H<sub>2</sub> adsorption capacity among the hierarchically porous Fe-BTCs synthesized in this study. Interestingly, neither the narrow micropore volume nor the micropore volume of Fe-BTC-3 is higher than the narrow micropore volume or the micropore volume of Fe-BTC-5.

Remarkably, among the synthesized hierarchically porous Fe-BTCs, it is Fe-BTC-3 that possesses ultramicropores in its pore structure. Presence of ultramicropores enhances the H<sub>2</sub> adsorption capacity of Fe-BTC-3, and a H<sub>2</sub> adsorption capacity 2.6, and 2.8 times higher than Fe-BTC-1, and Fe-BTC-5 is achieved. This relatively high H<sub>2</sub> adsorption capacity of Fe-BTC-3 indicates the crucial effect of ultramicropores on the adsorbed H<sub>2</sub> amount. Figure 167 compares the H<sub>2</sub> adsorption capacities (7.6 bar and 298 K) and the narrow micropore volumes of Fe-BTC-1, and Fe-BTC-5.

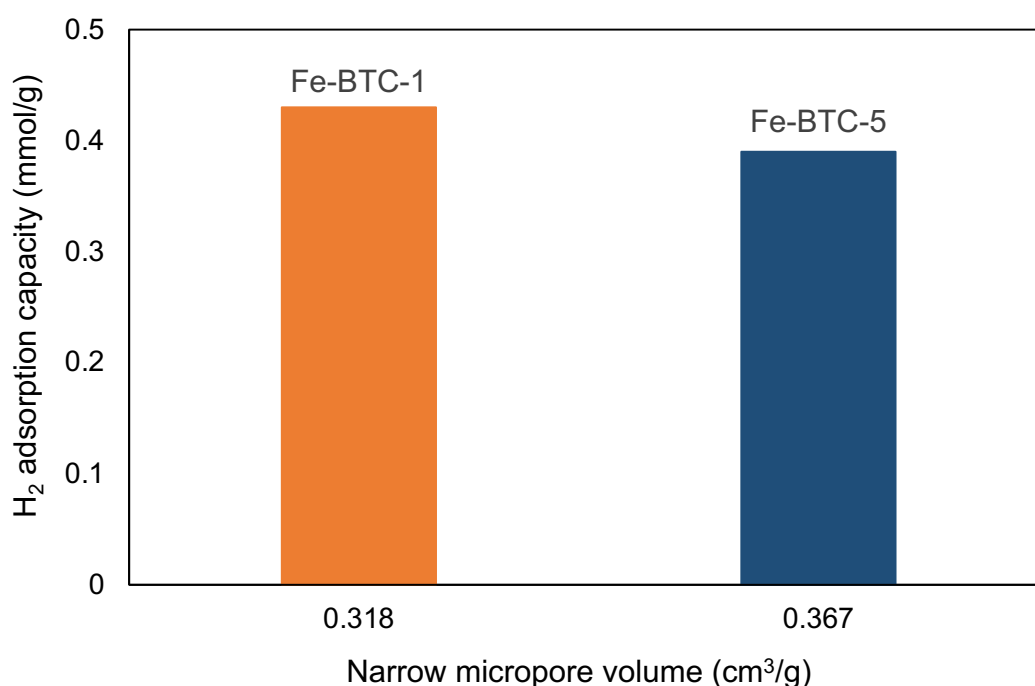


Figure 167. H<sub>2</sub> adsorption capacity (7.6 bar and 298 K) and narrow micropore volume of Fe-BTC-1 and Fe-BTC-5

Fe-BTC-1 which possesses a lower BET surface area (1.19 times), a lower narrow micropore (1.15 times), and a lower micropore volume (1.25 times) than Fe-BTC-5, possesses a H<sub>2</sub> adsorption capacity (0.43 wt.%) 1.1 times greater than Fe-BTC-5 (0.39 wt.%). We have attributed this relatively low H<sub>2</sub> adsorption capacity of Fe-BTC-5 to its lower fraction of narrow micropore volume through the micropore size distribution (narrow micropore volume/micropore volume). As the distribution of narrow micropores through the micropore size distribution becomes narrower, the adsorbed H<sub>2</sub> amount increases. Based on our results, we have attributed the differences in H<sub>2</sub> adsorption capacities to different pore size distributions of Fe-BTC-1, Fe-BTC-3, and Fe-BTC-5. Apparently, it is the pore size that

causes differences in the H<sub>2</sub> adsorption capacity. Revealed by theoretical studies, as pore diameters decrease below 1 nm, van der Waals interaction between the pores and the H<sub>2</sub> molecules strengthen and a higher adsorption potential is achieved (K. Xia, Gao, Wu, Song, & Ruan, 2007). In accordance with Lenard-Jones potential, the highest van der Waals potential is achieved by the pores with pore diameters of 6 to 8 Å (Schlichtenmayer & Hirscher, 2012). On the contrary, theoretical studies illustrate that when hydrogen is adsorbed on wider pores, a hydrogen layer forms on the walls located close to the pore walls and a less dense layer of hydrogen is adsorbed on the center of the pores which results in a lower H<sub>2</sub> adsorption capacity (Becher et al., 2003; Broom et al., 2019; Murray, Dincă, et al., 2009; Barbara Panella et al., 2005a; Schlichtenmayer & Hirscher, 2012, 2016; Schlichtenmayer et al., 2011).

In line with what has been reported in theoretical studies (Becher et al., 2003; Broom et al., 2019; Murray, Dincă, et al., 2009; Barbara Panella et al., 2005a; Schlichtenmayer & Hirscher, 2012, 2016; Schlichtenmayer et al., 2011), our results show that the presence of ultramicropores is the reason why an enhanced H<sub>2</sub> adsorption capacity is observed in Fe-BTC-3. Fe-BTC that has ultramicropores (Fe-BTC-3) in its pore structure possesses a larger adsorption potential and a higher H<sub>2</sub> adsorption capacity than Fe-BTC-1, and Fe-BTC-5. Figure 168 compares the H<sub>2</sub> adsorption capacities (7.6 bar and 298 K) and the narrow micropore volumes of Fe-BTCs. It is clear from Figure 168 that despite the lower narrow micropore volume of Fe-BTC-3, the highest H<sub>2</sub> adsorption capacity belongs to Fe-BTC-3. In line with our results and the theoretical studies conducted by other researchers (Becher et al., 2003; Broom et al., 2019; Murray, Dincă, et al., 2009; Barbara Panella et al., 2005a; Schlichtenmayer & Hirscher, 2012, 2016; Schlichtenmayer et al., 2011), we conclude that the adsorbed H<sub>2</sub> amount depends on: i) the pore size of the sorbent; ii) the presence of ultramicropores; and iii) the volume fraction of narrow micropores to micropores.



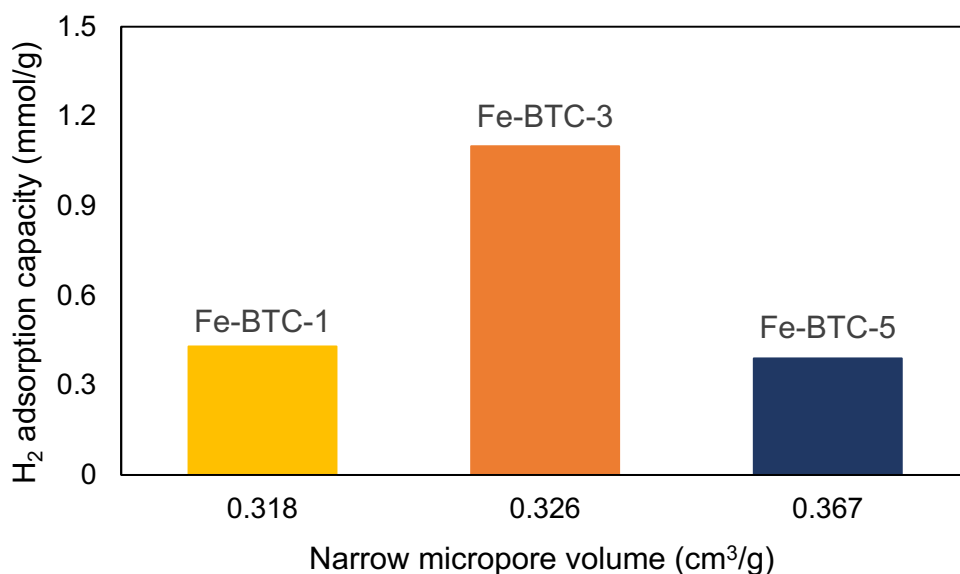


Figure 168. H<sub>2</sub> adsorption capacity (7.6 bar and 298 K) and the narrow micropore volume of Fe-BTCs

It has been reported that physisorption, which is the main adsorption mechanism in MOFs, is affected by the pore size heavily (Dinča et al., 2006; Michael Hirscher & Panella, 2007; Michael Hirscher et al., 2010; Latroche, Surblé, Serre, Mellot-Draznieks, Llewellyn, Lee, Chang, Sung, et al., 2006a; R. E. Morris & Wheatley, 2008; Murray, Dincă, et al., 2009; Barbara Panella et al., 2006, 2008; Schlichtenmayer et al., 2011; Schmitz et al., 2008). Bhatia and Myers showed that 15.1 kJ/mol of energy is thermodynamically needed for an adsorbent to store hydrogen at ambient temperature (Bhatia & Myers, 2006a). However, very weak interactions exist between the physisorbed H<sub>2</sub> molecules and MOFs, and the isosteric heat of adsorption has been found to be in between 4 to 7 kJ/mol (Dinča et al., 2006; R. E. Morris & Wheatley, 2008) meaning that cryogenic temperatures are necessary to adsorb considerable amount of H<sub>2</sub>. To increase the isosteric heat of adsorption of H<sub>2</sub> binding at ambient temperature two strategies were suggested: i) forming narrow pores within the framework of MOFs (Dinča et al., 2006; Michael Hirscher & Panella, 2007; Michael Hirscher et al., 2010; Y. H. Hu & Zhang, 2010; Latroche, Surblé, Serre, Mellot-Draznieks, Llewellyn, Lee, Chang, Sung, et al., 2006b; R. E. Morris & Wheatley, 2008; Barbara Panella et al., 2008; Schmitz et al., 2008); and ii) the presence of unsaturated metal sites (Dinča et al., 2006; Dincă & Long, 2005). In one of the studies it was figured out that the desorption temperature increases with the decrease in the pore size (Barbara Panella et al., 2008). Moreover, it was shown that the

desorption temperature and the pore size was directly correlated since the hydrogen adsorbed in the larger pores were desorbed at lower temperatures while the hydrogen adsorbed in the narrower pores were desorbed at higher temperatures (Michael Hirscher et al., 2010; Barbara Panella et al., 2008). Thereof, based on the thermal desorption studies and temperature dependent adsorption isotherm measurements of the researchers, they have concluded that the heat of adsorption of H<sub>2</sub> binding is determined by the pore size (Barbara Panella et al., 2008) and pointed out that the synthesise of a framework with a high specific surface area that possess narrow pores is a challenge to be addressed (Michael Hirscher et al., 2010; Barbara Panella et al., 2008; Schmitz et al., 2008).

In line with what has been addressed and reported in literature, by synthesizing Fe-BTCs via the perturbation assisted nanofusion synthesis strategy, we have introduced both narrow micropores and mesopores to the pore structure. Thereby, the BET surface and the total pore volume of Fe-BTC have been enhanced by 1.6 and 3.1 times, respectively. By introducing ultramicropores and narrow micropores to the pore structure of Fe-BTC-3, the H<sub>2</sub> adsorption capacity has been enhanced by 2.6 times (1.10 wt.% at 7.6 bar and 298 K) and showed experimentally that the presence of ultramicropores influences the adsorbed H<sub>2</sub> amounts, crucially.

#### **7.4. Comparison with Literature**

To the best of our knowledge, this research is the first study that reports the H<sub>2</sub> adsorption capacity of Fe-BTC at 298 K. By the perturbation assisted nanofusion synthesis strategy and control over textural porosity, an Fe-BTC that possesses ultramicropores in its pore structure were synthesized. Table 58 illustrates the H<sub>2</sub> adsorption capacity of some of those MOFs reported in literature.

Table 58. BET surface area, pore volume, and H<sub>2</sub> adsorption capacity of MOFs reported in literature

| MOF                                      | BET Surface Area (m <sup>2</sup> /g) | Pore Volume (cm <sup>3</sup> /g) | Pressure (bar) | Temperature (K) | H <sub>2</sub> Sorption Capacity | Reference                                                                               |
|------------------------------------------|--------------------------------------|----------------------------------|----------------|-----------------|----------------------------------|-----------------------------------------------------------------------------------------|
| Fe-BTC-3                                 | 1312.7                               | 1.41                             | 1              | 298             | 0.43 wt. % (2.1 mmol/g)          | This study                                                                              |
| Fe-BTC-3                                 | 1312.7                               | 1.41                             | 7.6            | 298             | 1.10 wt. % (5.47 mmol/g)         | This study                                                                              |
| MIL-100                                  |                                      | 1.0                              | 73.3           | 298             | 0.15 wt. %                       | (Latroche, Surblé, Serre, Mellot-Draznieks, Llewellyn, Lee, Chang, Sung, et al., 2006b) |
| MIL-101 (Cr)                             |                                      | 1.9                              | 80.0           | 298             | 0.43 wt. %                       | (Latroche, Surblé, Serre, Mellot-Draznieks, Llewellyn, Lee, Chang, Sung, et al., 2006b) |
| Co <sub>2</sub> (BDC) <sub>2</sub> dabco | 1595                                 | 0.77                             | 10             | 298             | 0.03 wt. %                       | (L. G. Zhu & Xiao, 2008)                                                                |
| HKUST-1                                  | 1154                                 |                                  | 65             | 298             | 0.35 wt. %                       | (Barbara Panella et al., 2006)                                                          |
| ZIF-8                                    |                                      |                                  | 60             | 298             | 0.13 wt. %                       | (W. Zhou et al., 2007)                                                                  |
| ZIF-8                                    | 1297                                 | 1.225                            | 10             | 298             | 0.390 mmol/g                     | (H. Zhou et al., 2015b)                                                                 |
| ZIF-8/GO                                 | 1247                                 | 1.281                            | 10             | 298             | 0.364 mmol/g                     | (H. Zhou et al., 2015b)                                                                 |
| Pt@ZIF-8/GO                              | 619                                  | 0.586                            | 10             | 298             | 0.841 mmol/g                     | (H. Zhou et al., 2015b)                                                                 |
| MOF-5                                    | 2296                                 |                                  | 65             | 298             | 0.28 wt. %                       | (Barbara Panella et al., 2006)                                                          |
| IRMOF-8                                  |                                      |                                  | 30             | 298             | 0.4 wt. %                        | (Dailly et al., 2006)                                                                   |
| Co-IRMOF-74                              | 1985                                 | 0.86                             | 170            | 298             | 0.29 wt. %                       | (Montes-Andrés, Orcajo, Martos, Botas, & Calleja, 2019)                                 |
| Ni <sub>50</sub> Co-IRMOF-74             | 1913                                 | 0.78                             | 170            | 298             | 0.39 wt. %                       | (Montes-Andrés et al., 2019)                                                            |
| MOF-184-Mg                               | 3154                                 |                                  | 20             | 298             | 0.15 wt. %                       | (Oh et al., 2017)                                                                       |
| MOF-184-Ni                               | 2449                                 |                                  | 20             | 298             | 0.11 wt. %                       | (Oh et al., 2017)                                                                       |

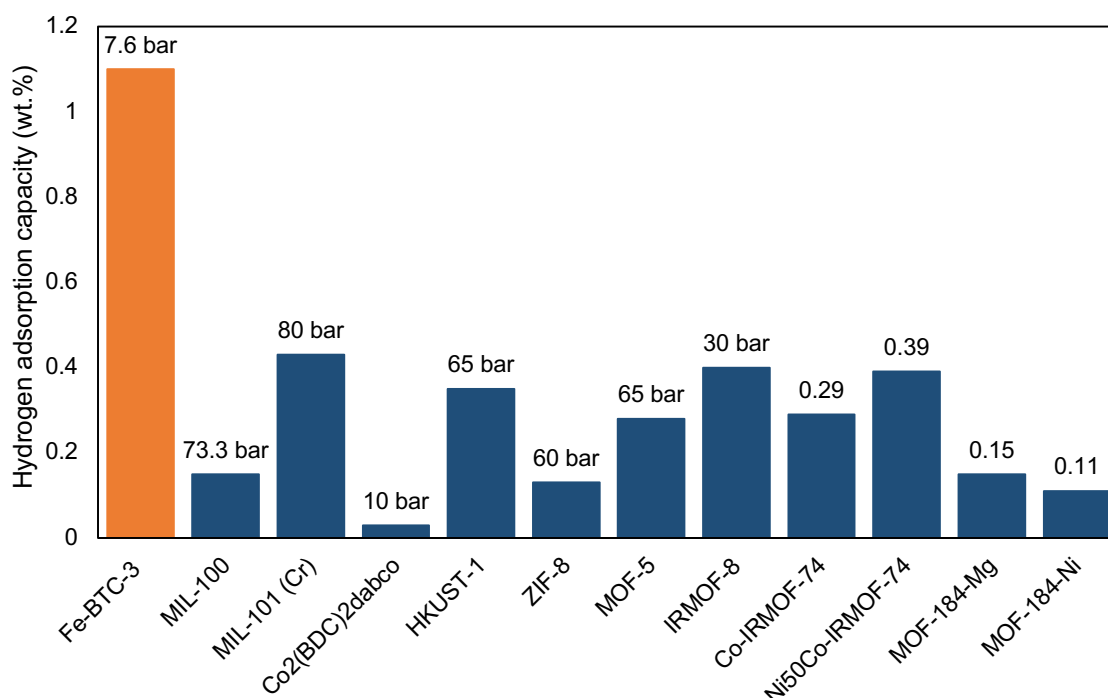


Figure 169. Comparison of H<sub>2</sub> adsorption capacities of Fe-BTC-3 and some of the MOFs reported in literature

By the perturbation assisted nanofusion synthesis strategy and control over textural porosity, a H<sub>2</sub> adsorption capacity (1.10 wt. % at 7.6 bar and 298 K) higher than those of reported MOFs has been achieved. Particularly, the measured H<sub>2</sub> adsorption capacity of MIL-100 at 73.3 bar and 298 K is 0.15 wt.% (Langmuir surface area: 2700 m<sup>2</sup>/g) (Latroche, Surblé, Serre, Mellot-Draznieks, Llewellyn, Lee, Chang, Sung, et al., 2006b); the measured H<sub>2</sub> sorption capacity of MIL-101(Cr) at 80 bar and 298 K is 0.43 wt.% (Langmuir surface area: 5500 m<sup>2</sup>/g) (Latroche, Surblé, Serre, Mellot-Draznieks, Llewellyn, Lee, Chang, Sung, et al., 2006b); the measured H<sub>2</sub> sorption capacity of Co<sub>2</sub>(BDC)<sub>2</sub>dabco at 10 bar and 298 K is 0.03 wt.% (BET surface area: 1595 m<sup>2</sup>/g, and pore volume. 0.77 cm<sup>3</sup>/g) (L. G. Zhu & Xiao, 2008); the measured H<sub>2</sub> sorption capacity of HKUST-1 at 65 bar and 298 K is 0.35 wt. % (BET surface area: 1154 m<sup>2</sup>/g) (Barbara Panella et al., 2006); the measured H<sub>2</sub> sorption capacity of ZIF-8 at 60 bar and 298 K is 0.13 wt. % (W. Zhou et al., 2007); the measured H<sub>2</sub> sorption capacity of MOF-5 at 65 bar and 298 K is 0.28 wt. % (BET surface area: 2296 m<sup>2</sup>/g) (Barbara Panella et al., 2006); the measured H<sub>2</sub> sorption capacity of IRMOF-8 at 30 bar and 298 K is 0.4 wt. % (Langmuir surface area: 1818 m<sup>2</sup>/g) (Dailly et al., 2006).

## 7.5. Concluding Remarks

The present study reports the H<sub>2</sub> adsorption capacity of hierarchically porous Fe-BTCs that has not been reported yet. A H<sub>2</sub> adsorption capacity (1.10 wt.% is achieved at 7.6 bar and 298 K) higher than those of reported MOFs (MIL-100 (Latroche, Surblé, Serre, Mellot-Draznieks, Llewellyn, Lee, Chang, Sung, et al., 2006b), MIL-101(Cr) (Latroche, Surblé, Serre, Mellot-Draznieks, Llewellyn, Lee, Chang, Sung, et al., 2006b), Co<sub>2</sub>(BDC)<sub>2</sub>dabco (L. G. Zhu & Xiao, 2008), HKUST-1 (Barbara Panella et al., 2006), ZIF-8 (W. Zhou et al., 2007), MOF-5 (Barbara Panella et al., 2006), and IRMOF-8 (Dailly et al., 2006)) has been achieved. By forming hierarchical pores, the highest BET surface area and the total pore volume for Fe-BTC has been reported (Dhakshinamoorthy, Alvaro, Chevreau, et al., 2012; Dhakshinamoorthy et al., 2011; Dhakshinamoorthy, Alvaro, & Garcia, 2012; X. Hu et al., 2016; Majano et al., 2013; Opanasenko et al., 2013; Torres et al., 2018; Zukal et al., 2015).

Herein, by the control of textural porosity via Fe:BTC ratio, an Fe-BTC that has ultramicropores in its pore structure has been synthesized and a BET surface area, and total pore volume that is higher than those of reported Fe-BTCs have been achieved (Dhakshinamoorthy, Alvaro, Chevreau, et al., 2012; Dhakshinamoorthy et al., 2011; Dhakshinamoorthy, Alvaro, & Garcia, 2012; X. Hu et al., 2016; Majano et al., 2013; Opanasenko et al., 2013; Torres et al., 2018; Zukal et al., 2015). Fe-BTC-3 possesses a H<sub>2</sub> adsorption capacity 2.6, and 2.8 times higher than Fe-BTC-1, and Fe-BTC-5, respectively. We have attributed this relatively high H<sub>2</sub> adsorption capacity to the ultramicropores present in its pore structure. Presence of ultramicropores maximizes the van der Waals potential. Thereby, the attraction felt from the surface of the ultramicropore walls increases which causes adsorbed H<sub>2</sub> amount to increase. In the case of Fe-BTC-1 and Fe-BTC-5, despite the relatively low BET surface area, and the relatively low narrow micropore volume of Fe-BTC-1, the H<sub>2</sub> adsorption capacity of Fe-BTC-1 is 1.1 times greater than Fe-BTC-5. The relatively high H<sub>2</sub> adsorption capacity of Fe-BTC-1 in comparison to Fe-BTC-5 is attributed to the narrow distribution of narrow micropores of Fe-BTC-1.

Our results indicate that H<sub>2</sub> adsorption capacity depends on: i) the presence of ultramicropores; and ii) the narrow distribution of narrow micropores (pore diameters smaller than 1 nm) through the micropore size distribution. Based on our results, we have

concluded that higher the ultramicropore volume and the narrower the narrow micropore distribution (pore diameters smaller than 1 nm) through the micropores, the higher will be the adsorbed H<sub>2</sub> amount.

By the control of textural porosity via Fe:BTC ratio, an Fe-BTC that has ultramicropores in its pore structure has been synthesized and a BET surface area, and total pore volume that is higher than those of reported Fe-BTCs have been achieved (Dhakshinamoorthy, Alvaro, Chevreau, et al., 2012; Dhakshinamoorthy et al., 2011; Dhakshinamoorthy, Alvaro, & Garcia, 2012; X. Hu et al., 2016; Majano et al., 2013; Opanasenko et al., 2013; Torres et al., 2018; Zukał et al., 2015). Presence of ultramicropores enhances the H<sub>2</sub> adsorption capacity by 2.6 and 2.8 times and a H<sub>2</sub> sorption capacity that is higher than those of reported MOFs has been reported.

Our results experimentally prove that presence of ultramicropores enhances the H<sub>2</sub> adsorption capacity. Nevertheless, studies should be focused on synthesizing ultramicroporous sorbents to achieve the H<sub>2</sub> storage target set by DOE.

## Chapter VIII

### Conclusion and future works

#### 8.1. Conclusion

In this Ph.D. thesis, hierarchical porous MOFs and its advantages over the gas adsorption studies have been discussed. It is found that via a perturbation assisted nanofusion synthesis strategy, hierarchical porous MOFs with enhanced BET surface areas, increased pore volumes and improved gas adsorption capacities can be synthesized. In addition, the significance of ultramicropores, and narrow micropores on the gas adsorption capacities have been shown, experimentally.

Perturbation assisted nanofusion synthesis strategy offers a variety of opportunities. Perturbation assisted nanofusion synthesis strategy is a template free synthesis strategy that there is no need to remove the template and thus, the possibility of framework collapse is eliminated. Moreover, by the perturbation assisted nanofusion synthesis strategy a two-pore system is created at which micropores increase the surface area and mesopores enhance the mass transport properties. Additionally, by varying the synthesis temperature and metal to linker ratio, sizes of textural pores can be tuned, finely. For instance, at high synthesis temperatures ( $> 120\text{ }^{\circ}\text{C}$ ), MIL-88B nanorods pack loosely and wider mesopores form while at lower synthesis temperatures ( $< 120\text{ }^{\circ}\text{C}$ ), MIL-88B nanorods pack tightly and narrower pores form. Moreover, in the presence of excess metal salt (a high metal to linker ratio), iron oxide clusters form prior to SBU formation, interparticle voids in between the SBU aggregates widen and wider pores are formed.

Textural porosity provides flexibility to tune the pore size via synthesis temperature and metal to linker ratio. Moreover, by the perturbation assisted nanofusion synthesis strategy, BET surface area and the pore volume are enhanced significantly, and the highest of all the reported BET surface areas and the pore volumes for MIL-88B and Fe-BTC are achieved. Particularly, BET surface areas of MIL-88B and Fe-BTC are enhanced by 2.7 and 1.6 times, respectively while the total pore volumes of MIL-88B and Fe-BTC are enhanced by 4.1, and 3.1 times, respectively.

Besides the improvements achieved in textural properties, by constructing hierarchical pores, gas adsorption performances of hierarchical porous MIL-88B and Fe-BTC are improved, considerably. As reported by Bhatia and Myers, thermodynamically 15.1 kJ/mol of energy is needed to adsorb considerable amount of gas at 298 K (Bhatia & Myers, 2006b). However, the isosteric heat of adsorption values of MOFs range in between 4 to 7 kJ/mol. Reported strategies to date, show promising results with enhancements in gas adsorption capacities. However, achieved gas adsorption capacities are not sufficient enough to meet the DOE target of onboard hydrogen storage. Despite the given efforts, there is still room for improvement for gas adsorption studies conducted at ambient temperature. To increase the isosteric heat of adsorption value of MOFs at ambient temperatures, we synthesized hierarchically porous MOFs and introduced ultramicropores to the pore structure. Forming textural pores and introducing ultramicropores to the pore structure enhanced the gas adsorption capacities of the two MOFs reported in this study. Particularly, CO<sub>2</sub> adsorption capacities of MIL-88B and Fe-BTC are enhanced by 2.1 and 1.6 times, respectively while H<sub>2</sub> adsorption capacities of MIL-88B and Fe-BTC are enhanced by 1.96 and 2.6 times, respectively. The enhanced gas (CO<sub>2</sub> and H<sub>2</sub>) adsorption capacities are attributed to: i) the presence of ultramicropores (pore diameters smaller than 0.7 nm), ii) the volume of ultramicropores, iii) the volume of narrow micropores (pore diameters smaller than 1 nm), and iv) the narrow distribution of ultramicropores through the micropore size distribution (high fraction of ultramicropores).

The significance of ultramicropores lies behind their increased binding energies. Revealed by theoretical studies, as pore diameters decrease below 1 nm, van der Waals interactions between the pores and the gas molecules strengthen and higher adsorption capacities can be achieved. Theoretically, the highest gas adsorption capacity can be achieved by pores with pore diameters of 6 to 8 Å which can be explained by Lenard-Jones potential. As the gas molecules and the adsorbent are separated by a long distance, attractive forces dominate while the repulsion forces dominate when the gas molecules and the adsorbent are separated by a short distance. Particularly, theoretical studies show that when hydrogen molecules are adsorbed on wider pores, a hydrogen layer would be formed on the wells located close to the pore walls and a less dense layer of hydrogen would be adsorbed on the center of the pore that minimizes the attraction felt by the pore walls, and thereby H<sub>2</sub> adsorption capacity decreases. In line with what has been reported in theoretical studies, our



results experimentally prove that presence of ultramicropores enhances the gas adsorption capacities, considerably.

We designed and synthesized hierarchical porous MOFs with enhanced BET surface area and pore volume and improved gas adsorption performances. Forming ultramicropores and hierarchical pores has a key role in enhancing the gas adsorption capacities. By experimentally proving the necessity of ultramicropores in gas adsorption studies, we report an effortless, feasible synthesis strategy that can enhance the gas adsorption capacities, considerably and pave the way for the design and use of hierarchical porous MOFs.

## 8.2. Future work

Hierarchical porous MOFs show promising results in CO<sub>2</sub> and H<sub>2</sub> adsorption studies. However, the following has to be considered for the commercial use of these materials:

It is known that CO<sub>2</sub> adsorption capacities of MOFs decrease in the presence of water molecules as the water molecules compete with CO<sub>2</sub> molecules for the available adsorption sites. Therefore, CO<sub>2</sub> adsorption capacities should be retested in the presence of water.

Moreover, flue gas possesses different kinds of molecules which would compete with CO<sub>2</sub> molecules for the available adsorption sites. CO<sub>2</sub> adsorption capacity of hierarchical porous MOFs should be investigated under flue gas environment.

For the commercial use of hierarchical porous MOFs, mechanical strength of these materials should be tested. MOFs are shaped into pellets prior to their use in commercial applications. Adsorption capacity of hierarchical porous MOF pellets should be retested.

The CO<sub>2</sub>/N<sub>2</sub> selectivity of hierarchical porous MOFs were not tested since the scope of this study was limited with the development of hierarchical porous MOFs for enhanced CO<sub>2</sub> and H<sub>2</sub> adsorption capacities (at 298 K). However, isosteric heat of adsorption values of CO<sub>2</sub> and N<sub>2</sub> may provide insight about the performance of selective CO<sub>2</sub>/N<sub>2</sub> separation. For further studies, isosteric heat of adsorption values of CO<sub>2</sub> and N<sub>2</sub> should be investigated.

The measured H<sub>2</sub> adsorption capacities of the two hierarchical porous MOFs reported in this study cannot meet the DOE target for onboard hydrogen storage. However, forming ultramicropores enhances the measured H<sub>2</sub> adsorption capacities, considerably. This strategy of forming textural pores should be tested on other MOFs and their H<sub>2</sub> adsorption capacities should be investigated.

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